

Purpose: Specify layout of piping system. Specify materials (type + quantity) Explain why kinetic radial pump is needed. Demonstrate that pump will not suffer cavitation. Prepare a list of materials.

Final Test

Data

$$Sg_{\text{coolant}} = 0.94 \quad \rho = 58.7 \text{ lb/ft}^3$$

Freezing point = 0°

V = 1.5 x that of water (temp?)

Operation:

2 shifts / day > relevant?

7 days / wk

Reservoir Pump - Wkly

Coolant Pickup - monthly

Coolant Storage: 15,000 gal

Reservoir: 1000 gal

Dirty coolant: 1000 gal / wk

• pick up 1 / month

• $4(1000) + 1000$ (emergency)

= 5,000 gal

Frost Line: 30"

Time constraint ≥ 6 hoursPipe Lengths: Rail Tank $\rightarrow$ Storage: 700'Storage $\rightarrow$ Reservoir $\rightarrow$ 110' Reservoir to Machine: $3.28' \times (2)$ Reservoir $\rightarrow$ Dirty Coolant: 400' Dirty Coolant $\rightarrow$ Truck: 10'Procedure: critical velocity $3 \text{ m/s} = 9.843 \text{ ft/s} = 0.0928 \text{ ft/s}$

$$Q = \frac{V}{t} = \frac{1500 \text{ gal}}{3600} = 41.67 \text{ gpm} \quad \text{① Select pipe material / size}$$

$$Q = V \times A$$

$$0.0928 \text{ ft/s} = 9.843 \text{ ft/s} \times A$$

$$A = 0.009428 \text{ ft}^2 = 1.358 \text{ in}^2$$

$$V = \frac{Q}{A} = \frac{5.571 \text{ ft}^3/\text{min}}{0.02333 \text{ ft}^2} = 3.98 \text{ ft/s} \quad \checkmark$$

$$d = \sqrt{\frac{4(1.358)}{\pi}} = 1.3149 \text{ in}$$

Choice: 2" schedule 40 steel

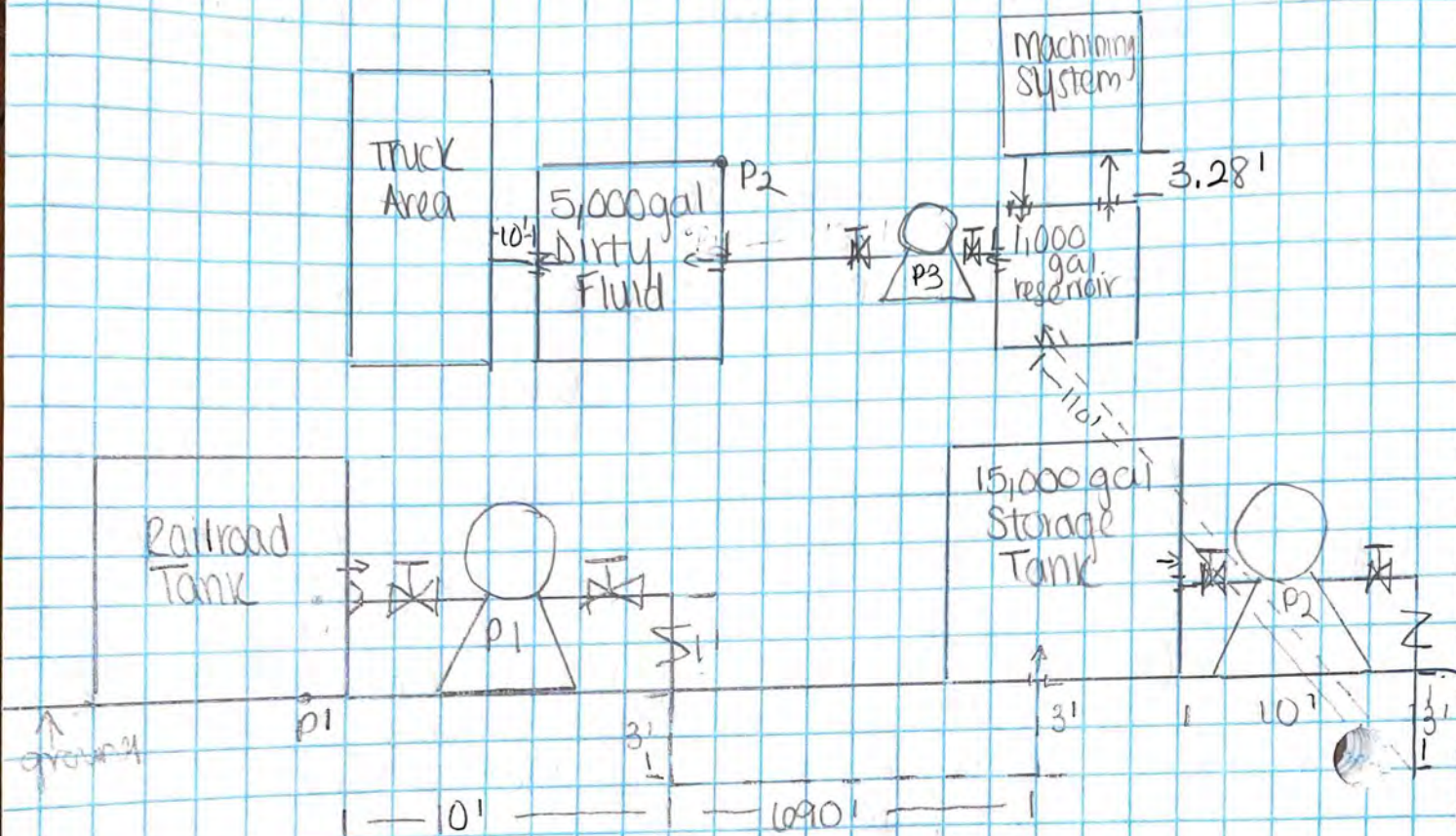
$$d_o = 2.067, d_i = 2.375 \text{ in}$$

$$A_p = 0.02333 \text{ ft}^2$$

② Decide Route: 10' of pipe from RR Tank to elbow, 1' down to ground, 3' below ground, 1090' to storage, 3' to meet tank, 10' from storage to elbow, 1' down to ground, 3' underground, 110' underground to reservoir, 6.56' from reservoir to machine and back, 400' from reservoir to dirty tank, 10' to truck area.

underground total: 809' Above ground total: 438.56'
Total pipe length: 1247.56'

② Drawing: Proposed pipe/pump system



Materials: (3) pumps: (1) 1.5x3-8 (10" impeller), (2) 1x2-7.5 (5" impeller)

Pipe length: 1247.56 ft, 2" sch. 40 pipe

(6) gate valves $\frac{L_e}{D} = 8 = 48$

(2) check valves $\frac{L_e}{D} = 50 = 100$

(5) elbow (90°) $\frac{L_e}{D} = 30 = 150$

(5) sharp edged outlets, $K = 1.0 = 5.0$

(4) sharp edged inlets, $K = 0.5 = 2.0$

$$\Delta z = 4.92'$$

③ compute h_L using Bernoulli: $h_L = \left(f \frac{L_{eq}}{D} + \sum K \right) \frac{V^2}{2g}$

(A) RR Tank to Storage Tank:

$$V_1 = \frac{0.1114 \text{ ft}^3/\text{s}}{0.0233 \text{ ft}^2} = 4.78 \text{ ft/s} \quad \frac{(4.78 \text{ ft/s})^2}{(2 \times 32.2)} = 0.355 \text{ ft}$$

$$Re = \frac{VD}{\nu} = \frac{4.78 \times 0.17225}{1.62 \times 10^{-5}} = 50,820 \text{ (turbulent)} \quad f = 0.023$$

③ cont.

(B) Storage Tank to Reservoir

$$V_B = \frac{0.0371 \text{ ft}^3/\text{s}}{0.0233 \text{ ft}^2} = 1.59 \text{ ft/s} \quad \frac{(1.59 \text{ ft/s})^2}{(2 \times 32.2)} = 0.039 \text{ ft}$$

$$Re = \frac{1.59 \times 0.17225}{1.62 \times 10^{-5}} = 16,910 \text{ (turbulent)} \quad f = 0.028$$

④ $\left(\frac{L_e}{D}\right) = 2(8) + 50 + 3(30) = 156$

$$L_{eq} = 704 + (156 \times 0.17225) = 730.87$$

$$\sum K_A = 0.5 + 1.0 = 1.5$$

$$h_{LA} = \left(0.2333 \times \frac{730.87}{0.17225} + 1.5\right) \times 0.355 \text{ ft} = 35.48 \text{ ft}$$

⑤ $\sum \frac{L_e}{D} = 4(8) + 50 + 2(30) = 142 \quad L_{eq} = 543.50' + (142 \times 0.17225) = 568.02'$

$$\sum K_B = 1.5 + 4 = 5.5$$

$$h_{LB} = \left(0.0278 \times \frac{568.02}{0.17225} + 5.5\right) \times 0.039' = 3.79'$$

$$h_{total} = 35.48 + 3.79 = 39.27 \text{ ft} + \Delta z(4.92) = 44.19 \text{ ft}$$

④ Select pumps from catalog: Req. $P_1 - 50 \text{ gpm}$ $P_2/P_3 - 16.67 \text{ gpm}$
 $1.5 \times 3 \times 8$ Pumps: $1 \times 2 \times 7.5$ (see attached
 $P_1: 6''$ impeller $P_2/P_3: 5''$ impeller pump map)
 (See attached performance curve)

$$BHP = \frac{Q \times H \times SG}{3960 \times \eta_p} = \frac{50 \times 44.19 \times 0.94}{3960 \times 0.45} = 0.524 \text{ HP} = 1.16 \times 1.1 = 1.28 \text{ HP}$$

$$BHP_{P_2/P_3} = \frac{16.67 \times 44.19 \times 0.94}{3960 \times 0.45} = 0.1718 = 0.388 \times 1.1 = 0.427 \text{ HP}$$

1.51 HP

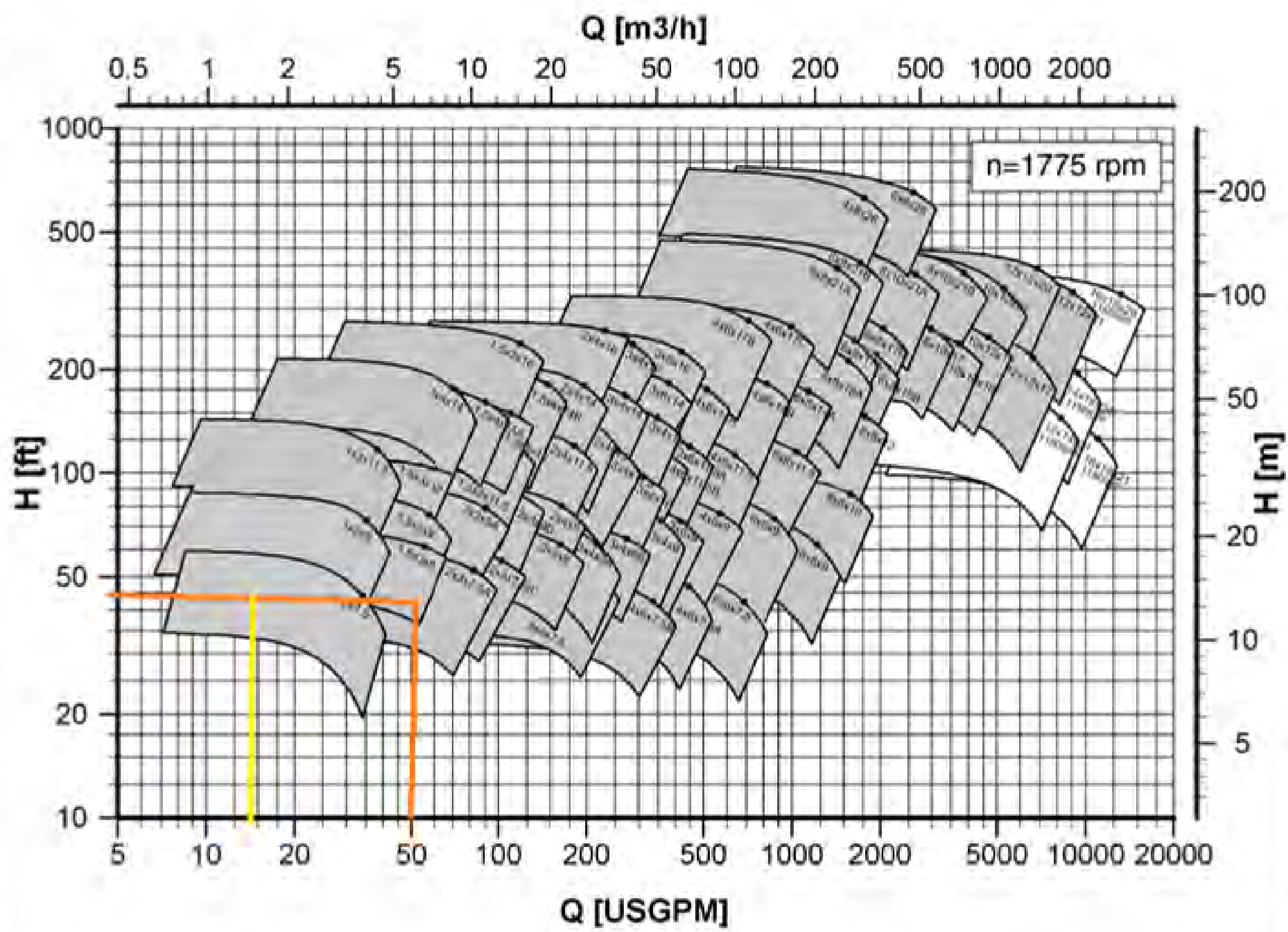
P_1 $NSPH_r = 2.0 \text{ ft}$ $NSPH = 34.14 \text{ ft} \times 2 \times 0.3 - 2.3 \text{ ft} = 33.5 \text{ ft}$ $33.5 \text{ ft} > 2.0 \text{ ft}$

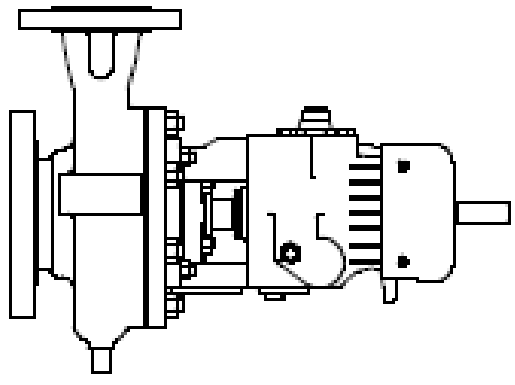
P_2/P_3 $NSPH_r = 1.5 \text{ ft}$ $NSPH = 33.57 \text{ ft}$ ✓

The head far exceeds pump requirements.
No cavitation

Kinetic vs. Positive Displacement: Kinetic pumps are best for fluids up to moderate viscosity. Our fluid is 1.5x more viscous than water. The head for the system is high with a low flow rate which is great for kinetic radial pump. Positive displacement pumps are for highly viscous fluids or system with very high pressure.

④
Summary ; Since the head is significantly higher than required head for system there will be no cavitation. The actual flow rate at operating point is 36.10 gpm and roughly 55 ft of head. Pump 1 will require 1.5 HP, and 2+3: 0.5 HP. The total lengths of pipes and fittings are as listed under materials.





1 x 2 x 7.5 -1 OHH

SULZER

Series 2.00 / 60Hz E001

Curve No	OHH 53-1-1-02	NSS	10190 (197)	Speed 3520
Efficiency Basis	API Std. clearances	NS	560 (11)	
Max Solid	.20 in (5 mm)	Rotation	CCW viewed from coupling	

