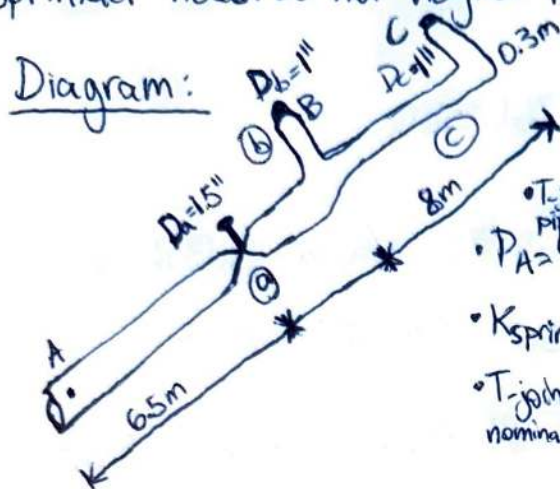


*Please grade Question 2 towards this test.

1) Purpose: For a wide-open ball valve, determine the flow rate delivered to each sprinkler head. Do not neglect minor losses.



Data & Variables

- A to T-joint: 1 1/2 in nominal pipe of 6.5 m
- T-joint to 1st sprinkler head: 1 in nominal pipe of 0.3 m
- $P_A = 400 \text{ kPa (gauge)}$
- $K_{\text{sprinkler}} = 50$
- T-joint to 2nd sprinkler head: 1 in nominal pipe of 8.3 m

Sources:

Mott & Untener. "Applied Fluid Mechanics", 7th edition, Pearson Education Inc (2015)

Design Considerations:

- Incompressible Fluid
- Steady state
- Isothermal

Materials:

Water flowing in Schedule 40 steel pipe

Procedure & Calculations:

Applying Bernoulli between A & B:

$$\frac{P_A}{\rho} + \frac{V_A^2}{2g} + Z_A = \frac{P_B}{\rho} + \frac{V_B^2}{2g} + Z_B + (h_L)_{A-B}$$

$$\frac{P_A}{\rho} - Z_B = \frac{V_B^2 - V_A^2}{2g} + (h_L)_{A-B} \rightarrow (1)$$

$$(h_L)_{A-B} = (h_L)_{\text{pipe-a}} + (h_L)_{\text{pipe-b}} + (h_L)_{\text{valve}} +$$

$$(h_L)_{T\text{-joint}} + (h_L)_{\text{sprinkler}} + (h_L)_{\text{reduction}}$$

$$\begin{aligned} (h_L)_{\text{pipe-a}} &= f_a \frac{L_a}{D_a} \frac{V_a^2}{2g} \\ &= f_a \left(\frac{L_a}{D_a} \right) \frac{1}{2g} \left(\frac{Q_a}{A_a} \right)^2 \\ &= \frac{8 f_a L_a Q_a^2}{\pi^2 g D_a^5} \\ &= \frac{8 f_a (6.5) Q_a^2}{\pi^2 (9.81) (40.9 \times 10^{-3})^5} \\ &= 4692648.781 f_a Q_a^2 \end{aligned}$$

$$\begin{aligned} (h_L)_{\text{pipe-b}} &= \frac{8 f_b L_b Q_b^2}{\pi^2 g D_b^5} \\ &= \frac{8 f_b (0.3) Q_b^2}{\pi^2 (9.81) (26.6 \times 10^{-3})^5} \\ &= 1861376.839 f_b Q_b^2 \end{aligned}$$

$$\begin{aligned} (h_L)_{\text{valve}} &= K_{\text{valve}} \left(\frac{V_a^2}{2g} \right) = \frac{K_{\text{valve}}}{2g} \left(\frac{4 Q_a}{\pi D_a^2} \right)^2 \\ &= 340 \times 0.02 \frac{8}{\pi^2 \times 9.81} \times \frac{1}{(40.9 \times 10^{-3})^4} Q_a^2 \\ &= 200787.612 Q_a^2 \end{aligned}$$

$$(h_L)_{T\text{-joint}} = K_T \times \frac{V_a^2}{2g} = 35433.108 Q_a^2$$

$$\begin{aligned} (h_L)_{\text{reduction-b}} &= K_{\text{elb-b}} \times \frac{V_b^2}{2g} \\ &= 0.14 \times 8 \times \frac{Q_b^2}{\pi^2 \times 9.81 (26.6 \times 10^{-3})^4} \\ &= 23105.891 Q_b^2 \end{aligned}$$

$$(h_L)_{\text{sprinkler}} = K_{\text{spr}} \times \frac{8Q_b^2}{\pi^2 g D_b^5}$$

$$= 50 \times \frac{8Q_b^2}{\pi^2 \times 9.81 \times (26.6 \times 10^{-3})^5}$$

$$= 8252103.988 Q_b^2$$

$$(h_L)_{\text{pipe-c}} = \frac{8f_c L_c Q_c^2}{\pi^2 g D_c^5} = \frac{0.029 \times 8 \times 8.3 \times Q_c^2}{(26.6 \times 10^{-3})^5 \pi^2 \times 9.81}$$

$$= 1493444.684 Q_c^2$$

$$(h_L)_{\text{To bend}} = K_{\text{rec}} \times \frac{8Q_a^2}{\pi^2 g D_a^4}$$

$$= \frac{20 \times 0.02 \times 8Q_a^2}{\pi^2 \times 9.81 \times (40.9 \times 10^{-3})^4}$$

$$= 11811.036 Q_a^2$$

$$(h_L)_{\text{red c}} = K_{\text{red}} \times \frac{8Q_c^2}{\pi^2 g D_c^4}$$

$$= \frac{0.14 \times 8Q_c^2}{\pi^2 \times 9.81 \times (26.6 \times 10^{-3})^4}$$

$$= 23105.891 Q_c^2$$

$$(h_L)_{\text{elbow}} = \frac{50 \times 0.022 \times 8Q_c^2}{\pi^2 \times 9.81 \times (26.6 \times 10^{-3})^4}$$

$$= 108927.773 Q_c^2$$

$$(h_L)_{\text{Spri}} = 8252103.988 Q_c^2$$

$$40.599 = \frac{V_c^2 - V_a^2}{2g} + (h_L) \left| \begin{array}{l} V_c = \frac{4Q_c}{\pi D_c^2} \\ V_a = \frac{4Q_a}{\pi D_a^2} \end{array} \right.$$

Analysis:

The flows through sprinklers are very similar. There is a difference of 5.26%, so no need to modify the system. The flow velocity varies from 3.02 m/s to 3.69 m/s (for 1st sprinkler). We should use a larger pipe in path (b) but that will increase the flow rate towards 1st sprinkler. We could either leave pipe (b) as it is a increase in size, but use a valve in pipe (b) to control flow.

Substitute in Bernoulli's equ. ①

$$\frac{P_A}{\gamma} - Z_B = \frac{V_B^2 - V_A^2}{2g} + (h_L)_{A \rightarrow B}$$

$$V_B = \frac{4Q_b}{\pi D_b^2} = 1799.479 Q_b$$

$$V_A = \frac{4Q_a}{\pi D_a^2} = 761.138 Q_a$$

$$\frac{P_A}{\gamma} - Z_B = 4692648.781 f_a Q_a^2 + 1861376.839 f_b Q_b^2 + 206693.144 Q_a^2 + 8440251.958 Q_b^2$$

$$40.599 = 8510984.278 Q_b^2 + 324009.3635 Q_a^2 \rightarrow \text{②}$$

Bernoulli's between A-C:

$$\frac{P_A}{\gamma} - Z_C = \frac{V_c^2 - V_A^2}{2g} + (h_L)_{\text{pipe-a}} + (h_L)_{\text{pipe-c}} + (h_L)_{\text{valve}} + (h_L)_{\text{T-bend}} + (h_L)_{\text{red c}} + (h_L)_{\text{elb}} + (h_L)_{\text{spri-c}}$$

$$40.599 = 165042.079 Q_c^2 - 29527.576 Q_a^2 + 1493444.684 Q_c^2 + 200787.612 Q_a^2 + 11811.036 Q_a^2 + 23105.891 Q_c^2 + 108927.773 Q_c^2 + 8252103.988 Q_c^2$$

$$40.599 = 300387.2915 Q_a^2 + 10042624.42 Q_c^2 \rightarrow \text{④}$$

From ②, ④ we have 2 equations & 3 unknowns and $Q_a = Q_b + Q_c \rightarrow \text{③}$

②, ③, ④

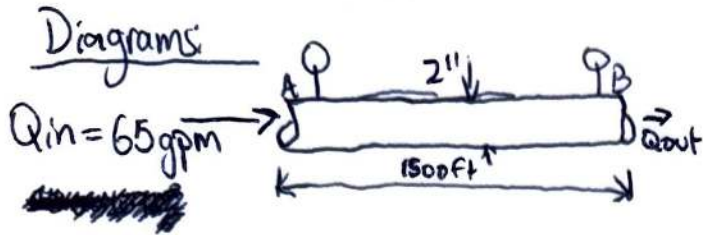
$$\rightarrow Q_b = 0.002 \text{ m}^3/\text{s}$$

$$Q_c = 0.0019 \text{ m}^3/\text{s}$$

$$Q_a = 0.0039 \text{ m}^3/\text{s}$$

2) Purpose: Determine the pressure drop & expected increase in flow rate after modification

Diagrams:



Data & Variables:

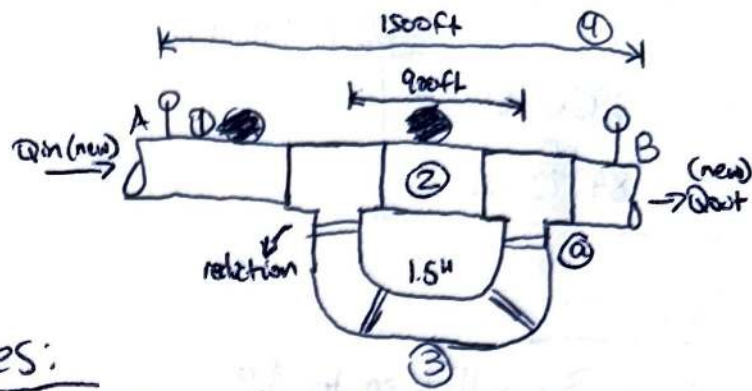
- Length of standard steel tubing = 1500 ft
- D (inner diameter of 2 in tube) = 0.1558 ft
- g (acceleration due to gravity) = 32.2 ft/s²
- Q (Flow rate) = 65 gpm = 0.144831 cubic ft/s

Sources:

Mott & Untener. "Applied Fluid Mechanics", 7th edition
Pearson Education Inc (2015)

Materials:

water flowing through standard steel tubing



Design Considerations:

- Incompressible state
- Steady state
- Isothermal

Procedure & Calculations:

For case 1:

Applying Bernoulli's equation between A & B:

$$\frac{P_A}{\rho g} + \frac{V_A^2}{2g} + Z_A = \frac{P_B}{\rho g} + \frac{V_B^2}{2g} + Z_B + h_L \quad (1)$$

As, flow rate is same throughout tube & diameter is also the same. $V_A = V_B$, $Z_A = Z_B$ (elevation change)

$$\frac{P_A - P_B}{\rho g} = h_L \Rightarrow \Delta P = \rho g h_L \quad (2)$$

Cross sectional area of tube:

$$A = \frac{\pi}{4} \times D^2 = \frac{\pi}{4} \times 0.1558^2$$

$$A = 0.01906 \text{ ft}^2$$

By continuity equation:

$$\text{Flow rate, } Q = A \times V$$

$$V = \frac{Q}{A} = \frac{0.144831}{0.01906}$$

$$V = 7.5947 \text{ ft/sec}$$

Reynolds number:

$$Re = \frac{VD}{\nu} = \frac{7.5947 \times 0.1558}{1.89 \times 10^{-5}}$$

$$(\text{Kinematic viscosity} = 1.89 \times 10^{-5} \text{ ft}^2/\text{sec})$$

$$Re = 62,606.1$$

$$\text{Relative Roughness} = \frac{D}{E} = \frac{0.1558}{1.5 \times 10^{-4}} = 1038.67$$

(For steel pipe, $E = 1.5 \times 10^{-4} \text{ ft}$)

$$\text{Relative Roughness} = 1038.67$$

From Moody chart, Friction Factor, $f = 0.024$

$$\text{Head loss, } h_L = f \left(\frac{L}{D} \right) \frac{V^2}{2g}$$

$$= 0.024 \left(\frac{1500}{0.1558} \right) \left(\frac{7.5947^2}{2 \times 32.2} \right)$$

$$h_L = 206.952 \text{ ft}$$

From eq. (2):

$$\text{Pressure drop } (\Delta P) = sg \cdot h_L \\ = 62.43 \times 206.952$$

$$\Delta P = 12920 \text{ lbf/ft}^2 \\ \text{or} \\ 89.72 \text{ psi}$$

Case 2:

Applying Bernoulli's eq. to A-B:

$$\frac{P_A}{sg} + \frac{V_A^2}{2g} + Z_A = \frac{P_B}{sg} + \frac{V_B^2}{2g} + Z_B + h_L$$

$$(\because Z_A = Z_B \text{ \& } V_A = V_B)$$

$$\frac{P_A - P_B}{sg} = h_L \rightarrow (3)$$

Energy loss @ branch 2:

$$\frac{\Delta P}{sg} = f_2 \left(\frac{L}{D} \right) \left(\frac{V_2^2}{2g} \right) + 2 \left[20 f_r \frac{V_2^2}{2g} \right] \rightarrow (4)$$

$$A_1 Q_1 = A_2 V_2 \rightarrow V_2 = \frac{Q_2}{A_2}$$

$$\frac{\Delta P}{sg} = \left[f_2 \left(\frac{1500}{0.1558} \right) + 2(20)(0.019) \right] \times \frac{1}{2(32.2)} \frac{1}{(0.01906)^2} \times Q_2^2$$

$$Q_2 = \sqrt{\left(\frac{0.0234 \Delta P}{sg} \right) \left(\frac{1}{f_2(9627.7) + 0.76} \right)}$$

Let us assume $f_2 = 0.01$

$$Q_2 = \sqrt{\frac{(0.0234)(12920)}{62.43} \left(\frac{1}{0.01(9627.7) + 0.76} \right)}$$

$$Q_2 = 0.223395 \text{ ft}^3/\text{s} \text{ or } 100.266 \text{ gpm}$$

Analysis:

Rate of flow through sections 1 & 4 will remain unchanged as initial.

Increased flow rate for section 2:

Similarity for section 3,

$$\frac{\Delta P}{sg} = h_{L3} + 2(h_L)_{TEE} + (h_L)_{\text{reduction}} + (2h_L)_{\text{elbow}} + h_{L(\text{enlargement})}$$

$$\Rightarrow \frac{\Delta P}{sg} = f_3 \left(\frac{L}{D} \right) \frac{V_3^2}{2g} + 2(60 \text{ ft}) \frac{V_3^2}{2g} + 0.045 \left(\frac{V_3^2}{2g} \right) + 2(30 \text{ ft}) \frac{V_3^2}{2g} + 0.36 \left[\frac{V_3^2}{2g} \right]$$

$$\Rightarrow \frac{\Delta P}{sg} = \frac{V_3^2}{2g} \left[f_3 \left(\frac{L}{D} \right) + 2(60(0.022)) + 0.045 + 2(30)(0.022) + 0.36 \right]$$

$$\Rightarrow \frac{\Delta P}{sg} = \frac{1}{2g A_3^2} Q_3^2 \left[f_3 \left(\frac{900}{0.1142} \right) + 4.365 \right] = \frac{1}{2(32.2)(0.0123)^2} Q_3^2 \left[f_3(7880.9) + 4.365 \right]$$

$$[\because A_3 = \frac{\pi}{4} \times d_3^2 \text{ \& } d_3 = 1.5 \text{ in} = 0.125 \text{ ft}]$$

$$A_3 = \frac{\pi}{4} \times (0.125)^2 = 0.0123 \text{ ft}^2$$

$$\Rightarrow Q_3 = \sqrt{\left(\frac{0.00675 \Delta P}{sg} \right) \left(\frac{1}{f_3(7880.9) + 4.365} \right)}$$

Let us assume $f_3 = 0.01$

$$Q_3 = \sqrt{\frac{0.00675 \times 12920}{62.4 \times [0.01 \times 7880.9 + 4.365]}}$$

$$Q_3 = 0.129596 \text{ ft}^3/\text{s} \text{ or } 58.166724 \text{ gpm}$$

Increased flow rate through section 3