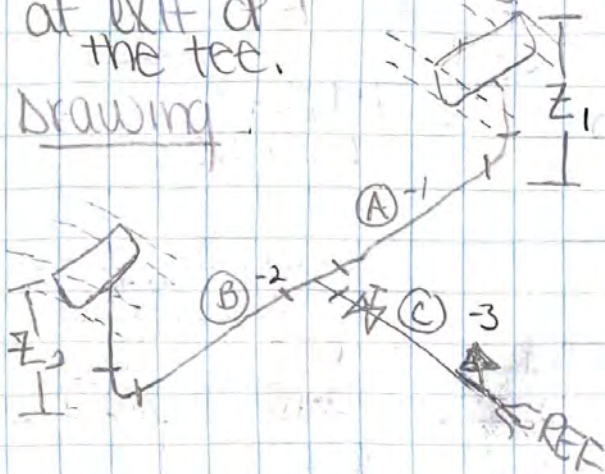


① Purpose: Determine the flow out of the system if gate valve is half open. Determine if velocity meets criteria. Compute pressure at exit of the tee.

Drawing



Sources: MOTT, Robert L.; UNTENER, JOSEPH A., Applied Fluid Mechanics, 7th, -2015.

Design Considerations:

- ① Incompressible
- ② Isothermal
- ③ Steady State

Data + Variables

$D = 0.75 \text{ in} = 0.0254 \text{ m}$ $\mu = 0.01905 \text{ m}$ Roughness: $\Delta/\epsilon = 0.01905 \text{ m} / 4.6 \times 10^{-5} \text{ m} = 414.13$
 $L_A = 10 \text{ m}$ $L_B = 9 \text{ m}$ $L_C = 10 \text{ m}$ $f_T = 0.0246$ (moody chart)
 $z_1 = 4 \text{ m}$ $z_2 = 3 \text{ m}$ $z_3 = 0 \text{ m}$ $sw = 9.79 \text{ kN/m}^3$
 $\epsilon = 4.6 \times 10^{-5} \text{ m}$ (table 8.2) $K_{\text{valve}} = 160$ $K_{\text{tee}} = 60$ $K_{\text{entrance}} = 0.5$ (fig 10.14) $K_{\text{exit}} = 30$

Calculations + Procedures:

Materials: water

Apply Bernoulli's Energy equation: A-C

$A = \frac{\pi D^2}{4} \rightarrow V = \frac{Q}{A} = \frac{4Q}{\pi D^2}$

$$z_1 = \frac{V_C^2}{2g} + K_{\text{ent}} \frac{V_A^2}{2g} + K_{\text{elb}} \frac{V_A^2}{2g} + K_{\text{tee}} \frac{V_A^2}{2g} + K_{\text{valve}} \frac{V_A^2}{2g} + f \frac{L_A}{D} \frac{V_A^2}{2g} + f \frac{L_C}{D} \frac{V_C^2}{2g}$$

Substituted:

$$z_1 = \left(\frac{8}{9\pi^2 D^4} + \frac{8K_{\text{val}} \cdot 1/2}{9\pi^2 D^4} + \frac{8f L_C}{9\pi^2 D^5} \right) Q_3^2 + \left[\frac{8}{9\pi^2 D^4} (K_{\text{ent}} + K_{\text{elb}} + K_{\text{tee}}) + \frac{8f L_A}{9\pi^2 D^5} \right] Q_1^2$$

Substitute:

$$4 \text{ m} = \left(\frac{8}{9.81 \times \pi^2 (0.01905)^4} + \frac{8 \times 160 \times 0.0246}{9.81 \times \pi^2 (0.01905)^4} + \frac{8 \times 0.0246 \times 10}{9.81 \times \pi^2 (0.01905)^5} \right) Q_3^2 + \left[\frac{8}{9.81 \times \pi^2 (0.01905)^4} (0.5 + 30 \times 0.0246 + 60 \times 0.0246) + \frac{8 \times 0.0246 \times 10}{9.81 \times \pi^2 (0.01905)^5} \right] Q_1^2$$

EQ ① $4 \text{ m} = 11198622.15 Q_3^2 + 9804549.62 Q_1^2$

Apply Bernoulli's Energy Equation B-C:

$$z_2 = \frac{V_C^2}{2g} + K_{\text{ent}} \frac{V_B^2}{2g} + K_{\text{elb}} \frac{V_B^2}{2g} + K_{\text{tee}} \frac{V_B^2}{2g} + K_{1/2} \frac{V_C^2}{2g} + f \frac{L_B}{D} \frac{V_B^2}{2g} + f \frac{L_C}{D} \frac{V_C^2}{2g}$$

$$z_2 = 11198622.15 Q_3^2 + [627,395.38 \times 2.745 \text{ m} + \frac{8 \times 0.0246 \times 9}{9\pi^2 (0.01905)^5}] Q_2^2$$

$$3 = 11198622.5 Q_3^2 + 9013819.03 Q_2^2 \quad \text{EQ 2}$$

$$Q_3 = Q_2 + Q_1 \quad \text{EQ 3}$$

Solve for flow rate:

$$Q_1 = \sqrt{\frac{4 - 11198622.5 Q_3^2}{9804549.62}} \quad Q_2 = \sqrt{\frac{3 - 11198622.5 Q_3^2}{9013819.03}}$$

Solve Q_3 by iterations: Q_3 guess: $0.5 \times 10^{-3} \text{ m}^3/\text{s}$

Iteration #3	Q_3 (m^3/s)	V (m/s)	Re	NEW #3	% diff	
5	0.02626	4.05×10^{-4}	1.15	2.16	0.02626	0.00%

Plug in Q_3 to solve Q_2 :

$$Q_2 = \sqrt{\frac{3 - 11198622.5 (4.05 \cdot 10^{-4})^2}{9013819.03}} = 1.73 \cdot 10^{-4}$$

Solve Q_1 :

$$Q_3 = Q_2 + Q_1$$

$$4.05 \times 10^{-4} = 1.73 \cdot 10^{-4} + Q_1$$

$$Q_1 = 2.32 \cdot 10^{-4}$$

$$Q_3 = 4.05 \times 10^{-4} \text{ m}^3/\text{s} \quad Q_1 = 2.32 \times 10^{-4} \text{ m}^3/\text{s}$$

$$Q_2 = 1.73 \times 10^{-4} \text{ m}^3/\text{s}$$

Check velocities to meet criteria:

$$V_A = \frac{Q}{A} = \frac{Q}{\pi(D)^2} = \frac{2.32 \times 10^{-4}}{2.85 \times 10^{-4}} = 0.814 \text{ m/s} \quad \checkmark$$

$$V_B = \frac{1.73 \times 10^{-4}}{2.85 \times 10^{-4}} = 0.607 \text{ m/s} \quad \checkmark$$

$$V_C = \frac{4.05 \times 10^{-4}}{2.85 \times 10^{-4}} = 1.42 \text{ m/s} \quad \checkmark$$

All velocities are below the V_{max} of 3 m/s

Summary:

The flow rate for pipe a is $2.32 \times 10^{-4} \text{ m}^3/\text{s}$, @ 0.814 m/s , $1.73 \times 10^{-4} \text{ m}^3/\text{s}$, and @ 0.607 m/s , $4.05 \times 10^{-4} \text{ m}^3/\text{s}$, which is the sum of $Q_2 + Q_1$. The velocities are all well below V_{max} which means that they meet the criteria.

Analysis: The lower the elevation, the slower the flow rate as is the case with pipe b. Pipe (A) has a higher flow rate due to higher elevation, I have no suggestions, as the velocities meet criteria.

② Purpose: Find the pump power required for flow configuration. Determine electrical power requirements.

Sources:

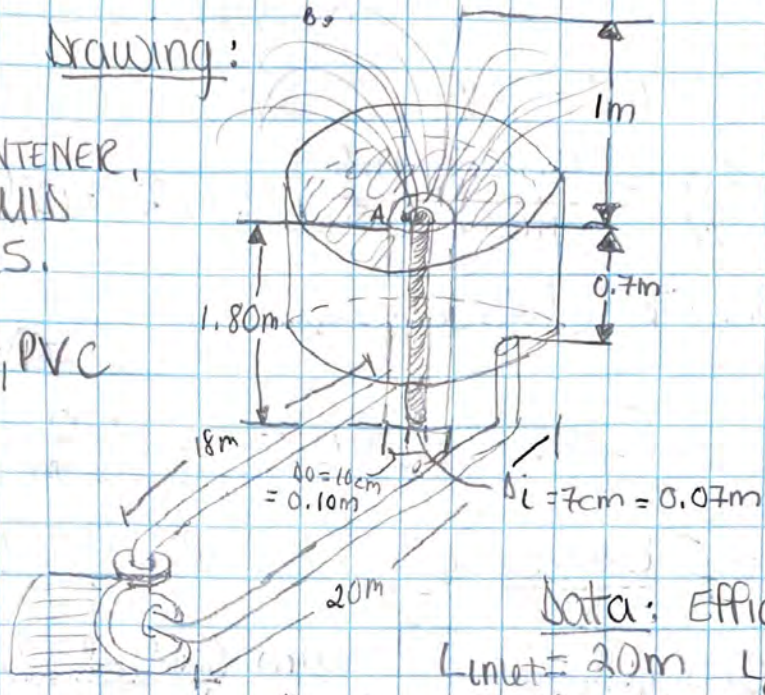
MOTT, Robert L., UNTENER, JOSEPH A., APPLIED FLUID MECHANICS, 7th, -2015.

materials: water, PVC

Design Considerations:

- ① Incompressible
- ② Isothermal
- ③ Steady state
- ④ considering all minor losses

Drawing:



Data: Efficiency $92\% = 0.92$

$L_{inlet} = 20m$ $L_{outlet} = 18m$
 $K_{ent} = 0.5$ $L = 1.80m$ $D_0 = 10cm = 0.10m$
 $K_{elb} = 30$ $K = 2$ $\Delta L = 7cm = 0.07m$
 $n_{water} = 1m$ $t = 3/2 = 1.5cm = 15mm$
 $\rho_{water} = 998 kg/m^3$
 $\epsilon = 3.0 \times 10^{-7} m$ (table 8.2)
 $V = 1.05 \times 10^{-5} m^2/s$ (table A.2)
 $V_{venturi} = 3m/s$

Calculations / Procedures:

Apply Bernoulli to ensure proper Q:

$$h_A + \frac{P_A}{\gamma} + \frac{V_A^2}{2g} + z_A = \frac{P_B}{\gamma} + \frac{V_B^2}{2g} + z_B + h_L + h_R$$

$$\frac{V_A^2}{2g} = z_B - z_A = 1m$$

$$V_A^2 = 2(9.81 m/s^2) = 19.62$$

$$V_A = 4.429 m/s \text{ (for water to reach 1m)} = 0.0177 m^3/s$$

Flow rate Q :

$$Q = VA = 4.429 m/s \cdot \left(\frac{\pi}{4} (0.10m^2 - 0.07m^2) \right)$$

PVC pipe diameters:

$$Q = \frac{\pi}{4} D^2 V \text{ rearrange to solve for } D : D = \sqrt{\frac{4Q}{\pi V}}$$

$$D = \sqrt{\frac{4(0.0177 m^3/s)}{\pi (3 m/s)}} = \sqrt{\frac{0.0708}{9.425}} = 0.08667m = 86.67mm \text{ (inside)}$$

125mm pipe is the smallest pipe I can choose based on

Req. $D_i \geq 86.67$.

Apply Bernoulli to find pump power required.

$$h_A + \frac{P_A}{\gamma} + \frac{V_A^2}{2g} + z_A = \frac{P_B}{\gamma} + \frac{V_B^2}{2g} + z_B + h_L + h_R \rightarrow \text{Simplified: } h_A = h_L$$

$$h_L = h_{pipe} + h_{annu} + h_{ent. annu.} + (4)h_{elb.} + h_{ent.}$$

$$h_{ent} = 0.5 \frac{(1.692 m/s)^2}{2(9.81)}$$

$$V = Q/A = \frac{0.0177}{1.046 \cdot 10^{-2}} = 1.692 m/s$$

$$h_{pipe} = 0.0731m$$

$$h_{elb} = \frac{L}{D} = 30 \cdot 0.1154 = 3.462$$

$$125mm D = 0.1154m$$

$$A = 1.046 \times 10^{-2} m^2$$

$$h_{ent. annu.} = 2.0 \left(\frac{(1.692)^2}{2(9.81)} \right) = 0.2918$$

Hydraulic radius for energy loss at annulus: (Fig 9.9)

$$A = \frac{\pi}{4} (\Delta^2 - d^2) \quad NP = \pi (\Delta + d) \quad R = \frac{A}{NP} = \frac{0.004}{0.5341} = 0.0075 \text{ m}$$

$$= \frac{\pi}{4} (0.10^2 - 0.07^2) = \pi (0.10 + 0.07) = 0.5341$$

(9-b) $\Delta = 4R : 4(0.0075 \text{ m}) = 0.03 \text{ m}$

$$Re = \frac{VD}{\nu} = \frac{4.429 \cdot 0.03}{1.05 \times 10^{-5} \text{ m}^2/\text{s}} = 1.27 \times 10^4 \quad \frac{D}{E} = \frac{0.03}{3.0 \times 10^{-7}} = 100,000$$

$f = 0.017$ (table 10.5)

$f = 0.017$ (table 10.5)

$$h_{\text{annulus}} = f \frac{L}{5e} \frac{V^2}{2g} = 0.017 \cdot 5 \left(\frac{1.8 \text{ m}}{0.03 \text{ m}} \frac{(4.429 \text{ m/s})^2}{2(9.81 \text{ m/s}^2)} \right) = 1.05 \text{ m}$$

$$h_{\text{pipe}} = f \frac{L + \sum Le}{D} \frac{V^2}{2g}$$

$$Re = \frac{VD}{\nu} = \frac{1.692 \cdot 0.1154}{1.05 \times 10^{-5}} = 1.8 \times 10^4$$

$$f = 0.017 \left(\frac{18 + 20 + 4 \times 3.462 \text{ m}}{0.1154 \text{ m}} \right) \frac{(1.692 \text{ m/s})^2}{2(9.81 \text{ m/s}^2)} \quad \frac{D}{E} = \frac{0.1154}{3 \times 10^{-7}} = 384,666$$

$$= 1.114 \text{ m}$$

$$\sum h_A = 1.114 \text{ m} + 1.05 \text{ m} + 0.2918 \text{ m} + 0.0731 \text{ m} = 2.5289 \text{ m}$$

Calculate pump power: $P = \rho g \cdot Q \cdot h_A$

$$= 998 \text{ kg/m}^3 \cdot 9.81 \text{ m/s}^2 \cdot 0.0177 \text{ m}^3/\text{s} \cdot 2.5289 \text{ m}$$

$$= 438.23 \text{ W}$$

Convert watts to HP:

$$0.588 \text{ HP}$$

Calculate electric power using efficiency:

$$P_{\text{electric}} = \frac{0.588}{0.92} = 0.639 \text{ HP}$$

Summary

The pump power required for the flow configuration shown is 0.588 HP. With an efficiency of 92%, the electrical power requirement is 0.639 HP.

Analysis:

The benefit of using PVC pipe is that it is generally smooth w/ a relatively low roughness factor. PVC is practical for this decorative fountain, but a bigger one with higher pressure would benefit from iron or steel fixture.