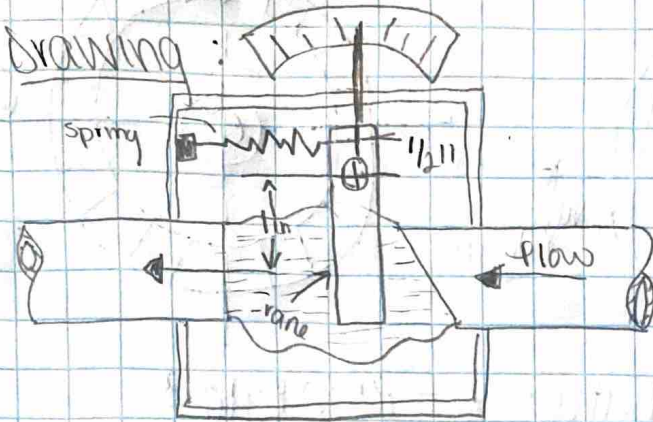


16-11 Purpose: calculate the spring force required to hold the vane in a vertical position.



Design considerations:

- ① incompressible fluid
- ② isothermal
- ③ steady state

Data: $Q = 100 \text{ gal/min} = 0.2228 \text{ ft}^3/\text{s}$
 $\text{sch. 40: } D = 1.049 \text{ in} = 0.0874 \text{ ft}$
 $A_p = 0.006 \text{ ft}^2$
 $\rho_{\text{water}} = 1.94 \text{ slug/ft}^3$

Procedure

Calculate velocity: $v = \frac{Q}{A} = \frac{0.2228 \text{ ft}^3/\text{s}}{0.006 \text{ ft}^2} = 37.133 \text{ ft/s}$

Calculate system mass flow rate: $m = \rho Q$
 $(1.94 \text{ slug/ft}^3)(0.2228 \text{ ft}^3/\text{s}) = 0.432 \text{ slug/s}$

$F_{\text{fluid}} = m \cdot \Delta v_x = (0.432 \text{ slug/s}) \cdot (37.13 \text{ ft/s}) = 16.05 \text{ lb}$

$\sum M = 0$ (about pivot point)
 $(F_{\text{fluid}} \cdot r_{\text{fluid}}) - (F_s \cdot r_s) = 0$
 $(16.05 \text{ lb} \cdot 1 \text{ in}) - (F_s \cdot 0.5 \text{ in}) = 0$

$F_{\text{spring}} = \frac{16.05 \text{ lb} \cdot 1.0 \text{ in}}{0.5 \text{ in}} =$
 $F_{\text{spring}} = \boxed{32.1 \text{ lb}}$

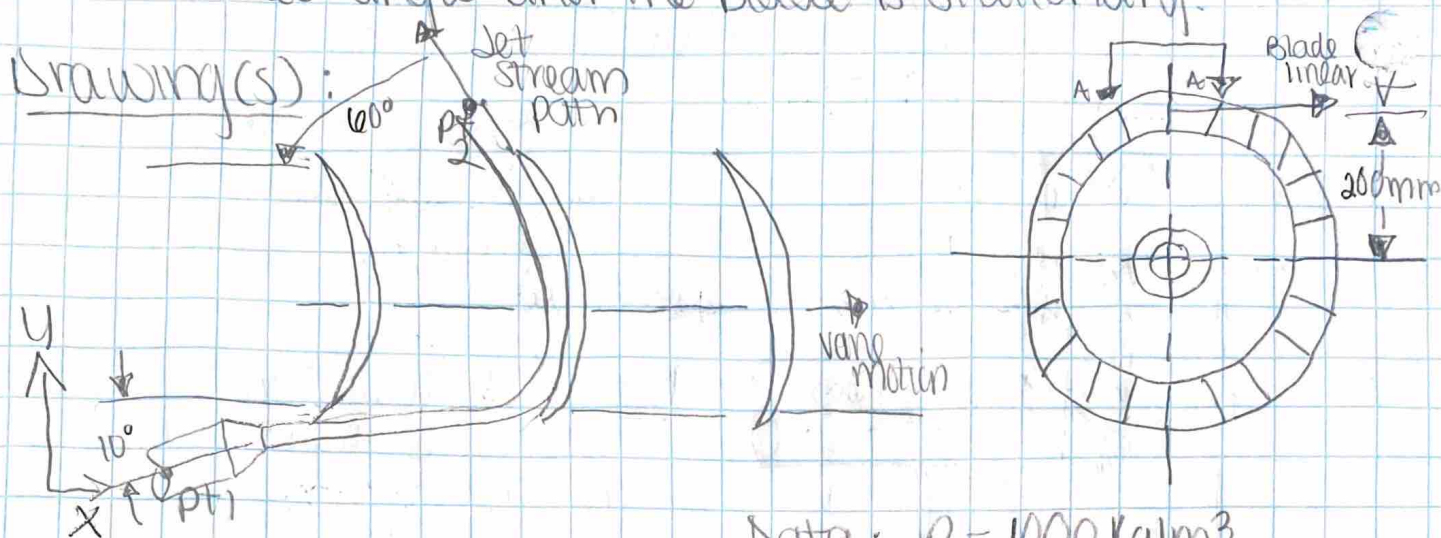
Summary: The spring force required to hold the vane in a vertical position is 32.1 lb.

Materials: water

Analysis: If the spring were to move further away from the pivot point, the lever arm would increase in efficiency and less force would be required to keep the vane vertical. The inverse is also true. The closer the spring is to the pivot point the less mechanical advantage it has and more force would be required.

16-29

Purpose: Compute the force on one blade of the turbine if the stream is deflected through 60° angle and the blade is stationary.



Design considerations:

- ① Steady state
- ② incompressible fluid
- ③ Isothermal

Data: $\rho = 1000 \text{ kg/m}^3$

$$d_{\text{jet}} = 7.5 \text{ mm} = 0.0075 \text{ m}$$

$$V = 25 \text{ m/s}$$

$$\text{Inlet } \theta = 10^\circ$$

$$\text{Outlet } \theta = 60^\circ$$

$$A_{\text{jet}} = \frac{\pi}{4} d^2 = \frac{\pi}{4} (0.0075 \text{ m})^2 = 4.418 \times 10^{-5} \text{ m}^2$$

Procedure: calculate jet area:

Calculate mass flow rate: $\dot{m} = \rho A V$

$$(1000 \text{ kg/m}^3) \cdot (4.418 \times 10^{-5}) \cdot 25 \text{ m/s} = 1.1045 \text{ kg/s}$$

Inlet:

$$V_{1x} = V \cdot \cos(10) = 25 \cdot \cos(10) = 24.62 \text{ m/s}$$

$$V_{1y} = V \cdot \sin(10) = 25 \cdot \sin(10) = 4.34 \text{ m/s}$$

Outlet:

$$V_{2x} = -V \cdot \cos(60) = -25 \cdot \cos(60) = -12.5 \text{ m/s}$$

$$-V \cdot \sin(60) = 25 \cdot \sin(60) = 21.65 \text{ m/s}$$

The force exerted on blade is equal to rate of change of momentum

$$F_x = \dot{m} \cdot (V_{1x} - V_{2x}) = 1.1045 \cdot (24.62 - (-12.5)) = \boxed{41.0 \text{ N}}$$

$$F_y = \dot{m} \cdot (V_{1y} - V_{2y}) = 1.1045 \cdot (4.34 - 21.65) = \boxed{-19.12 \text{ N}}$$

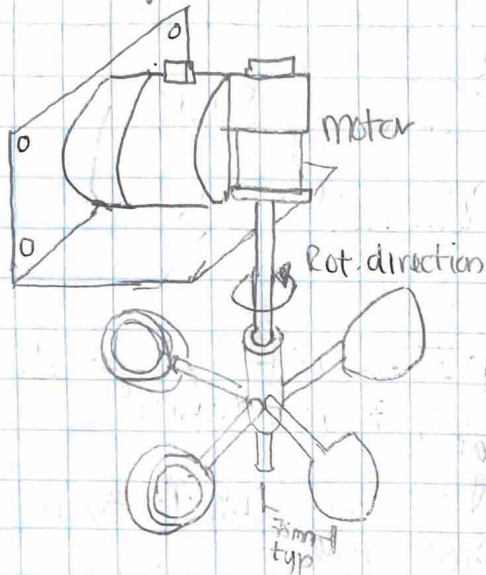
Summary: The force on one stationary blade would be 41.0 N in the x and -19.12 N in the y direction.

Material: water.

17-11 Purpose: Calculate the torque that the motor must produce to maintain motion at 20 rpm when cups are: (a) air @ 30°C (b) gas at 20°C.

Materials: air + gasoline

Drawing:



Design considerations:

- ① incompressible
- ② isothermal
- ③ steady state

Data:

$$R = 75 \text{ mm} = 0.075 \text{ m}$$

$$N = 20 \text{ rpm}$$

$$\omega = \frac{2\pi(20)}{60} = 2.094 \text{ rad/s}$$

$$V = \omega \cdot R = 2.094 \times 0.075 = 0.1571 \text{ m/s}$$

$$d_{\text{cup}} = 25 \text{ mm} = 0.025 \text{ m}$$

$$A = \frac{\pi d^2}{4} = \frac{\pi (0.025)^2}{4} = 4.909 \times 10^{-4} \text{ m}^2$$

$$\rho_{\text{air @ } 30} = 1.164 \text{ kg/m}^3$$

$$\rho_{\text{gas @ } 20} = 680 \text{ kg/m}^3$$

Procedure:

$$C_D = 1.35 \text{ (Table 17.1)}$$

4 cups acting same distance

from R:

$$T = 4(F_D \times R) = 4\left(\frac{1}{2} C_D \cdot \rho \cdot V^2 \cdot A\right) R$$

$$= 2(C_D \cdot \rho \cdot V^2 \cdot A \cdot R) = 2 \times 1.35 \times \rho \cdot (0.1571)^2 \times (4.909 \times 10^{-4}) \times 0.075$$

$$T = C_D \cdot \rho \cdot (1.815 \times 10^{-6})$$

(a) in Air @ 30°C

$$T = 1.35 \times 1.164 \times 1.815 \times 10^{-6} = \boxed{2.85 \times 10^{-6} \text{ N}\cdot\text{m}}$$

(b) gasoline @ 20°C

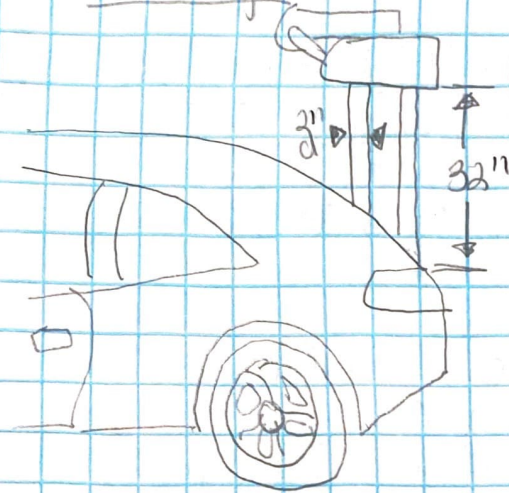
$$T = 1.35 \times 680 \times 1.815 \times 10^{-6} = \boxed{1.67 \times 10^{-3} \text{ N}\cdot\text{m}}$$

Summary: The torque that the motor must produce to maintain 20 rpm is $2.85 \times 10^{-6} \text{ N}\cdot\text{m}$ in air at 30°C and $1.67 \times 10^{-3} \text{ N}\cdot\text{m}$ in gasoline at 20°C.

17-14

Procedure: compute the drag force exerted on the car due to rods when car is travelling through still air.

Drawing:



Design considerations:

- ① incompressible
- ② isothermal
- ③ steady state

Material: air

Data:

$T = -20^\circ F$ $\rho_{air} = 2.80 \times 10^{-3} \frac{\text{slug}}{\text{ft}^3}$
 $\nu_{air} = 1.17 \times 10^{-4} \frac{\text{ft}^2}{\text{s}}$

Procedure:

calculate Reynolds number:

$$Re = \frac{V \cdot D}{\nu} = \frac{220 \text{ ft/s} \times 0.11607 \text{ ft}}{1.17 \times 10^{-4} \text{ ft}^2/\text{s}} = 3,345,3 = 3.13 \times 10^5$$

$N = 2 \text{ (rods)}$ $L_{rod} = 32 \text{ in} = 2.67 \text{ ft}$

$D_{rod} = 0.11607 \text{ ft}$

$V = 150 \text{ mph} = 220 \text{ ft/s}$

$A = 0.11607 \text{ ft} \cdot 2.67 \text{ ft} = 0.4445 \text{ ft}^2$

Determine C_D : 1.2 (Figure 7.16)

Compute drag force (F_D): $F_D = n \cdot (C_D \cdot \frac{1}{2} \rho V^2 \cdot A)$

$$F_D = 2 \cdot (1.2 \cdot (\frac{1}{2} (2.80 \times 10^{-3} \frac{\text{slug}}{\text{ft}^3}) (220 \text{ ft/s})^2 \cdot (0.4445 \text{ ft}^2))) = 2 \cdot (30,143 \text{ lb}) = 72,310 \text{ lb}$$

Summary: The drag force exerted on the car due to rods when the car is travelling through still air is 72,310 lb.