HW 1.3 02/01/2024 Angela Sicaja 22. End line FLOW Cylindar NOFE B OZ Piston moves 2014. in 155 TP 5 ft - Refrence live start Fluid reservoir oil sg = 0.9cylinder inside D = Sin t = 5sF= 11 000 lb E loss = 11.5 16-Ft/16 A cylinder = $\frac{\pi d^2}{4} = \frac{\pi (5)^2}{4} = \frac{19.641n^2}{4}$ Q = AVd) 20in . 12in) $\left(19.64 \text{ in}^2 \cdot \left(\frac{4 \text{f} \ell^2}{144 \text{in}^2}\right)\right)^*$ V = Distance time Acyl, L 2 = t 155 $a = 0.0152 \, \text{ft}^3/\text{s}$

b) $P_{cy1} = \frac{F}{A_{cy1}} = \frac{11000 \text{ lb}}{19.64 \text{ in}^2}, \left(\frac{144 \text{ in}^2}{1600 \text{ lb}}\right)$ **** Per = 80 672.3 16/ft2 c) $V_c = \frac{Q}{A_c} = \frac{0.0152 \text{ ft}^3/\text{s}}{0.000976 \text{ ft}^2} = 15.52 \text{ Ft/s}$ $v_{B} = v_{c} = 15.52 \text{ ft/s}$ $V_{D} = L = 20 \text{ in}, (1 \text{ ft}) = 0.1111 \text{ ft/s}$ Son = Sg(8H20) = 0.90(62.4 16/Ft3) $\delta ril = 56.1G Lb/ft^3$ 5 $\frac{P_{c}}{V_{oil}} + \frac{V_{c}^{2}}{2g} + \frac{V_{c}}{2g} - h_{LD} = \frac{P_{D}}{V_{oil}} + \frac{V_{D}^{2}}{2g} + \frac{V_{D}}{2g}$ $\frac{Pc}{Foil} = \frac{P_p}{Foil} + \frac{v_p^2}{29} + \frac{v_c^2}{29} - \frac{v_c^2}{29} - \frac{v_c^2}{29} + \frac{v_b^2}{29} + \frac{v_b$ $Pc = Pcy_{L} + fail \left(\frac{v_{D}^{2} - v_{c}^{2}}{2g} \right) + (2D - 2c) + h_{L}D \right]$ $P_{c} = 80\ 672.3 + 56.16 \left[\frac{0.1111^{2} - 15.52^{2}}{2(32.2)} + 10 + 35 \right]$ $P_{c} = 82.989.43.(6)ft^{2}$ ---5

d) $\frac{P_A}{F_{oil}} + \frac{v_A^2}{z_9} + z_A - h_{LS} = \frac{P_B}{F_{oil}} + \frac{v_B^2}{z_9} + z_B$ $\overline{z_A - h_{LS}} = \frac{P_R}{F_{oil}} + \frac{v_B^2}{z_g} + \overline{z_g}$ 0 0 $\frac{PB}{Foil} = \frac{z_A - h_{LS} - \frac{VB^2}{2g} - \frac{2B}{B}$ 0 $P_{B} = Foil\left[\left(2_{A} - 2_{B}\right) - \frac{V_{B}^{2}}{2g} - h_{LS}\right]$ $P_{B} = 56.16 \left[\left(-5 - 0 \right) - \frac{\left(15.52 \right)^{2}}{2(32.2)} - 11.5 \right]$ $PB = -1136.69 \text{ lb}\text{lft}^2$ e) $\frac{P_A}{S_{oil}} + \frac{v_A^2}{2g} + \frac{z_A + h_A - h_{LS} - h_{LO}}{S_{oil}} = \frac{P_O}{S_{oil}} + \frac{v_P^2}{2g} + \frac{z_P}{2g}$ 6666642d $h_A = \frac{P_{cyl}}{K_{2ll}} + \frac{v_B^2}{2g} + (z_B - z_A) + h_{LS} + h_{L\delta} \qquad P_p = P_{cyL}$ $h_{A} = \frac{30.672.3}{56.16} + \frac{(0.1111)^{2}}{2(32.2)} + (10+5) + 11.5 + 35$ 4A = 1497.97 Ft P= ha foil. 2 P= 1497.97 Ft . 56.16 16/ft 3 . 0.0152 ft 3/s P= 1274. 509 16. ft/s P= 2.317 hp

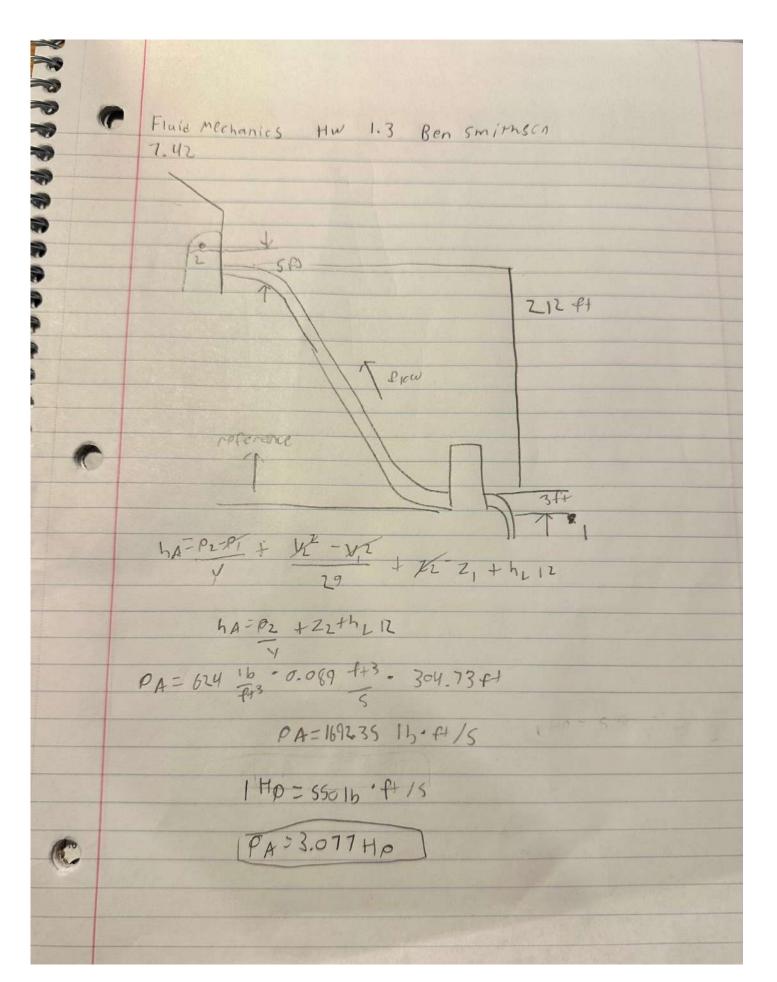
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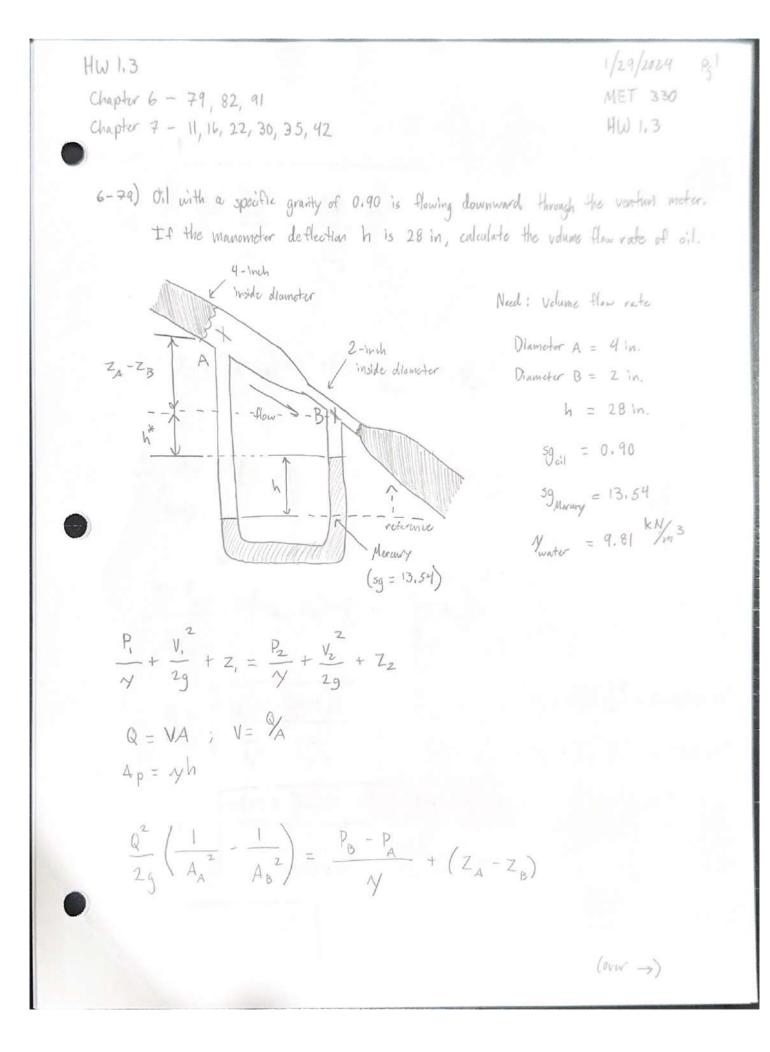
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0 Finid Mechanics Hw 1.3 Ben Smithson 7-16 Air at 82511pa 1:50 fire 00 3. reference 3m e \$ 198-DN 65 C Chedule 10 1 59 011 = 0,85 Q - 8402 / min = 0.014 m3/5 hr = 4.2 hi suction = 1.4 m bern 0allis hat 9 + 12 + 27 + 2 + 22 + 22 + Liz p = YQhA $h_{A} = \frac{p_{2} - p_{1}}{7} + \frac{1}{12} + \frac{1}{29} + \frac{1}{22} + \frac{1}{22} + \frac{1}{12} + \frac$ hA=Pz+ZzthLIZ $h_{A} = \frac{825}{7.45 - 9816N} + 14.5m + 4.2m = 117.64 m$

Power Pump P (0.85 ,9810 m3) . 0.014 m3 . 117-64 m P= 13,733 KW O ppa gage $\frac{p_{1}^{2} + v_{1}^{2}}{\sqrt{\frac{29}{29}}} + \frac{p_{3}^{2}}{\sqrt{\frac{1}{29}}} + \frac{v_{3}^{2}}{\sqrt{\frac{29}{29}}} + \frac{v$ P3 V3 = A3 - back of the book = 3.09.10 3 m2 $V_3 = \frac{0.014 \text{ m}^3/\text{s}}{3.09^{\circ} \text{h}^3 \text{m}^2} = 4.531 \text{ m}/\text{s}$ p;=(0.85, 98 10 1/2) (- (4.5315)² 2,9.81 = - 3m − 1.4m P= - 45.41 KOQ





1/24/2024 Взг мет 330 460 1.3

$$\begin{array}{l} 6-79 \\ Q = \\ \sqrt{\frac{2g(\frac{P_{B}-P_{A}}{\gamma} + (z_{A}-z_{B}))}{\frac{1}{A_{A}^{2}} - \frac{1}{A_{B}^{2}}}} \\ P_{A} + Y_{oil} \left((z_{A}-z_{B}) + h^{*} + h \right) - \gamma h - Y_{oil} h^{*} = P_{B} \\ P_{A} = P_{A} \\ \end{array}$$

.

$$\frac{P_{B} - P_{A}}{\gamma} = (Z_{A} - Z_{B}) + (1 - \frac{\gamma_{Marany}}{\gamma_{oil}})h$$

$$\frac{P_{B} - P_{A}}{\gamma_{Marany}} = (Z_{A} - Z_{B}) + (1 - \frac{59_{Marany}}{39_{oil}})h$$

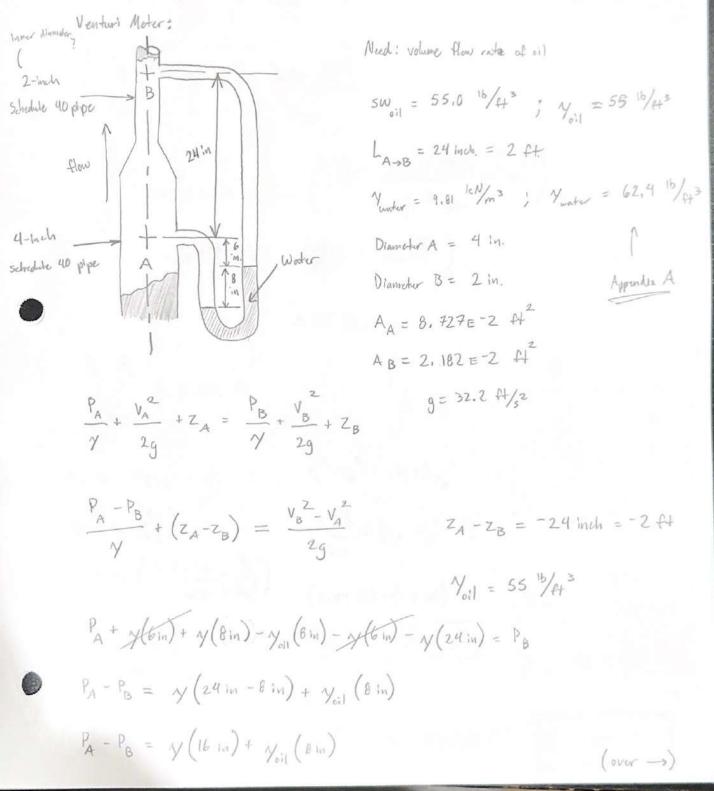
$$\therefore \ \ Q = \sqrt{\frac{2g\left(1 - \frac{59_{Muruny}}{59_{0}11}\right)h}{\frac{1}{A_{4}^{2}} - \frac{1}{A_{B}^{2}}}} \qquad \qquad A_{A} = \frac{\pi}{4} \left(\frac{4}{12}\right)^{2} = 0.6873 \ 4^{2}$$

$$A_{B} = \frac{\pi}{4} \left(\frac{z}{12}\right)^{2} = 0.6218 \ 4^{2}$$

$$Q = \int \frac{2(32.2 + \frac{1}{32})(1 - \frac{13.54}{0.90})(281n)(\frac{14}{121n})}{(0.08+3.44^2)^2} \rightarrow \int \frac{[\frac{4}{5^2}][\frac{4}{5^2}]}{[\frac{1}{5^2}][\frac{4}{5^2}]} \rightarrow \int \frac{[\frac{4}{5^2}][\frac{4}{5^2}]}{[\frac{4}{5^2}][\frac{4}{5^2}]} \rightarrow \int \frac{[\frac{4}{5^2}][\frac{4}{5^2}]}{[\frac{4}{5^2}]} \rightarrow \int \frac{[\frac{4}{5^2}][\frac{4}{5^2}]}{[\frac{4}{5^2}]}} \rightarrow \int \frac{[\frac{4}{5^2}][\frac{4}{5^2}]}{[\frac{4}{5^2}]}$$

1/24/2024 Rg 3 MET 330 HW 1.3

● 6-82) Oil with a specific weight of 55.0 ¹⁶/₁₄³ flows from A to B through the system. Calculate the volume flew rate of the oil.



1/29/2024 Bg 4 MET 330 HW 1.3

P4/S

$$\begin{array}{l} 6-22 \\ P_{A}^{-P_{B}} = Y_{oil}^{-} (16 \text{ in}) + Y_{under}^{-} (18 \text{ in}) \\ \\ \frac{P_{A}^{-P_{B}}}{Y_{oil}} = (16 \text{ in}) + \frac{Y_{under}^{-} (10 \text{ in})}{Y_{oil}} \\ = (16 \text{ in}) (\frac{144}{12\text{ km}}) + \left(\frac{(42.4 \frac{10}{2}\text{ km}^{2})(10 \text{ km})(\frac{1.44}{12\text{ km}})}{55 \frac{10}{12\text{ km}^{2}}}\right) \\ = (1.33 \text{ H}) + \left(\frac{(42.4 \frac{10}{2}\text{ km}^{2})(10 \text{ km})(\frac{1.44}{12\text{ km}^{2}})}{55 \frac{10}{12\text{ km}^{2}}}\right) \\ = (1.33 \text{ H}) + \left(0.76 \text{ H}\right) \\ \\ \frac{P_{A}^{-P_{B}}}{Y_{oil}} = 2.09 \text{ H} \\ \\ \frac{P_{A}^{-P_{B}}}{Y_{oil}} = 2.09 \text{ H} \\ \\ \frac{P_{A}^{-P_{B}}}{Y_{oil}} = 2.09 \text{ H} \\ \\ \frac{P_{A}^{-P_{B}}}{Y_{oil}} = (1.33 \text{ H}) + (0.76 \text{ H}) \\ \\ \frac{P_{A}^{-P_{B}}}{Y_{oil}} = (2.09 \text{ H}) \\ \\ \frac{P_{A}^{-P_{A}}}{Y_{oil}} = (2.$$

CARSON AND INCOMENDATION OF A DESCRIPTION OF A DESCRIPTIO

1/29/2024 P35 MET 330 HW 1,3 6-91) To what height will the jet of Phild rise for the conditions shown? Vopun to estimosphere open to 1 P= 0.0 psig N water = 9.81 KN/m3 75 mm 2,60 m Z, = 2.60 m Aluid 0.85 reference $\frac{P_{1}}{\gamma} + \frac{V_{1}^{2}}{2g} + Z_{1} = \frac{P_{2}}{\gamma} + \frac{V_{2}^{2}}{2g} + Z_{2}$ $Z_{2} = \frac{P_{1} - P_{2}}{\gamma} + \frac{\gamma_{1}^{2} - \gamma_{2}}{2g} + Z_{1}$ V, - assume negligible (large tank) $V_2 \rightarrow 0$ $Z_{2} = \frac{x_{1}^{2} - x_{2}^{2}}{x_{1}^{2}} + Z_{1}$ " Zz = Z1 Z2 = 2,60 m

$$7 - 11$$

$$No el T$$

$$Air Hopsig Q = 745 gol/h$$

$$Storage tank = \frac{1in - 5chudulle 40 pipe}{h_{L} = 10.5 lb - ft / lb}$$

$$h_{L} = 10.5 lb - ft / lb$$

$$h_{L} = 10.5 lb - ft / lb / ft^{3}$$

$$A = 0.0006 ft^{2}$$

$$U = \frac{745 gol}{h_{L}} \left(\frac{11}{600 yir}\right) \left(\frac{116t^{2}}{605 y}\right) \left(\frac{116t^{2}}{7.4 k got}\right)$$

$$N = 4.6 lf f / 5$$

$$h_{L} = \frac{72}{7 k} + \frac{2}{2} + h_{L}$$

$$= \frac{400 psi h}{7 k (k)} \left(\frac{1}{10 k}\right)$$

$$h_{L} = 10.5 kb - ft / lb$$

$$h_{L} = 1 hp$$

$$l_{Primp} = \frac{h_{tot} t}{lop t}$$

$$st + lb - \frac{1}{lb} = 0.7068 hp$$

$$= \frac{0.7068 hp}{l hp} = 0.7068$$

$$l_{L} hp$$

$$H_{Primp} = 0.7068$$

1.110

$$\begin{array}{c}
\left(5 - 82 \right) \\
\left(5 - 82 \right) \\
\left(7 + 82 \right)$$

$$6-82 \qquad \text{Moel} \quad T \qquad \frac{42}{2}$$

$$A_{A} \sqrt{A} = A_{B} \sqrt{B} \qquad A_{A} = (2.57)\pi^{2} \left(\frac{124}{12}\right)^{2} = 0.06$$

$$\sqrt{B} = \frac{A_{A} \sqrt{A}}{A_{B}} \qquad A_{B} = 3.14 \text{ in}^{2}$$

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$$\sqrt{A} = \frac{A_{B} \sqrt{A}}{A_{B}} \qquad A_{B$$



4444444422 1 7.30) T= 60°F 1 Q = 1000 901/min 165 Ft Nw = 62.4 18 -A= 0.3472 ft2 -2 Ret -5 Flow $h_{A} + \frac{1}{5} + \frac{1}{25} + \frac{1}{21} = \frac{1}{5} + \frac{1}{25} + \frac{1$ 2 -1.843E-36P=15 $\frac{P_{R} - h_{R} \vee Q}{P_{R} - \frac{37h_{P}}{8Q} - \frac{20076}{(62.4\frac{11}{P_{P}})} \left(\frac{1000941}{(62.4\frac{11}{P_{P}})} - \frac{144.316}{(62.4\frac{11}{P_{P}})} - \frac{144.316}{16}\right)$ --5 -5 4 4 4 4 $Q = VA \rightarrow V = \frac{Q}{A} = \frac{2.23}{5} = 6.42 \frac{f+3}{5}$ $h_{L} = -\frac{V_{2}^{2}}{25} - h_{R} + 2_{1} = \frac{6.42^{2}}{2(32.2)} - 144.3 + 1(5 = 21.34)$ --> VGIVE -3 $h_{L} = \frac{V^{2}}{29} \qquad \begin{array}{c} f_{T} = \\ k = 8f_{T} = 8(0.014) \\ \hline \\ h_{L} = (0.112) \\ \hline \\ 2x32.2 \end{array} \qquad \begin{array}{c} f_{T} = \\ k = 0.112 \\ \hline \\ k = 0.112 \end{array}$ Ft= 0.014 (from slides) 2 -7 0 h= 0.011165 Total: 1 = 21.35 18 ft -3 -3 -

HW 1.3 REFLECTION PARAGRAPH

This week we have learned about the formula for inclined surfaces, and force acting on a submerged curved surface. In one of the problems in the video lecture, we saw that for the decomposed surfaces we have to split them into two parts. Vertical which is equal to weight W, and Horizontal which is equal to the projected area that computes it. Furthermore, we went over on how to obtain the location of the weight for the Vertical surfaces. We just use the centroid of the volume in this case. One of the problems we did had a connection with the force on a curbed surface with fluid below it. We talked about buoyancy and pressure and said that the center of buoyancy is the center of displaced volume. Lastly, the condition for stability of bodies completely submerged in a fluid is that the center of gravity of the body must be below the center of buoyancy.

$$\begin{array}{c} 1/3 \\ 3 \text{ relative} & 1/3 \\ 10 \text{ relative} &$$

$$Z = 3$$

$$\frac{p_{2}}{b} + \frac{y_{1}^{2}}{z_{2}^{2}} + \frac{y_{2}^{2}}{z_{2}^{2}} + h_{A} = \frac{p_{3}}{b} + \frac{y_{3}^{2}}{z_{3}^{2}} + \frac{y_{4}^{2}}{z_{3}^{2}} + \frac{y_{4}^{2}}{z_{3}^{2}}$$

 $h_{R} = \frac{P_{4} - P_{5}}{F} + z_{4} - z_{5}$ = 37,882.49 16/542 - 145.08 10/542 2 8+ 58.032 16/5+3 hr= 652.3 A PR = (58.032 10/57) (0,39-543/5) (652:3-5+) PR = 14152.1 16. 54/5 $P_R = 25.7hP$