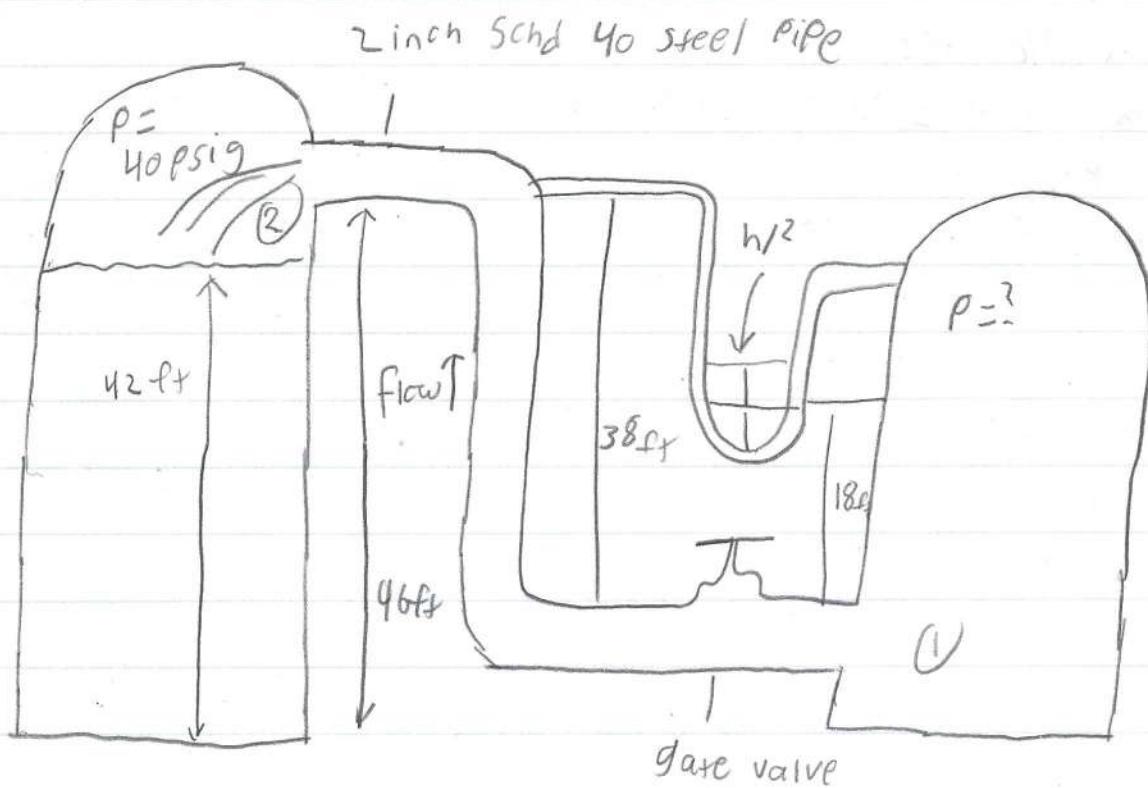


# Ben Smithson Fluid mechanics test 2

## Part A

Purpose: Determine the force magnitude through the pipe system, then calculate the horizontal and vertical forces for the system to be supported. Also, check the pressure drop out of the nozzle and factor in the effect of a water hammer.

Diagram:



Sources: Applied Fluid Mechanics Eighth edition  
Mott, Vansteener.

## Design considerations:

- 1) Incompressible fluids
- 2) Static fluid
- 3) System is horizontal and vertical
- 4) Minor losses

Data 3 variables

Schedule 40 pipe

blind flange = 2 inch diameter

150 rpm

water temp is  $77^{\circ}\text{F}$

## Materials:

water

ethyl alcohol

steel pipe.

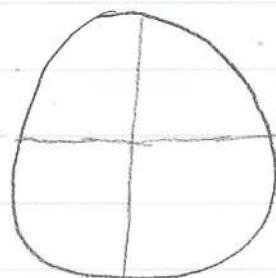
# Ben Smithson Fluid mechanics test 2

Procedure: First, I will draw the diagram. Then, find the points on the diagram in order to see pressure. Next, using static flow of liquids I will find the force magnitude at the blind flange. After that, I will continue to use static flow of liquids to determine the horizontal & vertical forces required to support the system. In the last steps I will use the general energy equation to calculate pressure drop out of the nozzle. Finally, using equation 11-9 I can find the effect of the water hammer on the system to see if there will be damage.

Calculations:

Part A

#1



blind flange  $d = 0.166 \text{ ft}$

$$A = \frac{\pi D^2}{4} = \frac{\pi (0.166)^2}{4} = 0.0216 \text{ ft}^2$$

$$F = A \cdot \rho \cdot P$$

F = pressure @ 150 gpm

& already carinated

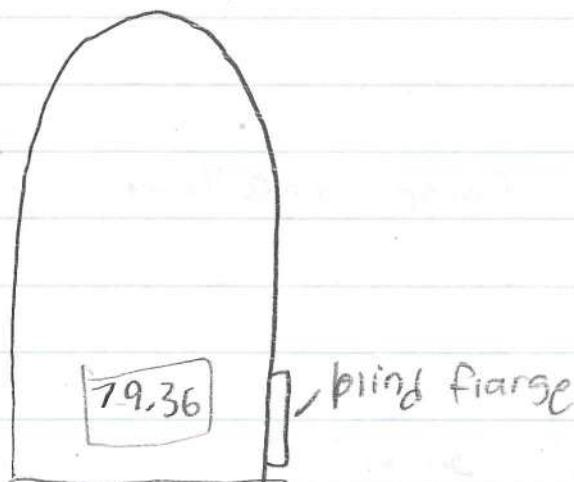
$$= 77 \text{ psi}$$

$$\Delta P = Y \cdot h$$

$$P + \varphi = P_{\text{atm}} + \gamma_{\text{ethyl}} \cdot Y_{\text{water}}$$

$$P_0 = 40 \text{ psi} + 0.787 \cdot 9.81 = 47.72$$

$$F = 77.2 \cdot 47.72 \cdot 0.0216 \text{ ft}^2 = 79.36$$



# Fluids test 2 Ben Smithson

Part A

2. Pressure in Second tank

$$p_1 = p_2 + \gamma (z_1 - z_2 + \frac{V_2^2}{2g}) + hL$$

$$Q = V \cdot A \quad V = \frac{Q}{A}$$

$$A = \frac{\pi}{4} D^2 = \frac{\pi}{4} (0.172)^2 = 0.0232 \text{ ft}^2$$

$$Q = 150 \text{ gpm} = 0.4013 \text{ ft}^3/\text{s}$$

$$V = \frac{0.4013}{0.0232} = 17.29 \text{ ft/s}$$

$$Re = \frac{\rho V D}{\mu} = \frac{\rho D}{\eta}$$

$$Re = \frac{17.29 \text{ ft/s} \cdot 0.172 \text{ ft}}{1.37 \cdot 10^{-5}} = 2.1707 \cdot 10^5$$

$$\frac{D}{e} = \frac{0.172}{1.5 \cdot 10^{-4}} = 1.146 e^{-5} = 1146$$

$$f = \frac{0.25}{\left[ \log \frac{1}{1146} + \left( \frac{5.74}{(2.17 \cdot 10^5)^{0.9}} \right) \right]^2} = 0.0267$$

$$h_L \text{ pipes} = f \cdot \frac{L}{D} \cdot \frac{V^2}{2g}$$

$$= 0.0267 \cdot \frac{110}{0.1724} \cdot \frac{17.29^2}{2 \cdot 32.2} = 79.26$$

$$h_{\text{head}} = k \frac{V^2}{2g} \quad k = 20 \text{ ft}$$

$$= 20(0.0267) \frac{17.29^2}{2 \cdot 32.2} = 2.47 \cdot 2 = 4.94$$

$$h_L \text{ gate } V = k \frac{V^2}{2g}$$

$$= 8(0.0267) \frac{17.29^2}{2 \cdot 32.2} = 0.99 \text{ ft}$$

$$h_L \text{ total} = 89.21 \text{ ft}$$

$$P_1 = P_2 + \gamma (z_1 - z_2 + \frac{V_2^2}{2g}) + h_L$$

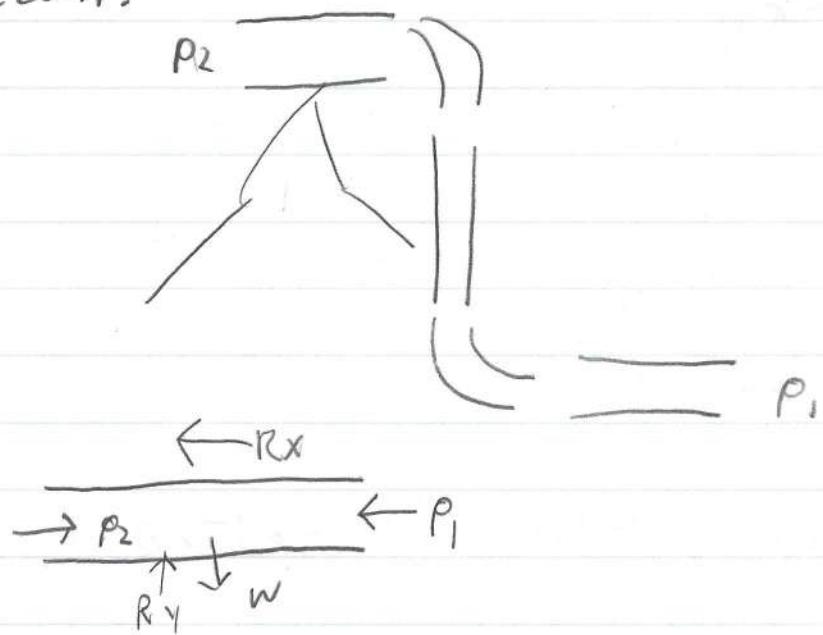
$$\rho_1 = 5760.16 \text{ lb/ft}^3 + 49.01 \left( (38 - 18) + \frac{(17.29^2)}{2 \cdot 32.2} + 89.21 \text{ ft} \right)$$

$$\rho_1 = 11143.84 \text{ lb/ft}^3 = 77.38 \text{ psi}$$

Ben Smithson

Part A

2 cont.



$$R_x = \frac{P_1 - P_2}{A} = \frac{77 - 40}{0.0232 \cdot 12} = 132.9$$

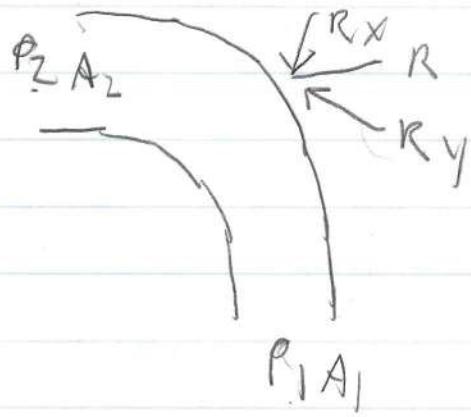
$$R_y = w$$

Specific weight,  $\gamma$  (lb/cu ft)

$$\gamma = w/V$$

$$w = \gamma \cdot V$$

$$w = 62.4 \cdot 17.29 = 847.38 = R_y$$



$$R_x = p_1 A_1 + \rho g V_1$$

$$R_x = 11143.84 \cdot 0.0232 + 1.53 = 0.4013 + 17.29$$

$$R_x = \boxed{17.6915}$$

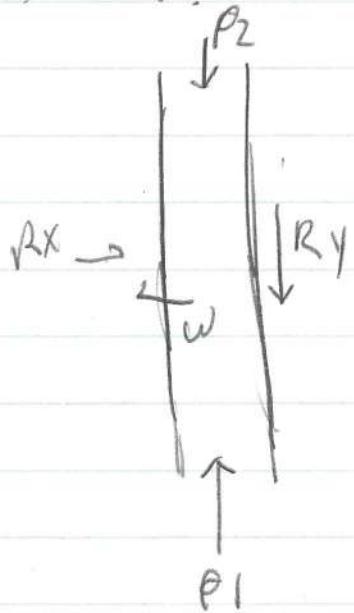
$$R_y = \rho g V_2 + w + p_2 A_2$$

$$11143.84 \cdot 0.4013 + 17.29 + 5760 - 0.0232 + 847.88$$

$$R_y = \boxed{1457.32}$$

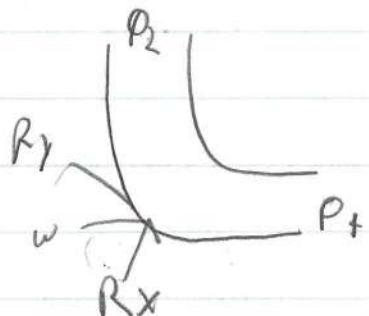
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2. cont.



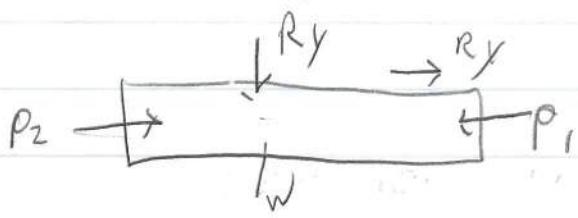
$$R_x = \frac{w}{A}$$
$$= 847.38$$

$$R_y = \frac{P_1 - P_2}{A} = \frac{77 - 40}{0.0232 \cdot 12} = 132.9$$



$$R_x = P_1 A_1 + P_2 V_2 = 269.19$$

$$R_y = P_2 V_2 + w + P_1 A_2 = 1457.32$$



$$R_{xz} = \frac{P_1 - P_2}{A} = 132.9$$

$$R_y = w = 847.39$$

$$R_x \text{ total} = 1651.48$$

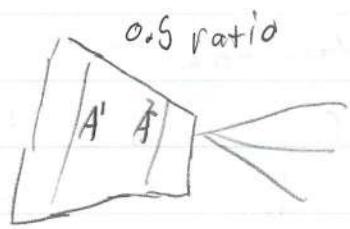
$$R_y \text{ total} = 4742.3$$

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3. given  $\beta = 0.5$

flow nozzle from notes

$$C = 0.9975 - 6.53 \sqrt{B/NR}$$



$$Re = \frac{\rho V D}{\mu} = \frac{\rho D}{\nu}$$

$$V = \frac{Q}{A} = Q = 150 \text{ gpm} = 0.401 \text{ ft}^3/\text{s}$$

$$A = \frac{\pi}{4} D^2 = \frac{\pi}{4} (0.172)^2 = 0.0232 \text{ ft}^2$$

$$V = \frac{0.401}{0.0232} = 17.28 \text{ ft/s}$$

$$Re = \frac{17.28 \cdot 0.172}{1.37 \cdot 10^{-5}} = 216945.98 \quad \text{- Appendix}$$

$$C = 0.9975 - 6.53 \sqrt{0.5 / 216945.98}$$

$$C = 0.9875$$

$$V_1 = C \sqrt{\frac{2g(p_1 - p_2) / \gamma}{(A_1 / A_2)^2 - 1}}$$

$$17.28 = 0.9875 \sqrt{\frac{(2 \cdot 32.2)(p_1 - p_2) / 49.01}{(0.172 / (0.172/2))^2 - 1}}$$

$$p_1 - p_2 = 699.09 \text{ lb}_f \text{ ft}^2 = 4.85 \text{ psi}$$

#### 4. Water hammer



$$C = \sqrt{\frac{E_0 / P}{1 + \frac{E_0 D}{E g}}}$$

2 inch Schedule 40 pipe  
thickness = 0.154 inch = 0.183 in  
Appendix F

$$C = \sqrt{\frac{130,000 \text{ psi}}{1.93 \text{ slug/l ft}^3}} > \text{ethyl alcohol}$$

$$\sqrt{1 + \frac{130,000 \text{ psi} \cdot 0.172}{200 \text{ gpa} \cdot 0.0154 \text{ in}}}$$

$$C = \sqrt{\frac{187,200,000}{1,053}}$$

$$\sqrt{1 + \frac{187,200 \cdot 0.172}{4,177,086.894 \cdot 0.1283}} = 357.16 \text{ ft/s}$$

$$\Delta P = P(CV) = (1.53)(33.97.33)(17.28) = 89,819.97 \text{ lb/ft}^3$$

$$P_{\max} = \rho_0 P + \Delta P = 777.38 \text{ psi} + 89,819.97 \text{ lb/ft}^3$$

$$= 91,143.84 + 89,819.97 \text{ lb/ft}^3 = 180,963.83 \text{ lb/ft}^3 = 101.12 \text{ psi}$$

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4 cont.

Pg 282

basic wall thickness calculation

$$t = \frac{P_D}{2(\sigma_E + \gamma Y)}$$

$$\sigma_{\text{design press}} = 701.1 \text{ psi}$$

D pipe outside diameter = 2.375 in (Appendix pg 494)

S allowable stress intension = 1371 psi (engineering toolbox)

E longitudinal joint quality factor = 0.85 (pg 282 welded)

Y correction factor (temp & type) = 0.4 (Pg 282)

$$t = \frac{701.1^3 (2.375)}{2((1371 \cdot 0.85) + (701.1 \cdot 0.4))} = 0.63 \text{ in}$$

Pipe will fail because 0.63 in > 0.154 in (pipe thickness)

cavitation

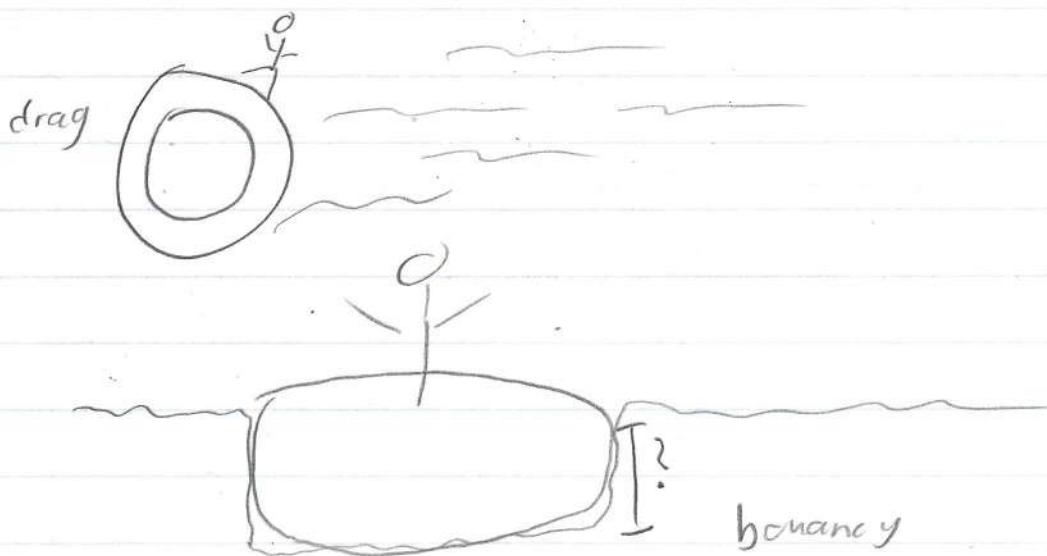
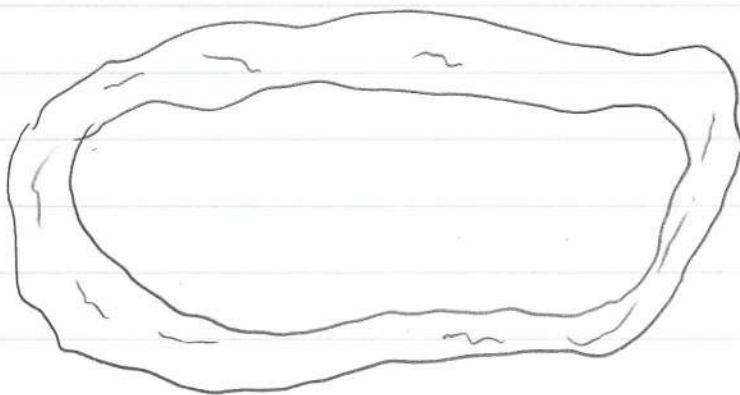
$$\frac{P_S}{\gamma} = \frac{P_0}{\gamma} - \frac{\Delta z - \frac{V_s^2}{2g}}{\gamma} - h_L - s$$

# Ben Smithson Fluid mechanics Test 2

## Part B:

Purpose: The purpose of this question is to design a lazy river that can show the flow rate, be stable, and have a reasonable drag force on individuals riding it.

## Diagrams:



Sources: mott & utlener, Applied Fluid Mechanics  
8th edition

Design considerations:

220 lb. person is floating

4 year old = 0.1% slope

water is flowing

Data } variables

220 lb (buoyancy)

0.1% slope

flow rate

static forces

Material

- water running out a nozzle to push

individuals

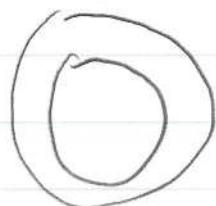
- pool float

## Ben Smithson fluid mechanics test 2

procedures First, using  $Q = VA$  I will find the required flow rate to push a 4 year old. Next, I will use drag force equation to see what drag the kid will feel while going around the lazy river. Finally using buoyancy I can see if the river will be stable with a 220lb person riding.

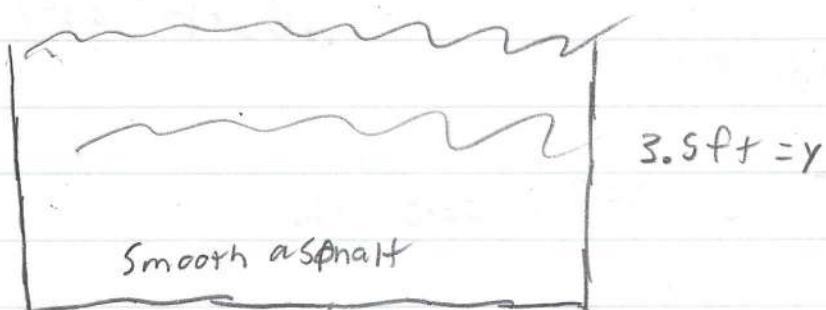
calculations:

5.



← waterpark tube width = 42 inches

$2 \cdot 42 = 84$  inches  $\rightarrow$  96 inches to be safe or 8ft wide  
depth about 3.5ft deep



$$8\text{ft} = b$$

$$A = by = 8 \cdot 3.5 = \underline{28\text{ft}^2}$$

$$R = \frac{by}{b+2y} = 1.866\text{ ft}$$

$$WP = b+2y = \underline{15\text{ft}}$$

5. cont.

Slope = 0.1%

Smooth asphalt  $N = 0.013$  Table 14.1

$$Q = \left(\frac{1.00}{N}\right) AR^{2/3} S^{1/2}$$

$$Q = \left(\frac{1.00}{0.013}\right)(28)(1.86)^{2/3} 0.001^{1/2}$$

$$Q = \boxed{103.012 \text{ ft}^2/\text{s}}$$

6.



$$A = \frac{\pi D^2}{4} = \frac{\pi \cdot 1^2}{4} = 0.785$$

Water @  $70^\circ\text{F}$  or  $50^\circ\text{C}$

$$NR = \frac{VD^2}{VJ}$$

$$J = 1.05 \cdot 10^{-5} \text{ ft}^2/\text{s} \quad (\text{A.2})$$

$$J = \frac{Q}{A} = \frac{103.12}{28} = 3.679 \text{ ft}^2/\text{s}$$

$$NR = \frac{3.679 \cdot 1}{1.05 \cdot 10^{-5}} = 350382.69 = 3.50 \cdot 10^5$$

$CD = 0.8$  based off graph

page 433

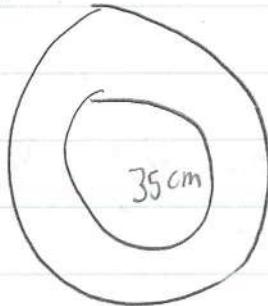
$$FD = CD \left( \frac{\rho V^2}{2} \right) A = 0.8 \cdot \left( \frac{1.94 \cdot 3.679^2}{2} \right) 0.785$$

$$\boxed{FD = 8.24}$$

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Part B

7.



$$w = 224.09 \text{ lbs} \quad \begin{matrix} \uparrow \\ \text{with guy and tube} \end{matrix}$$

2 kg weight  $\approx 4.409 \text{ lbs}$

$3.14 \text{ ft}$   $1.14 \text{ ft}$   $\rightarrow$  diameters

Volume hollow cylinder

$$V = \pi (R^2 - r^2) h$$

$$\begin{aligned} w &= y_B V \\ 224.09 &= 62.3 (V) \\ V &= 3.596 \end{aligned}$$

$$3.596 = \pi (1.97^2 - 0.97^2) h$$

$$h = 0.635 \text{ ft}$$



Stability

$$M_B = I / V_d$$

$$I = \frac{\pi (D^4)}{64} \rightarrow \text{hollow} \quad \frac{\pi (D^4 - d^4)}{64} = \frac{\pi (3.14^4 - 1.14^4)}{64}$$

$$I = 4.688$$

$$M_B = \frac{4.688}{3.596} = 1.303 \text{ ft}$$

7 cont.

$$Y_{MC} = Y_{CB} + \frac{M}{B}$$

$$Y_{CB} = \text{half of draft (fig 9.13 pg 105)} = Y_2 (0.535)$$

$$Y_{CB} = 0.2675$$

$$Y_{MC} = 0.2675 + 1.303 = \boxed{1.5748}$$

$$Y_{CG} = Y_2 (0.535) = 0.2675$$

$$Y_{MC} > Y_{CG}$$

- ∴ The tube + person are stable because the metacenter is above the center of gravity.

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Summary

Part A

The pipe system with the blind flange can occur with the location on the end. with the system for the civil engineers, they will have to hold up a decent amount of weight. Also, the pressure drop in the nozzle is significant by the water hammer could damage the system.

Part B.

The tube for the water park should be able to handle two rafts at a small flow rate with the drag force not being too significant. Also, the 220 lb man would have a stable raft in the lazy river.

Analysis:

part A. overall the system would most likely fail under a water hammer by with the weight of the system it may be unfeasible to spend money on.

Part B

The lazy river is able to have a flow  
of just over 100 ft/s by the drag force  
on a lid is 8.2N the 220 lb man is  
stable as well so overall the system is  
a success.