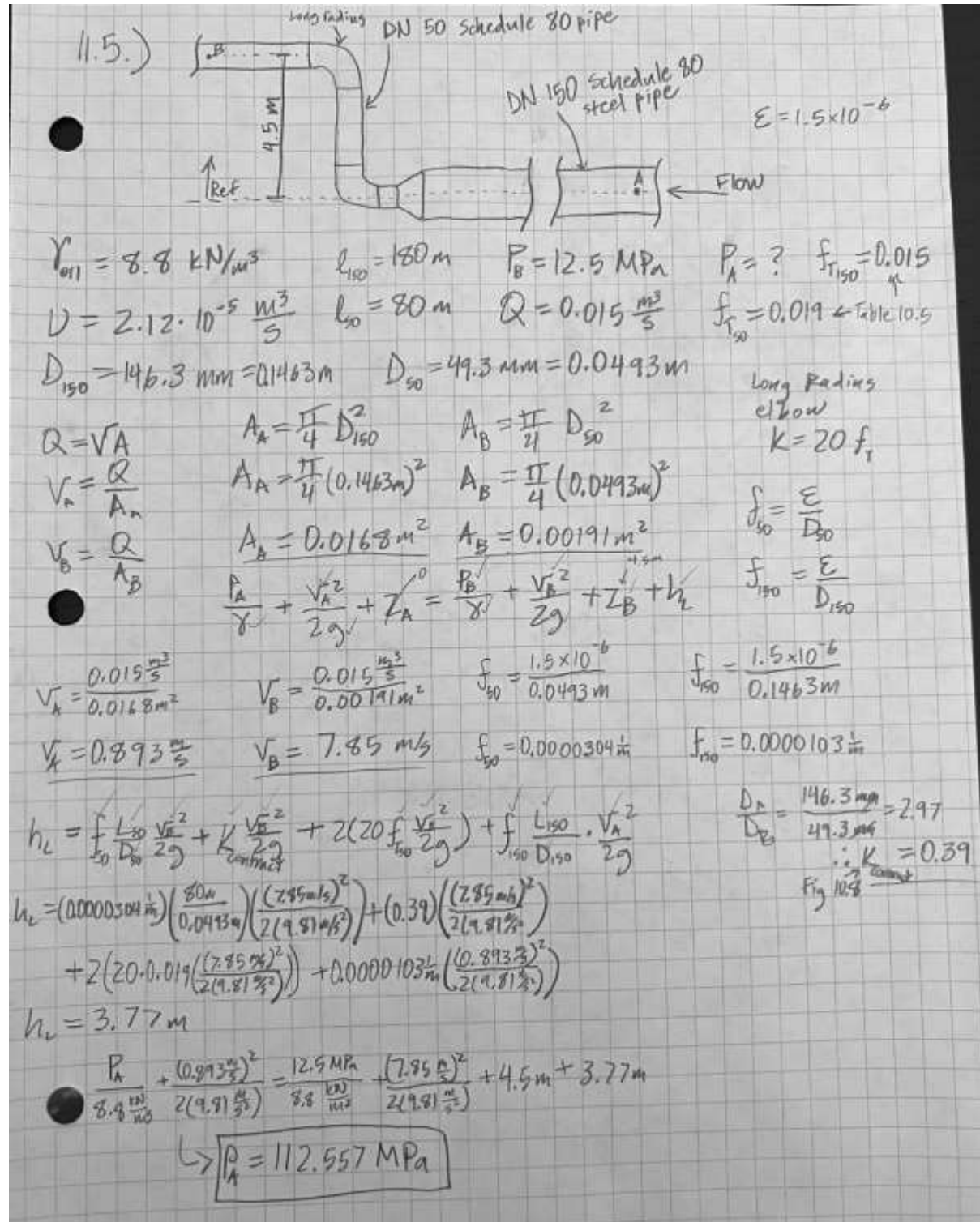


11.5



11.13

input data								
specific weight	62	lb/ft ³		For 20 psi				
kinematic viscosity	0.00000737	ft ² /s		Iteration	V (ft/s)	Re	f	RHS (m)
pressure A (80 psi)	11520	lb/ft ²		1	45	127204.9	0.028706	62.15937
pressure A (20 psi)	2880	lb/ft ²		2	45.9	129749	0.028686	64.67061
Pressure B	0	lb/ft ²		3	40	113071	0.028829	49.11359
Z_B	18	ft		4	30	84803.26	0.029184	27.6264
Tube Length	20	ft		5	32.44	91700.59	0.029079	32.30305
diameter_1	0.04166667	ft		6	31	87630.03	0.029139	29.49886
diameter_2	0.02083333	ft		7	30.5	86216.64	0.029161	28.55496
Wall Roughness	0.00015	ft		8	30.44	86047.04	0.029164	28.44272
Computable Data				for 80 psi				
Relative roughness (D/e)=	277.777778			Iteration	V (ft/s)	Re	f	RHS (m)
fT=	0.02755873			1	12	33921.3	0.031047	4.420233
K opening=	0.15			2	50	141338.8	0.028606	76.73996
K elbows=	0.82676178			3	40	113071	0.028829	49.11359
LHS (20 psi)=	28.4516129	ft		4	70	197874.3	0.028339	150.4103
LHS (80 psi)=	203.806452	ft		4	80	226142	0.028253	196.4542
				5	81	228968.8	0.028245	201.3963
				6	75	212008.1	0.028293	172.6649
				7	73.9	208898.7	0.028303	167.6372
				8	81.44	230212.6	0.028242	203.5902

11.20

P 11.20

Schedule 40 steel

$P_{\text{atm}} = 80 \text{ psig}$ $P_{\text{atm}} = 60 \text{ psig}$

$Q = 0.50 \text{ ft}^3/\text{s} @ 60^\circ\text{F}$

→ find diam of pipe

Wall thickness = 0.000150 ft

$V = 62.4 \text{ lb/ft}^3$ $\rho = 1.21 \times 10^{-2} \text{ lb/ft}^3$

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_{L_{1-2}}$$

$$h_L = f \frac{L}{D} \frac{V^2}{2g} \quad h_L = \frac{PVD}{\mu} = \frac{VD}{\gamma}$$

D/L (Reynolds) $V = \frac{4Q}{\pi D^2}$

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_{L_{1-2}}$$

$$\frac{P_1}{\gamma} = \frac{P_2}{\gamma} + z_2 + h_{L_{1-2}}$$

$$\frac{P_1 - P_2}{\gamma} - z_2 = h_{L_{1-2}} = f \frac{L}{D} \frac{V^2}{2g}$$

$$\frac{P_1 - P_2}{\gamma} - z_2 = f \frac{L}{D} \frac{16Q^2}{\pi^2 D^5} \Leftrightarrow \frac{f L 16 Q^2}{2g \pi^2 D^5}$$

→ Solve for D:

$$D = \sqrt[5]{\frac{f L 16 Q^2}{2g \pi^2 \left(\frac{P_1 - P_2}{\gamma} - z_2 \right)}}$$

Using excel:

- guess f
- calc D from f
- calc Re and Q/L
- Rec f again
- compare f_{old} and f_{new}

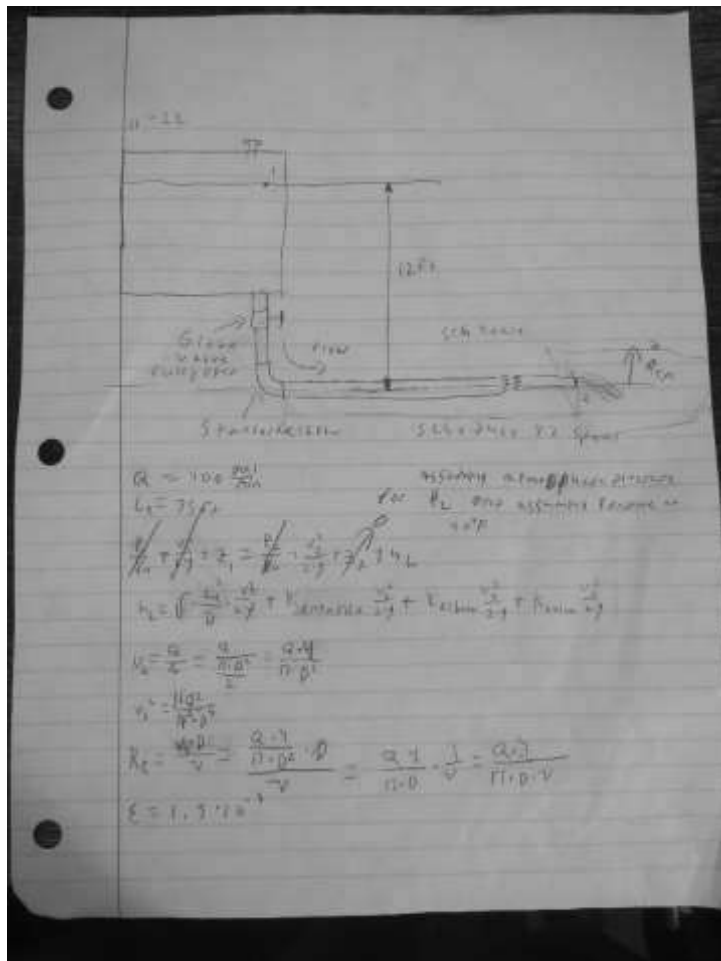
$$f = \frac{0.25}{\left[\log \left(\frac{2.5}{Re} + \frac{0.00015}{Re^{1/4}} \right) \right]^2}$$

Final Answer:

Gamma	62.4 lb/ft ³		Top	18.39057	Bot.	21.15385
Visc	1.21E-05 ft ² /s			11.03434		21.15385
PA	80 psig	11520 lb/ft ²		7.356227		21.15385
PB	60 psig	8640 lb/ft ²		3.678113		21.15385
ZB	25 ft			9.195284		
L	600 ft	Delta P	2880	8.09185		
Q	0.5 ft ³ /s			9.162181		
e	0.00015 ft					
g	32.2 ft/s ²					

Iteration	f	D	V	Re	D/e	f(new)	%diff
1	0.05	0.972392		5.41E+04	6482.61	2.38E-02	52.47421725
2	0.03	0.877953		6.00E+04	5853.022	2.44E-02	18.57799204
3	0.02	0.809568		6.50E+04	5397.118	2.50E-02	-24.86708559
4	0.01	0.70477		7.47E+04	4698.464	2.60E-02	-159.5167258
5	0.025	0.846516		6.22E+04	5643.44	2.47E-02	1.319047597
6	0.022	0.825148		6.38E+04	5500.985	2.48E-02	-12.92382639
7	0.02491	0.845906		6.22E+04	5639.371	2.47E-02	0.943018233

11.22



$$f = \frac{0.25}{\log\left(\frac{1}{1.5}\right)} + \frac{(0.25)^2}{0.001} \quad \text{Kantabir} = 0.25$$

$$f_s = \frac{0.25}{\log\left(\frac{1}{1.5}\right)}$$

$$Z_1 = \frac{1}{2} \cdot \frac{0.25}{0.001} + \frac{f_s}{0.001} \cdot \frac{0.25}{0.001} + \frac{f_s}{0.001} \cdot \frac{0.25}{0.001} + \frac{f_s}{0.001} \cdot \frac{0.25}{0.001} + \frac{f_s}{0.001} \cdot \frac{0.25}{0.001}$$

$$Z_2 = (1 + f_s \cdot \frac{0.25}{0.001} + 0.5 \cdot f_s) \cdot \frac{0.25}{0.001} + \frac{f_s}{0.001} \cdot \frac{0.25}{0.001}$$

4.25 iteration

0.3 gaussian 0.0.0

$\rho = 0.275 \text{ ft}$

z1	12 ft										
Q	400 gal/min	0.890868597	ft/s								
RHS1	1										
RHS3	0.5										
u	1.67E-05 ft/s										
e	1.50E-04 ft										
LHS	12 ft										
Le	75 ft										
Iteration	D	F	Ft	Re	RHS2	RHS4	RHS5	RHS6	RHS	%diff	
1	0.5	8.875617	0.01493702	4.537157	1331.342596	0.448110602	5.078586827	0.319655	427.8166	3465%	
2	0.2	6.910428	0.018329405	11.34289	2591.410658	0.549882138	6.231997563	12.48653	32461.13	270409%	
3	1	1.29675	0.012959657	2.268578	97.40628449	0.388789703	4.406283304	0.019978	2.071792	-83%	
4	0.6	4.373506	0.014375183	3.780964	546.6882334	0.431255494	4.88756227	0.154155	65.32569	611%	
5	0.9	1.561742	0.013233966	2.520643	131.811798	0.397018987	4.49954852	0.03045	4.208487	-65%	
6	0.8	2.023156	0.013551056	2.835723	189.6708578	0.406531676	4.607358991	0.048775	9.969009	-20%	
7	0.7	2.790145	0.013924523	3.240826	298.9441591	0.417735701	4.734337941	0.063209	25.42831	112%	
8	0.75	2.348046	0.013729659	3.024771	234.8046093	0.411889785	4.66808423	0.063142	15.24145	27%	
9	0.76	2.275278	0.013692718	2.984971	224.5339907	0.410781537	4.655524081	0.059864	13.8391	15%	
10	0.77	2.206728	0.013656405	2.946206	214.9409916	0.409682155	4.643177759	0.056833	12.58811	5%	
11	0.78	2.142056	0.013620703	2.908434	205.966884	0.408621075	4.631038852	0.053974	11.46979	-4%	
12	0.775	2.173927	0.013638479	2.927198	210.3799933	0.409154362	4.637082768	0.05538	12.01343	0%	

11.23

11.23) $h_A = \Delta h_L = h_1 + h_2 + h_3 + h_4 + h_5 + h_6 + h_7$

Labels: h_1 (EXPANSION), h_2 (FRICTION), h_3 (FRICTION), h_4 (FRICTION), h_5 (FRICTION), h_6 (DELIVERY), h_7 (EXIT LOSS)

SWINE ENGINE VAL.

DELIVERY PIPE VAL.

EXIT LOSS

$h_1 = K \left(\frac{V_1^2}{2g} \right) = 0.0675 \text{ ft}$

$h_2 = f \cdot \frac{L}{D} \cdot \frac{V_2^2}{2g} = 0.235 \text{ ft}$

$h_4 = f \cdot \frac{L_c}{D} \cdot \frac{V_c^2}{2g} = 0.0193 \text{ ft}$

$h_5 = f \cdot \frac{L_c}{D} \cdot \frac{V_5^2}{2g} = 1.412 \text{ ft}$

$h_6 = f \cdot \frac{L_c}{D} \cdot \frac{V_6^2}{2g} = 2.66 \text{ ft}$

$h_7 = 1.0 \left(\frac{V_7^2}{2g} \right) = 0.642$

$h_3 = f \cdot \left(\frac{L_c}{D} \right) \left(\frac{V_3^2}{2g} \right)$

$\Delta h_L = 5.23 \text{ ft}$

$h_A = h_L + (Z_2 - Z_1)$

$= 21.32 \text{ ft}$

Z in SCH 40

$V_5 = \frac{Q}{A} = 2.869 \text{ ft/s}$

$V_7 = \frac{Q}{A} = 6.423 \text{ ft/s}$

$NR = \frac{VD}{\mu} = 2.41 \times 10^4$

$NR = 3.67 \cdot 10^4$

$O/E = 746.67$

$F = 0.0265$

$ECI \cdot CO = \frac{P}{\rho} = 1148.87$

$P = \gamma Q h_A$

$= 0.169 \text{ hp}$

Paragraph:

We learned that the two equations given in the book to determine flow rate and to determine pipe diameter should not be used under any circumstances. Series pipeline systems are when fluid flows through a single continuous path. Therefore, the flow rate is equal throughout the system, and energy losses are equal to the sum of all the losses in the system. For the critical velocity of water in pipes, we are using three meters per second for this class when determining pipe diameter.

In parallel pipeline systems, the total flow rate is found by adding the flow rates of different parts of the system together. The energy losses of all parts of the system are equivalent and equal to the total energy losses of the system.