



CUSTOMER:

CASEY O'CONNOR

DATE:

PROJECT NO.

TITLE:

BY:

REFERENCE NO.

DESCRIPTION:

CKD:

REV:

PURPOSE

DESIGN COMBINATION LINE SERIES TO DELIVER WATER AT 275 gpm FROM TANK THROUGH HEAT EXCHANGER & BYPASSES.

- REQUIRED PUMP POWER CLOSED AND POWER AT DIFFERENT THROTTLED 1" GATE VALVES.

SOURCES

MOTT, R., UNITENAR JA, "APPLIED FLUID MECHANICS", 7TH EDITION, PEARSON INC (2013)

DESIGN CONSIDERATIONS :

INCOMPRESSIBLE FLUID
ISOTHERMAL 160° F
STEADY STATE
NEWTONIAN FLUID

MATERIALS:

WATER
STEEL SCH 40



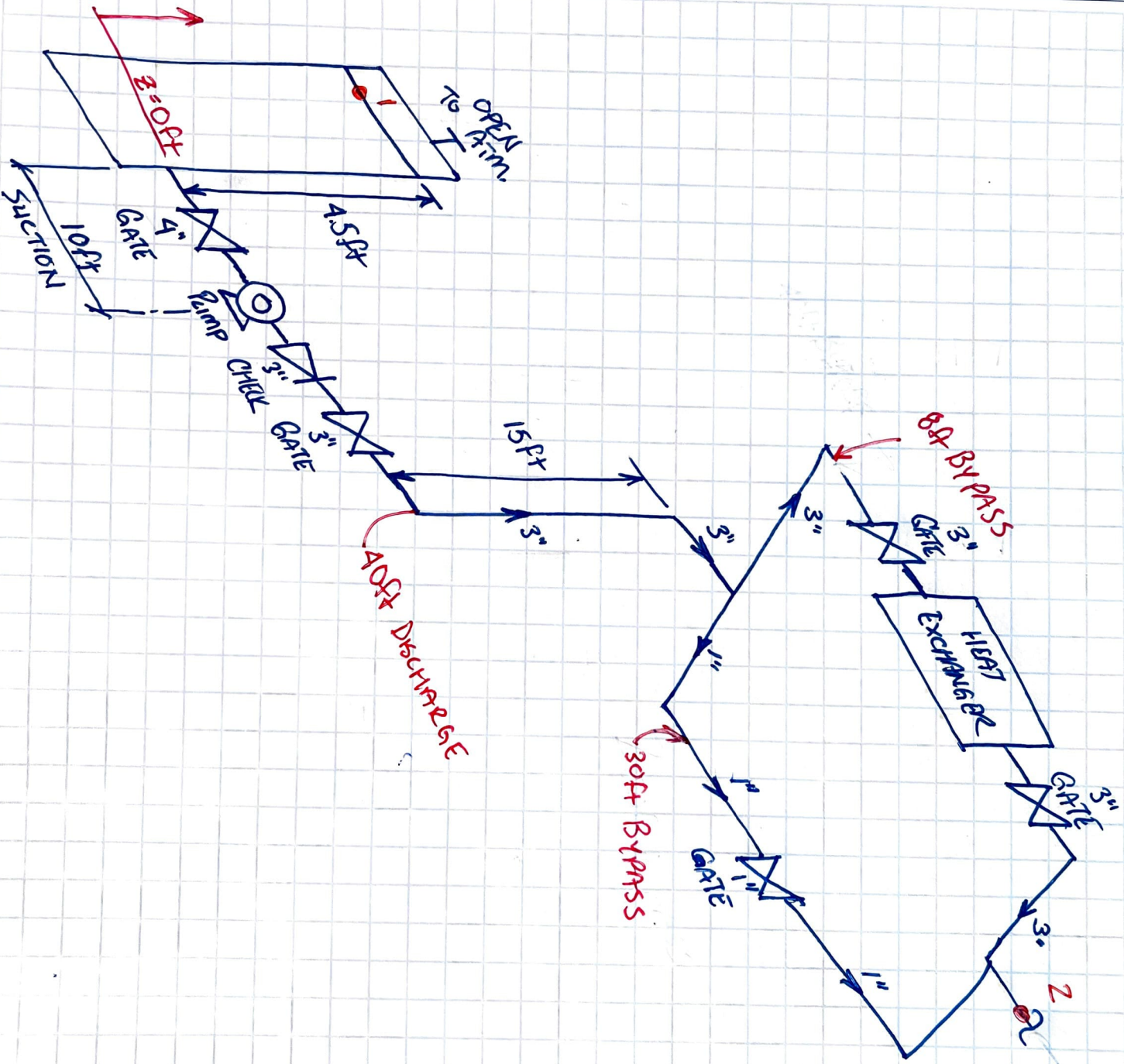
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DATA & VARIABLES

WATER 160°F

$$Q = 275 \text{ gpm} \Rightarrow .6127 \text{ ft}^3/\text{s}$$

$$\gamma_w = 61$$

$$\rho = 1.9$$

$$\eta = 8.3 \times 10^{-6}$$

$$\nu = 4.38 \times 10^{-6}$$

$$3" \text{ SCH40} \Rightarrow .05132 \text{ ft}^2, \text{ I.D.} = .2557 \text{ ft}$$

$$1" \text{ SCH40} \Rightarrow .006 \text{ ft}^2, \text{ I.D.} = .0874 \text{ ft}$$

$$4" \text{ SCH40} \Rightarrow .08840 \text{ ft}^2, \text{ I.D.} = .3355 \text{ ft}$$

Pipe ft

$$4": .016$$

$$3": .017$$

$$1": .022$$

$$4" \text{ GATE VLV} \Rightarrow K = 8 \text{ ft} \quad 8(.016) = .128$$

$$3" \text{ GATE VLV} \Rightarrow K = 8 \text{ ft} \quad 8(.017) = .136$$

$$3" \text{ CHECK VLV} \Rightarrow K = 100 \text{ ft} \quad 100(.017) = 1.7$$

$$3" 90^\circ \text{ ELBOW} \Rightarrow K = 30 \text{ ft} \quad 30(.017) = .51$$

PUMP

$$\text{HEAT EXCHANGER} \Rightarrow K = 12 \text{ ft} \quad 12$$

GATE

$$\text{OPEN} \quad 8$$

$$3/4 \quad 35$$

$$1/2 \quad 160$$

$$1/4 \quad 900$$

$$\text{TEE} * \text{SPECIAL FABRICATED} \Rightarrow K \text{ VALUE - SAME AS BOOK} \quad 60 \text{ ft} = 60(.017) = 1.02$$

$$\text{SQUARE EDGE INLET} - K = .5$$

$$1" \text{ GATE VLV} \Rightarrow K = 8 \text{ ft}$$



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CALCULATIONS: FIND Q IN 4" Ø SUCTION PIPE

$$Q = VA \Rightarrow .6127 \text{ ft}^3/\text{s} = V (.08840 \text{ ft}^2) = 6.93 \text{ ft/s}$$
$$4" V = 6.93 \text{ ft/s}$$

$$V \text{ of } 3" \phi$$
$$.6127 \text{ ft}^3/\text{s} = V (.05132 \text{ ft}^2) = 11.9 \text{ ft/s}$$

$$V \text{ of } 1" \phi$$

$$.6127 \text{ ft}^3/\text{s} = V (.006 \text{ ft}^2) = 102.1 \text{ ft/s}$$

$$\frac{V^2}{2g} \text{ of } 4" \Rightarrow \frac{6.93^2}{2(32.2)} = .746$$

$$\frac{V^2}{2g} \text{ of } 3" \Rightarrow \frac{11.9^2}{2(32.2)} = 2.2$$

$$h_L \text{ OF } 4" \Rightarrow h_{exit} = .5$$

$$h_{GATE} = .128$$

$$h_{PIPE} = .016 \frac{10}{.3355} = .477$$

$$.5 + .128 + .477 (.746) = .82433 \text{ ft}$$



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LOSSES IN DISCHARGE, 3"

$$\frac{V^2}{2g} \text{ OF } 3" = 2.2 \text{ ft/s}$$

$$3 \quad h_{\text{GATE}} = .136$$

$$h_{\text{CHECK}} = 1.7$$

$$4 \quad h_{\text{ELL}} = .51$$

$$2 \quad h_{\text{TEE}} = 1.02$$

$$h_{\text{DISCHARGE}} = .017 \left(\frac{40}{.2557} \right) = 2.659$$

$$h_{\text{TEE}} = 1.02$$

$$h_{\text{PIPE}} = .017 \left(\frac{8}{.2557} \right) = .5319$$

$$h_{\text{HE}} = 12(.017) = .204$$

$$h_{\text{OUTLET}} = 1(.017) = .017$$

$$\text{ADD } h_{\text{VALUES}} = 10.6199 (2.2) = 23.36 \text{ ft}$$



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BERNOULLI'S EQUATION

$$h_A + \frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_{L1-2}$$

$$h_A + 4.5\text{ft} = 2.2 + 15\text{ft} + 24.124$$

$$h_A = 2.2 + 10.5 + 24.124$$

$$h_A = 36.824\text{ft}$$

$$\text{CALC Pump Power} \Rightarrow \frac{\gamma Q h_A}{\eta}$$

$$= \frac{61 (.6127 \text{ ft}^3/\text{s}) (36.824)}{.7}$$

$$= 1966.12 \frac{\text{lb} \cdot \text{ft}}{\text{s}} / 550 = \boxed{3.57\text{hp}}$$



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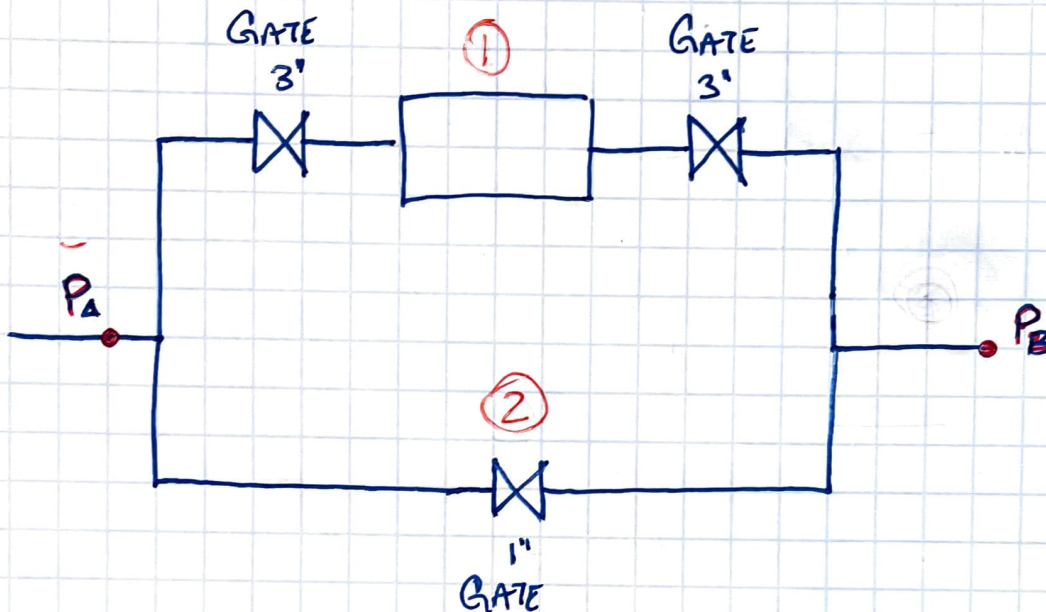
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$$\frac{P_A}{\gamma} = h_L AB$$

$$\frac{P_A}{61} = 1.02 + 2(.136) + .204 + 1.02 = 2.516(2.2)$$

$$\frac{P_A}{61} = 5.5352$$

$$P_A = 337.6472$$



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Summary -

TO DELIVER WATER FROM LOWER TANK THROUGH HIGHER HEAT EXCHANGER AT A RATE OF 275 gpm, WE WILL NEED A PUMP WITH 3.57hp, ASSUMING THE PUMP EFFICIENCY IS 70%.

THE PUMP POWER WILL NEED INCREASED WHEN THE 1" BYPASS GATE VALVE IS OPEN.

ANALYSIS -

THE PROCEDURE IN THE TEST IS SIMILAR TO PREVIOUS EXAMS. ADDITIONAL CONCEPTS FROM CHAPTER 10 WERE INTRODUCED. CALCULATING THE FLOW RATE FOR MULTIPLE BRANCH SYSTEMS IS A LONG PROCESS THAT REQUIRES SIGNIFICANT PRACTICE AND UNDERSTANDING OF THE CLASS CONCEPTS.