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MET 330

Hw 12
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13.2. $Q = 750 \text{ L/min}$ or 198 gal/min
 $T = 80^\circ\text{C}$



Commercial steel pipe because water won't corrode.

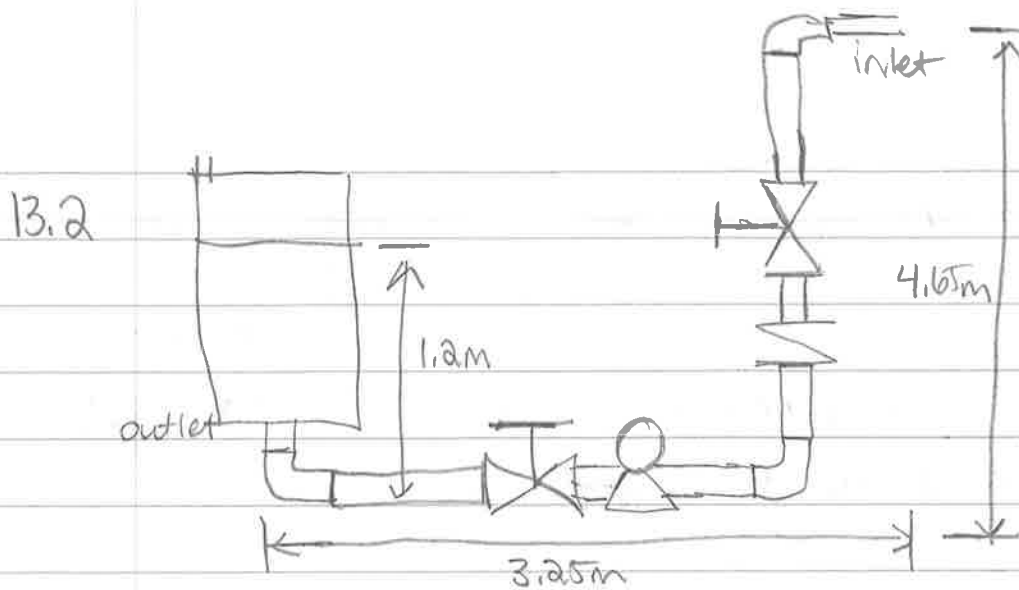
$Q = V \cdot A$ using criterion $V = 3 \text{ m/s}$

$$\frac{Q}{V} = A \quad \frac{750 \frac{\text{L}}{\text{min}}}{3 \text{ m/s}} \cdot \frac{1 \text{ m}^3/\text{s}}{1000 \frac{\text{L}}{\text{m}^3}} = 0.00417 \text{ m}^2$$
$$= 4.17 \times 10^{-3}$$

3" NPS steel pipe = $4.768 \times 10^{-3} \text{ m}^2$

$$\text{Real velocity} = \frac{Q}{A} = \frac{750 \cdot \frac{1}{1000}}{4.768 \times 10^{-3}} = 2.62 \text{ m/s}$$

meets criteria



$$H_A = H_L + \Delta z + \frac{v_a^2}{2g}$$

3 elbows, 2 gate valves, 1 check valve

Water @ 20°C ν (kinematic) = $3.60 \times 10^{-7} \text{ m}^2/\text{s}$

velocity $v = 2.162 \text{ m/s}$

$D = 77.9 \text{ mm} = 0.0779 \text{ m}$

$$N_R = \frac{(2.162)(0.0779)}{3.60 \times 10^{-7}} = \frac{566.939}{5.67 \times 10^{-5}}$$

$$\epsilon = 4.6 \times 10^{-5}$$

$$\frac{D}{\epsilon} = \frac{0.0779 \text{ m}}{4.6 \times 10^{-5}} = 1693.48$$

$$f = \frac{0.25}{\left[\log \left(\frac{1}{3.7(1693.48)} + \frac{5.74}{(5.67 \times 10^5)^{0.19}} \right) \right]^2}$$

$$\left[\log (0.000159 + 0.000038) \right]^2$$

$$f = 0.018$$

$$13.2 \text{ Total length of pipe} = 7.9 \text{ m}$$

$$4.15 \text{ m} + 3.25 \text{ m} = 7.9 \text{ m}$$

$$\frac{V_2^2}{2g} = \frac{2.62^2}{2 \cdot 9.81}$$

$$= 0.3499$$

$$= 0.350$$

$$\text{gate valve} = 8 \text{ ft} = 8(0.018) = 0.144$$

$$QTY 2 = 2 \times 0.144 = 0.288$$

$$\text{elbows} = 30 \text{ ft} = 30(0.018) = 0.54$$

$$QTY 3 = 3 \times 0.54 = 1.62$$

$$1 \text{ check valve (swing)} = 100 \text{ ft} = 100 \times 0.018 = 1.8$$

$$\text{entrance loss assume square edged inlet} = K = 0.5$$

$$h_L = K \left(\frac{V_2^2}{2g} \right) = 0.5 \left(\frac{(2.62)^2}{2 \cdot 9.81} \right) = 0.175$$

$$H_{L \text{ pipe}} = 0.018 \left(\frac{7.9 \text{ m}}{0.0779 \text{ m}} \right) = 1.83$$

$$H_{L \text{ all}} = 0.288 + 1.62 + 1.8 + 0.175 + 1.83 = 5.713 \text{ m}$$

$$\Delta z = 4.15 \text{ m}$$

$$H_A = 5.713 + 4.15 + 0.35 = 10.71 \text{ m}$$

$$= 35.14 \text{ ft}$$

$$\frac{V_2^2}{2g} = 0.35$$

$$Q = 198 \text{ gpm}$$

$$13.2 \quad H_a = H_L + \Delta z + \left(\frac{V_a^2}{2g} \right)$$

$$= 5.713 + 4.65 + 0.35 = 10.71 \text{ m} \quad Q = 198 \text{ gpm}$$

$$\frac{h_a'}{h_a^2} = \left(\frac{N_1}{N_2} \right)^2 = h_a^2 = h_a' \left(\frac{N_1}{N_2} \right)^2 = 10.71 \left(\frac{2916}{1475} \right)^2 = 42.84 \text{ m}$$

Pump preselection = 3x4x8B pump
 using sulzer curve - Type OHH and
 $H_A \approx 42.84 \text{ m} + Q = 198 \text{ gpm}$
 approx

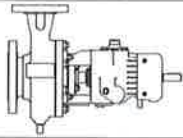
$$Q = 175 \text{ gpm} = 39.7 \text{ m}^3/\text{h}$$

$$Q = 200 \text{ gpm} = 45.4 \text{ m}^3/\text{h}$$

$$Q = 225 \text{ gpm} = 51.1 \text{ m}^3/\text{h}$$

$$\text{Impeller diameter} = 180 \text{ mm} = 7.09''$$

Final system would be 3 90° elbows,
 2 gate valves, 1 check swing valve, 3" nominal
 steel piping in total length of 7.9 m, and
 a pump in class 3x4x8B
 (verify with customer if flow rate 2198 gpm
 is acceptable). H_A after pump selection = 41 m
 Q after pump selection = 200 gpm

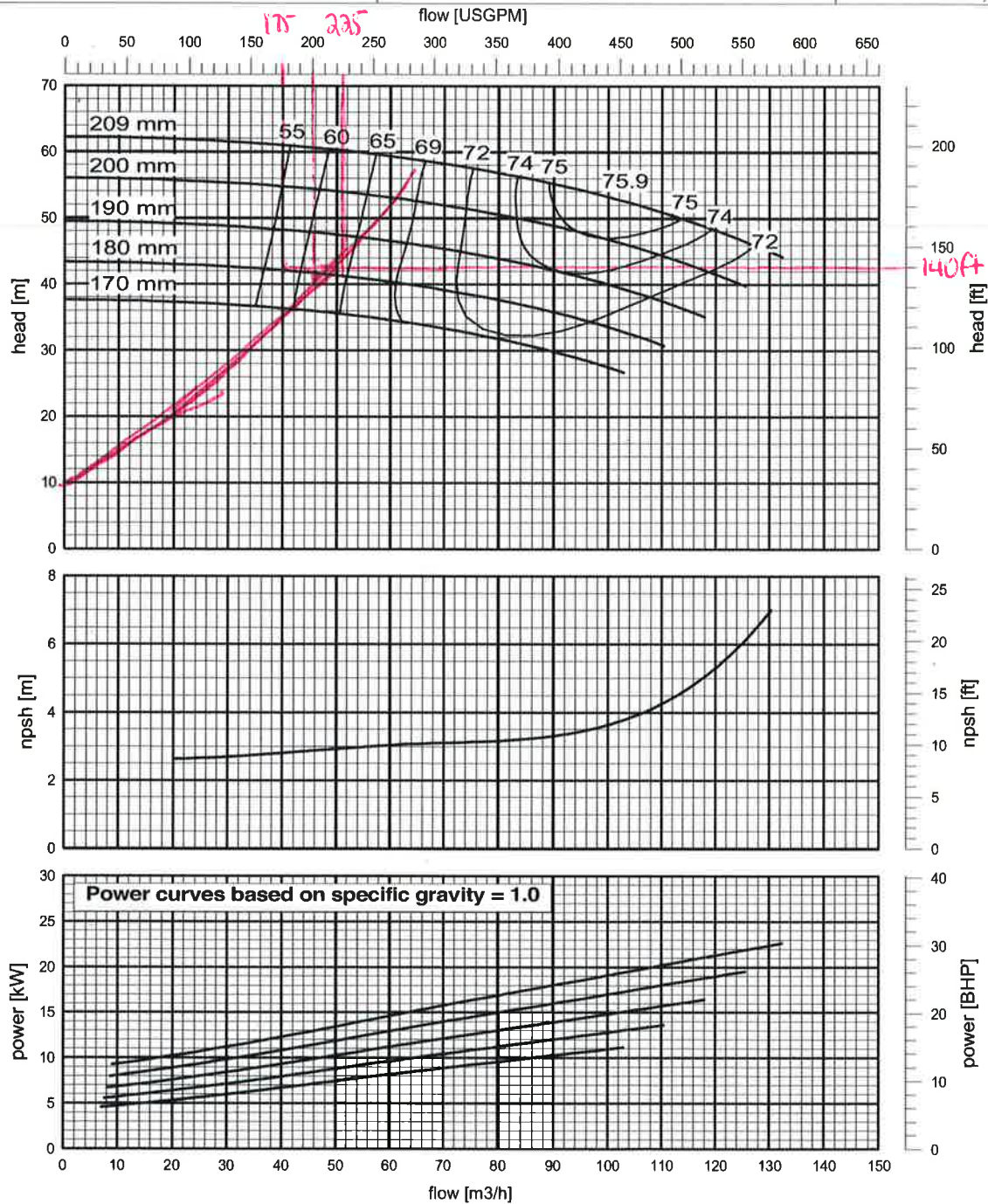


3 x 4 x 8B -1 OHH

SULZER

Series 2.00 / 50Hz E014

Curve No	OHH 68-1-2-01	NSS	183 (9448)	Speed
Efficiency Basis	API Std. clearances	nq	25 (1287)	2910
Max Solid	11 mm (.43 in)	Rotation	CCW viewed from coupling	rpm



Rated Conditions

Project	Item	
H =	Q =	P =
Calculated Efficiency =		NPSH _{3%} =
Issued: MSC / 12.21.2001		

SULZER

CURVES - TYPE OHH

Range of Performances - 50 Hertz / 1475 rpm

Series 2.00
CURVES
12 February 2002

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50hz
E0G

