

Note:

- Drawing not to scale

Part a | Chris Betton

Procedure

- We will select an appropriate pipe diameter for required Vel, fluid flow.
- We will use Bernoulli's Equation with energy losses & pump head
- Energy losses will be solved for in the piping and valve.
- Finally, solve for power of pump.

Materials

- Pump, 8" NPS piping sched. 40 two elbows, globe valve for pump discharge

Company Requirements

$$Q = 3.387 \frac{\text{ft}^3}{\text{s}}, v = 3 \frac{\text{m}}{\text{s}} = 9.8425 \frac{\text{ft}}{\text{s}}$$

$$K_{\text{valve}} = 5.3$$

$$\text{Pump Eff.} = 60\%$$

Assumptions

$$\gamma_w = 62.43 \frac{\text{lb}}{\text{ft}^3}$$

Data from Tables

$$D_{\text{pipe}} = 0.6651 \text{ ft}, 8" \text{ NPS}, A_{\text{flow}} = 0.3472 \text{ ft}^2$$

$$E_{\text{steel}} = 1.50 \times 10^{-4} \text{ ft}$$

$$\eta_{\text{water @ } 60^\circ\text{F}} = 2.50 \times 10^{-5} \frac{\text{lb-s}}{\text{ft}^2}$$

Calculations

$$Q = VA, A = \frac{\pi}{4} D^2 \therefore d = \sqrt{\frac{Q4}{v\pi}} = \sqrt{\frac{3.387 \text{ ft}^3/\text{s} \cdot 4}{9.8425 \text{ ft/s} \cdot \pi}} = 0.6619 \text{ ft} \approx 0.6651 \text{ ft}$$

$$h_A + \frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_L$$

P_1 & P_2 can be negated due to open channel

V_1 & V_2 can be negated due to large surface Area.

$$\therefore h_A = z_2 - z_1 + h_L$$

$$h_L = f \cdot \frac{L}{D} \cdot \frac{V^2}{2g} \text{ where } f = \frac{0.25}{\left[\log \frac{1}{3.7 \left(\frac{D}{E} \right) + \frac{5.74}{N_R^{0.9}}} \right]^2}$$

Note: friction factor calculated using excel

$$\left(\frac{D}{E} \right) = \frac{0.6651 \text{ ft}}{1.50 \times 10^{-4} \text{ ft}}$$

$$\therefore h_L = (0.014) \cdot \frac{2511}{0.6651} \cdot \frac{(9.8425)^2}{2 \cdot 32.2} = 79.508 \text{ ft}$$

$$\frac{(f+)}{(s)} \frac{\text{ft}}{\text{ft}} \frac{\text{ft}}{\text{ft}} \frac{\text{ft}}{\text{ft}}$$

$$h_L = 79.508 \text{ ft}$$

$$h_{L \text{ minor}} = K_{\text{valve}} \cdot \frac{V^2}{2g} = 5.3 \cdot \frac{9.8425^2}{2 \cdot 32.2} = 7.9726 \approx 10\% \text{ so must consider}$$

elbow = negligible because < 1%

$$h_A = 50 \text{ ft} + 79.508 + 7.9726 = 137.4806 \text{ ft}$$

$$P_A = \gamma \cdot Q \cdot h_A = \frac{62.43 \text{ lb/ft}^3}{\text{ft}^3} \cdot \frac{3.387 \text{ ft}^3/\text{s}}{\text{s}} \cdot \frac{137.4806 \text{ ft}}{\text{ft}} = 291.1 \text{ ft-lb/s}$$

$$P_A = 52.8297 \text{ HP}$$

$$P_M = \frac{52.8297 \text{ HP}}{0.60} = \boxed{88.04 \text{ HP}}$$

Analysis

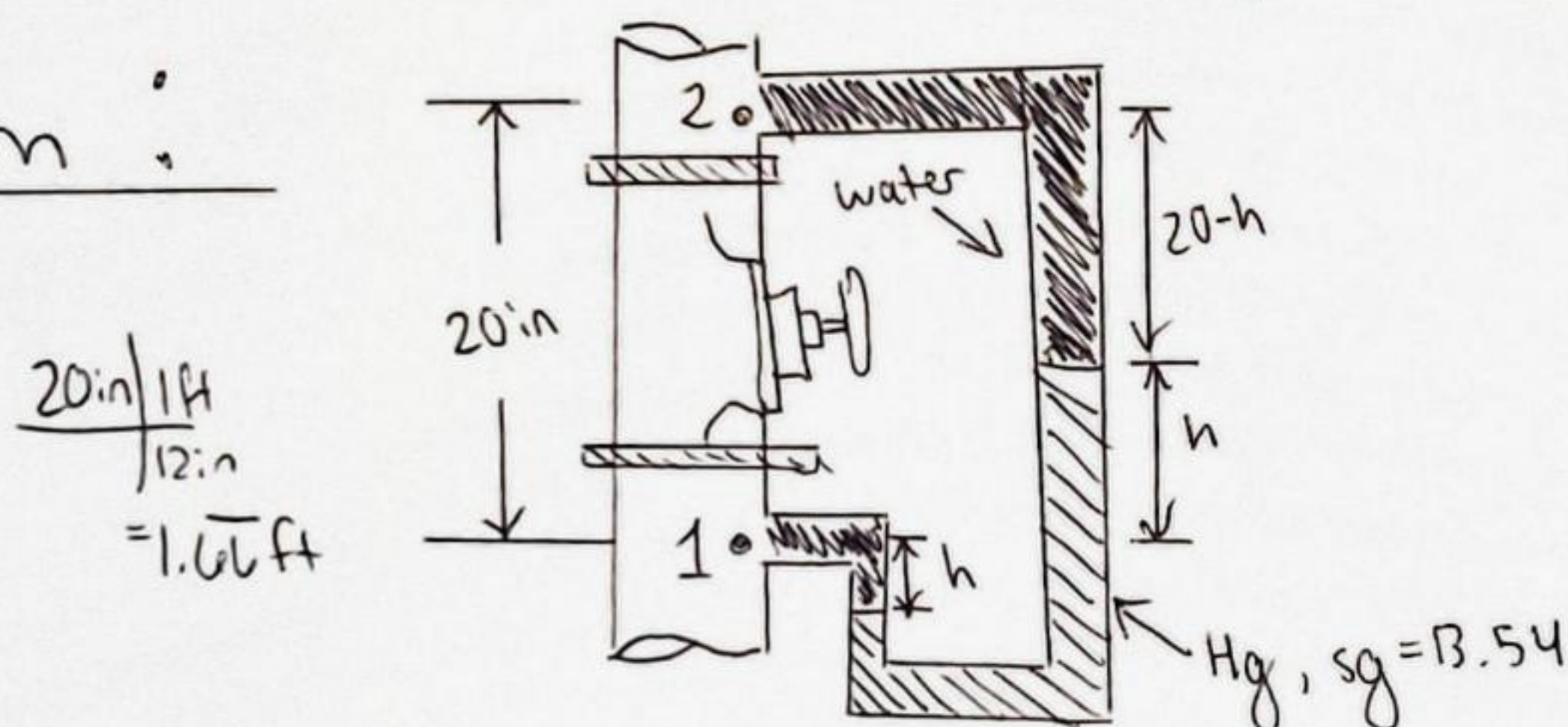
- The pumps power is proportional to head & flow rate.
- The elevation of the tanks in which the pump is transferring fluid directly effects its power.

Procedure

- First the change in pressure between point 1 & 2 was calculated.
- Then a manometric relation was formed based on the elevations of water & mercury (Hg) in the U-tube manometer.

Materials

- U-tube manometer, water, mercury

Diagram:Calculations

$$v = 9.8425 \frac{\text{ft}}{\text{s}} \text{ (see part a)}, \gamma_w = 62.43 \frac{\text{lb}}{\text{ft}^3}, K = 5.3, g = 32.2 \frac{\text{ft}}{\text{s}^2}$$

$$\frac{\Delta P}{\gamma_w} = K \cdot \frac{v^2}{2g} \therefore \Delta P = \gamma_w \left(K \cdot \frac{v^2}{2g} \right)$$

$$\Delta P = 62.43 \left(5.3 \cdot \frac{9.8425^2}{2(32.2)} \right)$$

$$P_1 - P_2 = \gamma_{\text{Hg}}(2h) + \gamma_w(1.67) - \gamma_w(h) - \gamma_w(h)$$

$$\Delta P = 13.54(62.43)(2h) + 62.43(20) - 62.43(h) - 62.43(h)$$

$$\Delta P = 1690.6044(h) + 104.0695 - 124.86(h)$$

$$497.49 - 1565.744(h) + 124.86$$

$$h = \frac{0.25128 \text{ ft}}{1 \text{ ft}} = 3.017 \text{ in Hg}$$

Equation for excel

$$h = \frac{\Delta P - \gamma_w(20)}{2\gamma_{\text{Hg}} - 2\gamma_w}$$

Analysis

- The water-mercury contact point drops a distance of 'h' which results in a raise of mercury surface level in the same amount.

The U-tube manometer is an effective tool for measuring differential pressure across the discharge valve.

This pressure is directly related to the valve's performance.

Data for Calculation			
Volume Flow - Q (ft ³ /s)	Average flow velocity - v (ft/s)	Valve resistance coefficient - k	Pump Efficiency
3.387	9.8425	5.3	0.6

Calculated Data		Friction Factor Calculation	
Calculated diameter (ft)	0.661926771	Relative Roughness (D/ε)	Reynolds Number N _R
Major System losses (ft)	80.40960178	4434	16347287.38
Minor System losses (ft)	7.972616042		
Total losses - h _L (ft)	88.38221782		
Energy addition - (ft) (Derived from Bernoulli's eq.)	138.3822178		
Pump power (HP)	53.20177581		
Power output from motor (HP)	88.66962635		

Assumptions			
Δz (ft)	Length of piping (ft)	Gravity (ft/s ²)	γ water (lb/ft ³)
50	2511	32.2	62.43

Assumption	Data From Tables		
Friction Factor	Reference Location	Variable	Value
0.014158693	Appendix D	Dynamic Viscosity water (60°F) (η)	0.000025
	Table 8.2	Pipe Roughness - ϵ (slug/ft*s)	0.00015
	Table F.1	Diameter (ft)	0.6651
	Table F.1	Flow area (ft ²)	0.3472
	Table F.1	NPS (in)	8

