

Purpose: a) Calculate pump power when the bypass valve is completely closed w/ minimum flow rate of 2.75 gpm, efficiency 70%

b) assuming pump power remains the same, calculate total flow rate if bypass valve is $\frac{1}{4}$, $\frac{1}{2}$, $\frac{3}{4}$, and fully open.

Drawing: Separate page

Sources: Mott, Untener, Applied Fluid Mechanics, 7th edition
Pearson Education 2015

Design consideration: - incompressible fluid
- isothermal
- steady state

Data & Variables: Separate pages

Procedure: used from pretest

Calculations: Separate

Summary & analysis: at end of a & b calculations

Test 3 pretest

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1) I think I understand the test prompt and do not have questions at this time. However, I expect that to change before I complete the test.

Procedure

2) a) 1) place points + reference

2) use Bernoulli's equation to find pumphead

3) plug in known values, cancel any terms necessary

4) compute energy losses

* some k values

given, others found in book

$h_L = k \frac{V^2}{2g}$ → used for gate valves, pipe, check valve, elbows, tees, exchanger, reduction + enlargement

5) compute pump power

$$P_A = \gamma Q h_A$$

$$P_{\text{input}} = P_A / \eta = \frac{\gamma Q h_A}{\eta}$$

b) Find Reynolds number for friction factor

$$Re = \frac{\rho V D}{\mu}$$

$$\frac{D}{\epsilon}$$

Other possible needed equations:

$$V = \frac{4Q}{\pi D^2}$$

$$Q = VA$$

→ find diameter of pipes inside from book

I am not 100% sure if the steps are in the correct order, but I am pretty sure those will be the necessary equations to do the problem. What I am not sure of is which of the valves, elbows, tees, sudden reduction / enlargement need to be included in the energy losses. Are we considering all losses in the whole system?

Procedure

b) 1) Pick points and reference (will be used again from part A)

2) Start with Bernoulli's and plug in known values / cancel anything necessary

3) compute pipe energy losses using

$$h_L = f \frac{L}{D} \frac{V^2}{2g} \rightarrow \text{for each type of loss}$$

4) Reynolds number and relative roughness are needed to find friction factor

$$Re = \frac{PVD}{\mu} = \frac{VD}{\nu} \quad D/\epsilon$$

5) Remember conservation of mass $Q_1 = Q_4 = Q_2 + Q_3$

6) Set up excel spreadsheet

1) guess friction factor

2) calculate flow rate (equation is previously

3) compute Reynolds number

derived)

4) find friction factor from Moody's chart using Re

5) compare new f to old f

6) repeat until % diff is near zero

7) this excel formula will need to be repeated with K values for each opening

$$3/4 = 35 \quad 1/2 = 160 \quad 1/4 = 900 \quad \text{fully} = 8$$

By changing friction factor in excel and 4) for the energy losses when the valve opening changes, it will give you a changing flow rate. I am not 100% sure how or if conservation of mass comes into play since it is only one flow rate per opening change

Data & Variables:

Water

- 160°F
- $\rho = 61 \text{ lb/ft}^3$
- $P = 61 \text{ lb/ft}^3$
- (m) • Dynamic viscosity = 8.28×10^{-6}
- (n) • Kinematic Visc = 4.37×10^{-6}
- $Q = 275 \text{ gpm} = 0.613 \text{ ft}^3/\text{s}$

$$\begin{aligned} 1'' &= 0.0874 \text{ ft} \\ 3'' &= 0.2557 \text{ ft} \\ 4'' &= 0.3355 \text{ ft} \end{aligned} \quad \left. \vphantom{\begin{aligned} 1'' &= 0.0874 \text{ ft} \\ 3'' &= 0.2557 \text{ ft} \\ 4'' &= 0.3355 \text{ ft} \end{aligned}} \right\} \text{ID}$$

$$\begin{aligned} 1'' &= 0.006 \text{ ft}^2 \\ 3'' &= 0.05132 \text{ ft}^2 \\ 4'' &= 0.0884 \text{ ft}^2 \end{aligned} \quad \left. \vphantom{\begin{aligned} 1'' &= 0.006 \text{ ft}^2 \\ 3'' &= 0.05132 \text{ ft}^2 \\ 4'' &= 0.0884 \text{ ft}^2 \end{aligned}} \right\} \text{Flow Area}$$

$$\epsilon (\text{steel pipe}) = 1.5 \times 10^{-4} \text{ ft}$$

Le/D

$$\begin{aligned} 3/4 \text{ open} &= 35 & 1'' &= 30/0.0874 = 343.25 \\ \text{fully open} &= 8 & 3'' &= 48/0.2557 = 187.72 \\ 1/2 \text{ open} &= 100 & 4'' &= 10/0.3355 = 29.81 \\ 1/4 \text{ open} &= 900 \end{aligned}$$

$$\begin{aligned} &\underline{K} \\ &\text{Square-edged inlet} = 0.5 \\ &\text{elbow} = 30 \text{ ft} \end{aligned}$$

$$V = Q/A$$

→ recalc on another page

$$\begin{aligned} 1'' &= 0.613/0.006 = 102.17 \text{ ft/s} \\ 3'' &= 0.613/0.05132 = 11.94 \text{ ft/s} \\ 4'' &= 0.613/0.0884 = 6.93 \text{ ft/s} \end{aligned}$$

D/ε

$$\begin{aligned} 1'' &= 0.0874/1.5 \times 10^{-4} = 582.67 \\ 3'' &= 0.2557/1.5 \times 10^{-4} = 1704.67 \\ 4'' &= 0.3355/1.5 \times 10^{-4} = 2236.67 \end{aligned}$$

$$Re = \rho V / \mu$$

$$1'' = \frac{102.17 \times 0.0874}{4.37 \times 10^{-6}} = 2,043,400$$

$$3'' = \frac{11.94 \times 0.2557}{4.37 \times 10^{-6}} = 698,640.3$$

$$4'' = \frac{6.93 \times 0.3355}{4.37 \times 10^{-6}} = 532,040.05$$

Data + Variables:

$Na > 4000$, so flow is turbulent

$$f_T = \frac{0.25}{\left(\log\left(\frac{1}{3.7D/\epsilon}\right)\right)^2}$$

$$1'' = \frac{0.25}{\left(\log\left(\frac{1}{3.7(582.67)}\right)\right)^2} = 0.0225$$

$$3'' = \frac{0.25}{\left(\log\left(\frac{1}{3.7(1704.67)}\right)\right)^2} = 0.0173$$

$$4'' = \frac{0.25}{\left(\log\left(\frac{1}{3.7(2236.67)}\right)\right)^2} = 0.0163$$

K

$$1'' = 343.25(0.0225) = 7.72$$

$$3'' = 187.72(0.0173) = 3.25$$

$$4'' = 29.81(0.0163) = 0.486$$

$$K = (L/D) f_T$$

$$\text{fully open} = 8(f_T)$$

$$\text{Check valve (swing)} = 100 f_T$$

$$3'' = 100(0.0173) = 1.73$$

$$1'' = 8(0.0225) = 0.18$$

$$3'' = 8(0.0173) = 0.1384$$

$$4'' = 8(0.0163) = 0.1304$$

$$3/4 \text{ open} = 35(f_T)$$

$$1'' = 35(0.0225) = 0.7875$$

$$3'' = 35(0.0173) = 0.6055$$

$$4'' = 35(0.0163) = 0.5705$$

$$1/2 \text{ open} = 160(f_T)$$

$$1'' = 160(0.0225) = 3.6$$

$$3'' = 160(0.0173) = 2.768$$

$$4'' = 160(0.0163) = 2.608$$

$$\text{Tees: flow thru branch} = 60 f_T$$

$$3''-3'' = 60(0.0173) = 1.038$$

$$3''-1'' = 60(0.0225) = 1.35$$

Elbows:

$$1'' = 30(0.0225) = 0.675$$

$$3'' = 30(0.0173) = 0.519$$

$$1/4 \text{ open} = 900(f_T)$$

$$1'' = 900(0.0225) = 20.25$$

$$3'' = 900(0.0173) = 15.57$$

$$4'' = 900(0.0163) = 14.67$$

gate
valve

$$\frac{V_2^2}{2g}$$

$$\frac{V_1^2}{2g} = \frac{102.17^2}{2(32.2)} = 162.09 \text{ ft} \quad (1")$$

$$\frac{V_3^2}{2g} = \frac{11.94^2}{64.4} = 2.21 \text{ ft} \quad (3")$$

$$\frac{V_4^2}{2g} = \frac{6.93^2}{64.4} = 0.746 \text{ ft} \quad (4")$$

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 + h_A = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_L$$

$$h_A = (z_2 - z_1) + \frac{V_2^2}{2g} + h_L$$

Losses: 4"

- ✓ gate valve
- ✓ entrance
- ✓ 10 ft pipe

3"

- ✓ 3 gate
- ✓ check
- ✓ 3 elbows
- ✓ 2 tees
- ✓ exchanger
- 48 ft pipe

1"

- ✓ 2 elbows
- sudden reduction
- gate → closed
- sudden enlargement
- 30 ft pipe
- 2 tees

$$(4") \quad h_L = 0.1304(0.746) + 0.5(0.746) + 0.486(0.746) = 0.833$$

$$(3") \quad h_L = 3(0.1304 \cdot 2.21) + 1.73(2.21) + 3(0.519 \cdot 2.21) + 2(1.038 \cdot 2.21) + (2 \cdot 2.21) + (3.25 \cdot 2.21) = 46.47$$

(1") I assume 1" line to not be considered b/c the valve is closed

$$h_L = 47.303$$

$$h_A = (15 - 4.5) + 2.21 + 47.303$$

$$h_A = 10.5 + 49.513$$

$$h_A = 60.013 \text{ ft}$$

$$\text{Power} = (0.613 \text{ ft}^3/\text{s}) (61 \text{ lb/ft}^3) (60.013 \text{ ft})$$

$$\text{Power} = 2244.07 \text{ lb ft}^2/\text{s}$$

$$2244.07 \frac{\text{lb ft}^2}{\text{s}} \left(\frac{0.0018 \text{ hp}}{1 \text{ lb ft}^2/\text{s}} \right) = \underline{\underline{4.04 \text{ hp}}}$$

$$\text{Efficiency} = \frac{4.04}{0.70} = \underline{\underline{5.77 \text{ hp}}}$$

B)

$$\cancel{\frac{P_A}{\rho}} + \cancel{\frac{V_A^2}{2g}} + z_1 + h_A = \cancel{\frac{P_B}{\rho}} + \cancel{\frac{V_B^2}{2g}} + z_2 + h_L$$

$$\frac{V_B^2}{2g} = (z_1 - z_2) + (h_A - h_L)$$

Branch 2

- 4 gate valves - 2 3", 2 4"
- ✓ 2 elbows - 3"
- ✓ 2 tees - 3"
- ✓ Exchanger
- ✓ Check valve - 4"
- 3" 4" pipe

$$\frac{V_2^2}{2g} = f_1 \frac{L_1}{D_1} \frac{V_1^2}{2g} + 2(f_1 \frac{L_e}{D})_{gv} \left(\frac{V_1^2}{2g} \right) + f_1 \left(\frac{L_e}{D} \right)_{cv} \left(\frac{V_1^2}{2g} \right) + 2(f_2 \frac{L_e}{D})_{tee} \left(\frac{V_2^2}{2g} \right) + 2(f_2 \frac{L_e}{D})_{elb} \left(\frac{V_2^2}{2g} \right) + 2(f_2 \frac{L_e}{D})_{gv} \left(\frac{V_2^2}{2g} \right) + K_{exc} \left(\frac{V_2^2}{2g} \right) + f_2 \frac{L_2}{D_2} \frac{V_2^2}{2g} + f_4 \frac{L_4}{D_4} \frac{V_4^2}{2g}$$

$$\frac{V_2}{2g} = f_1 \frac{L_1}{D_1} \left(\frac{16 Q_1^2}{\pi^2 D_1^4} \right) + 2(f_1 \frac{L_e}{D})_{gv} \left(\frac{16 Q_1^2}{\pi^2 D_1^4} \right) + f_1 \left(\frac{L_e}{D} \right)_{cv} \left(\frac{16 Q_1^2}{\pi^2 D_1^4} \right) + 2(f_2 \frac{L_e}{D})_{tee} \left(\frac{16 Q_2^2}{\pi^2 D_2^4} \right) + 2(f_2 \frac{L_e}{D})_{elb} \left(\frac{16 Q_2^2}{\pi^2 D_2^4} \right) + 2(f_2 \frac{L_e}{D})_{gv} \left(\frac{16 Q_2^2}{\pi^2 D_2^4} \right) + K_{exc} \left(\frac{16 Q_2^2}{\pi^2 D_2^4} \right) + f_2 \frac{L_2}{D_2} \left(\frac{16 Q_2^2}{\pi^2 D_2^4} \right) + f_4 \left(\frac{16 Q_4^2}{\pi^2 D_4^4} \right) \left(\frac{L_4}{D_4} \right)$$

$$\frac{V_2}{2g} = \left(f_1 \frac{L_1}{D_1} + 2f_1 \left(\frac{L_e}{D} \right)_{gv} + f_1 \left(\frac{L_e}{D} \right)_{cv} + f_4 \frac{L_4}{D_4} \right) \frac{8 Q_1^2}{g \pi^2 D_1^4} + (K_{exc} + 2f_2 \left(\frac{L_e}{D} \right)_{tee} + 2f_2 \left(\frac{L_e}{D} \right)_{elb} + 2f_2 \left(\frac{L_e}{D} \right)_{gv} + f_2 \frac{L_2}{D_2}) \frac{8 Q_2^2}{g \pi^2 D_2^4}$$

$$\frac{V_2}{2g} = f_1 \left(\frac{L_1 + L_4}{D_1} + 2 \left(\frac{L_e}{D} \right)_{gv} + \left(\frac{L_e}{D} \right)_{cv} \right) \frac{8 Q_1^2}{g \pi^2 D_1^4} + (K_{exc} + 2f_2 \left(\frac{L_e}{D} \right)_{tee} + 2f_2 \left(\frac{L_e}{D} \right)_{elb} + 2f_2 \left(\frac{L_e}{D} \right)_{gv} + f_2 \frac{L_2}{D_2}) \frac{8 Q_2^2}{g \pi^2 D_2^4}$$

Branch 3

$$\frac{V_3}{2g} = f_1 \left(\frac{L_1 + L_4}{D_1} + 2f_1 \left(\frac{L_e}{D} \right)_{gv} + f_1 \left(\frac{L_e}{D} \right)_{cv} \right) \frac{8 Q_1^2}{g \pi^2 D_1^4} + (2f_3 \left(\frac{L_e}{D} \right)_{elb} + f_3 \left(\frac{L_e}{D} \right)_{gv}) \frac{8 Q_3^2}{g \pi^2 D_3^4}$$

$$Q_1 = Q_2 + Q_3$$

Plug in branch 2:

$$\frac{V_2^2}{2g} = f_1 \left(\frac{10ft}{0.2557ft} + 2(8) + 100 \right) \frac{8}{32.2\pi^2} \frac{Q_1^2}{0.2557^4} \\ + (12 + f_2(2(60) + 2(30) + 2(8) + \left(\frac{8ft}{0.2557} \right)) \frac{8}{32.2\pi^2} \frac{Q_2^2}{0.2557^4}$$

$$\frac{V_2^2}{2g} = f_1(913.37)(Q_1^2) + 12 + f_2(1338.4)(Q_2^2)$$

Branch 3:

$$\frac{V_2^2}{2g} = f_1(913.37)(Q_1^2) + f_3(2(30) + 8) \frac{8}{9\pi^2} \frac{Q_3^2}{D_3^4}$$

$$\frac{V_2^2}{2g} = f_1(913.37)(Q_1^2) + f_3(29335.8)(Q_3^2)$$

$$\frac{4Q}{\pi D^2} = f_1(913.37)(Q_1^2) + 12 + f_2(1338.4)(Q_2^2)$$

$$19.47Q_2 = f_1(913.37)(Q_1^2) + 12 + f_2(1338.4)(Q_2^2)$$

$$Q_2 = \sqrt{\frac{f_1(913.37)(Q_1^2) + 12 + f_2(1338.4)}{19.47}}$$

$$\frac{4Q}{\pi D^2} = f_1(913.37)(Q_1^2) + f_3(29335.8)(Q_3^2)$$

$$\frac{4Q_3}{\pi(0.0874)^2} = f_1(913.37)(Q_1^2) + f_3(29335.8)(Q_3^2)$$

$$53.06Q_3 = f_1(913.37)(Q_1^2) + f_3(29335.8)(Q_3^2)$$

$$Q_3 = \sqrt{\frac{f_1(913.37)(Q_1^2) + f_3(29335.8)}{53.06}}$$

Summary: a) Power of the pump at 70% efficiency is 5.77hp.

b) I am unable to give a summary for part b due to the fact that my excel was incorrect.

Analysis: a) Many factors were needed in order to find pump power. After finding all necessary variables, calculating Re , V , D/z , f_r , $V^2/2g$, and losses, we were able to apply it to the power + efficiency equations to arrive at the solution. The power was a little different when the 70% efficiency was applied.

b) this part killed me. I was finally able to grasp the process necessary to find Q , but I struggled with the actual final equation ~~for~~ for Q . Of course, this was the one needed for excel. Due to my calculation struggles, I was unable to finish the problem in its entirety.