John Vasquez MET 330 Fluid Mechanics

Test 1

<u>Purpose</u>

Determine the amount of air pressure required by the tank on the right (B) needed to deliver 250 gal/min of ethyl alcohol. Once the air pressure in tank B begins to drop, determine at what air pressure the flow of the ethyl alcohol comes to a stop. Lastly determine the flow rate when the air pressure reaches 75 psi.

Drawings & Diagrams



Drawing Created in "One Note"

<u>Sources</u>

Mott, R., Untener, J.A. "Applied Fluid Mechanics", 7th edition Pearson Education, Inc, (2015)

Design Considerations

| -2 in Schedule 40 Steel Pipe | -Horizontal Pipe section 36ft |
|-------------------------------|-------------------------------|
| -Temperature 77°F | -Manometer Fluid = Mercury |
| -System Fluid = Ethyl alcohol | |

Data Variables:

-Tank A, pressure = 40 lb/in^2

-Volume Flow Rate Q= 250gal/min = 0.557 ft³/s

-Pipe Roughness $E = 1.5 \times 10^{-4}$

-Ethyl Alcohol @ 77°F pg. 490 | SG = .787 | y = 49.01 lb/ft³ | p = 1.53lb slug/ft³ | Dynamic Viscosity η = 2.10x10⁻⁵

-2in Schedule Pipe 40 pg. 500 | OD = 2.375in | Wall Thickness = 0.154in | ID = .1723ft, 2.067in | Flow Area = 0.02333 ft²

Procedure:

I would reference my sketch / drawing for the known variables, as I am to solve for pressure within tank B (right). I would then use the given heights to find the total distance from the reference to the height of the fluid (ethyl alcohol) within tank B. Utilizing Bernoulli's equation I would solve using the known values to provide a value for the pressure within tank B. After establishing my equation for pressure needed in tank B, I would identify any energy added, energy removed and energy loss within the system. After solving for the pressure within tank B, I would then utilize the needed equations to establish the readings displayed within the monometer portion of the system. I would then utilize calculations to proceed with calculating new manometer reading, along with flow rates as required.

Calculations:

| Part 1 Desolve for pl At Irn EB | |
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| Colculations | |
| $\frac{PL + N^{2} + 2I = P2 + V2^{2} + 22 + 61 + 61 + 61}{8 - 29} = \frac{PC}{29} = \frac$ | + hi thi overoir going 12 Pipe in Pipe |
| P1= P2+ & (22 42 + 22-2, +he leta) P9 40 | 71 Alcohol ethyl |
| • $7 = 49.01$ • $7 = 49.01$ • $7 = 37.2 + 7/c$ • $7 = 7$ • $7 = 7$ • $7 = 42 + 1$ • $7 = 7$ • $7 = 7/c$ • 7 | 49,01 16/048 |
| · NOW I Would Salve for Velues CX, V, A- given | PG 500 |
| $Q = A V_2$ $Q = \frac{250 \text{ grl/min}}{449} = \frac{557 \text{ Gr}^2}{1 \text{ Sec}} = \frac{V_2^2 - 23.81^2}{29} = \frac{8.85}{29}$ | |
| = V2= .557 FH/S = V2= 23.87 .02338 FVS | + he salira la |
| • New I would Selve for All Energy lost he = gave + Pipe 1. | + Pipe 2 + Pipe 144 A |
| -I need to salve for Pougherr of Pipe = 19185 equation + made |) Diegram |
| D - 1723 = 1148.67 | |
| - I need to Shue for Flow throug pipe = pg 103 equation 3 | Richen factor of Ruchen pipe |
| NR= VDP=(23.82)(1.723)(1.53) = Z99446.9 J= .020 Th Z10×10-5 Z99446.9 J= .019# | 5 = pg 185 Chert |
| - I ned to solve for energy loss of Both pipe bend | - 90° |
| $2h_{1} = 14\left(\frac{V_{2}^{2}}{7g}\right) = .57(8.95) = 2(5.044) = h_{1} = 10.88 \text{ f} + \frac{1}{7g}$ | Le = 30 |
| k = 5 + Le = .019(30) = .57 | Stendard 90 D |

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Summary:

The required air pressure needed for tank B (right) to deliver 250 gal/min of ethyl alcohol as required was derived to be 90 psig. There were several areas of friction loss throughout the system. The identified areas included: two pipe bends, inlet loss from tank B to pipe, gate valve at 100% "open" and the overall 110ft of pipe. The manometer deflection reading originally depicted by the system was at a value of "h" at 8.5ft. As the pressure in tank B was established at 90psig, manometer deflection reading resulted in a dropped height. The flow rate calculated at the range of 75 psig was approximated at 205 gal/min.

Materials:

-Ethyl alcohol

-Overall system components, 2-in Schedule 40 steel pipe (tanks, piping sections, valve and fittings)

-Manometer apparatus

Analysis:

-The required pressure needed to deliver 250 gal/min is 90 psig.

-No energy was added or removed within the system.

-Friction energy was loss thought the entire system (valve, overall pipe friction, two pipe bends, tank square inlet) $h_L = h_L$ gate valve + h_L pipe bend 1 + h_L pipe bend 2 + h_L pipe friction loss + h_L tank inlet.

-Manometer deflection was originally reflected 8.5ft = h, manometer deflection dropped as pressure was increased in tank B to approximately h = 1.4ft.

-Calculations reflect that as tank B was established to a pressure of 75 psig, the calculated flow would be approximately 205 gal/min.

| | Question 1 | | | | | | | | | | | | |
|---------------------------------|------------|-----------------------|----------|--------------------|--|---|--|---------|--------------------|--------------------|--------------------|--|--|
| Variable | Value | Unit | Value | Unit | | Variable | Equation | Value | Unit | | | | |
| P ₁ | 90.340 | lb/in ² | 13055.14 | lb/ft ² | | Berpullis Equation | $P1/v + V^2/2\sigma + 7 = P2/v + V^1/2\sigma + 7$ | | | | | | |
| V1 | 0.000 | ft/s | | | | Demains Equation | 11/9 . 0 1/26 . 21 - 12/9 . 0 2/26 . 22 | | - | | | | |
| $V_1^2/2g$ | 0.000 | ft/s | | | | | | | | | | | |
| Z1 | 26.000 | ft | | | | Bernullis Equation for | $P_{2} + v(V_{2}^{2} + V_{1}^{1} / 2\sigma + 7 + 7 + b)$ | 90 340 | psig | | | | |
| P ₂ | 40.000 | lb/in ² | 5760 | lb/ft ² | | P1 = | $F2 + y(v_1 + v_2)/2g + Z_2 + Z_1 + HL_total)$ | 50.540 | lb/in ² | | | | |
| V ₂ | 23.870 | ft/s | | | | | | | | | | | |
| V ₂ ² /2g | 8.850 | ft/s | | | | h _{L Pipe Bend 1& 2} | Ket (2 ² /2-) | 5.045 | 64 | | | | |
| Z ₂ | 42.000 | ft | | | | h _L =K _{Pipe Bend} (V2 ² /2g) | K*(V2 /2g) | 5.045 | п | | | | |
| h _{L Gate Valve} | 1.345 | ft | | | | | | | | | | | |
| h _{L Pipe Bend 1} | 5.045 | ft | | | | h _{L Gate Valve} | 1440.42 ² /2 | 1.245 | 6 | | | | |
| h _{L Pipe Bend 2} | 5.045 | ft | | | | h _L =K _{Gate Valve} (V2 ² /g) | K*(V2 ⁻ /2g) | 1.545 | π | | | | |
| h _{L Overall Pipe} | 107.351 | ft | | | | | | | | | | | |
| h _{L Entrance Loss} | 4.425 | ft | | | | h _{L Overall Pipe} | h _f +(1/D) +(1/2 ² /2-) | 107 251 | 6 | | | | |
| h _L Total | 123.210 | ft | | | | $h_L = f_f^{*}(L/D)^{*}(V2^2/2g)$ | n _L =t _f *(L/D)*(V2 /2g) | 107.351 | π | | | | |
| y Ethyl | 49.010 | slugs/ft ³ | | | | | | | | | | | |
| y Ethyl | 0.340 | ft | | | | h _{L Entrance Loss} | ь к (VD ² /D_) | 4.405 | | | | | |
| g | 32.200 | ft/s ² | | | | h _L =K _{square inlet} (V2 ² /2g) | N _L =K Entrance Loss(V2 / 2g) | 4.425 | π | | | | |
| Q Flow Rate | 0.557 | ft³/s | | | | | | | | | | | |
| Q Flow Rate | 250.000 | gal/min | | | | h Total Energy Loss | (hi Gata Value + hi Bine Band a + hi Bine Band a + hi | 100.010 | 4 | | | | |
| Area | 0.023 | ft² | | | | n _L rotal Energy Loss | Overall Pipe +hLTank Inlet) | 123.210 | π | | | | |
| K Pipe Bend | 0.570 | _ | | | | | | | | | | | |
| K Gate Valve | 0.152 | - | | | | | Question 2 | | | | | | |
| K Entrance Loss | 0.500 | - | | | | Bernullis Equation | $D_{1}/(1 + N^{2}/2 + 7)$ | 169 255 | | lb/in ² | lb/ft ² | | |
| Friction Factor | 0.019 | - | | | | Equalization P1 | $r_1/y + v_1/2g + Z_1$ | 106.000 | - | 48.45 | 6978 | | |
| Length of Pipe | 110.000 | ft | | | | Bernullis Equation | $D_{1} = (1 + 1)^{2} = (1 - 1)^{2}$ | 100.077 | | | | | |
| Diameter of Pipe | 0.172 | ft | | | | Equalization P2 | $P_2/\gamma + V_2/2g + Z_2$ | 168.577 | - | | | | |
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