

HW 2.4

15-41 a Sharp-edged orifice placed in a 6 in diameter pipe

Carrying Ammonia. Volume flow rate is 25 gal/min.

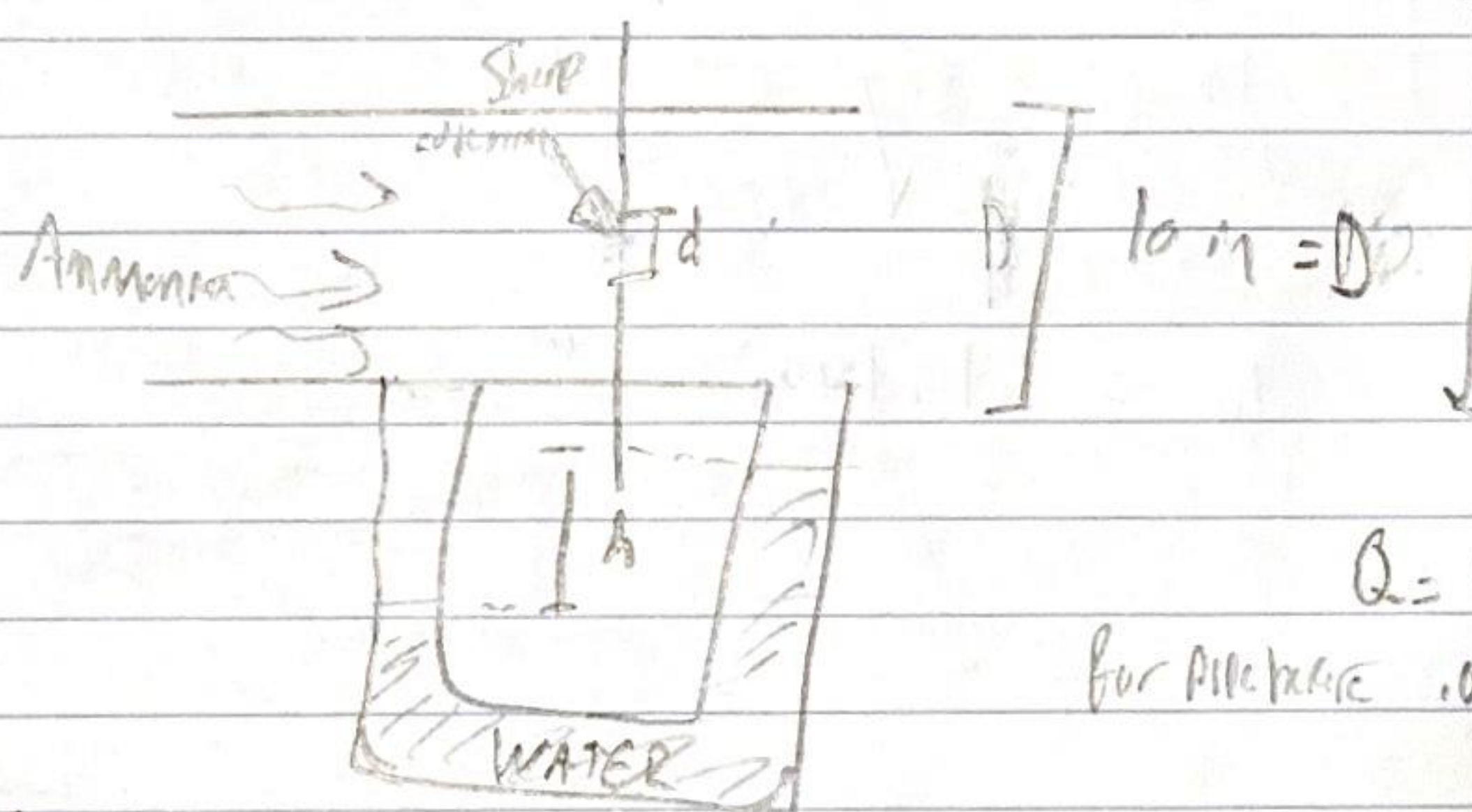
Read deflection of water manometer is

a.) orifice diameter = 1.0 in

b.) orifice diameter = 7.0 in

at 60 degrees Ammonia $SG = .83$ Dynamic Viscosity = $2.5 \times 10^{-6} \text{ lb} \cdot \text{s} / \text{ft}^2$

$$Q = 25 \text{ gal/min} \cdot (1 \text{ ft}^3/\text{s}) / (449 \text{ gal/min}) = .0557 \text{ ft}^3/\text{s}$$



$$Q = VA$$

$$\text{for Ammonia } .0557 \text{ ft}^3/\text{s} = V(\pi (1.5 \text{ in})^2)$$

$$V = .102 \text{ ft/s}$$

Useful

Eq 15.6

$$V_1 = C \cdot \sqrt{\frac{2gh[(\gamma_m/\gamma_f) - 1]}{(A_1/A_2)^2 - 1}}$$

$$N_R = \frac{VDP}{\eta}$$

$$= \frac{(.102 \text{ ft/s})(\frac{10}{12} \text{ ft})(.83 - 1.94 \text{ Slugs/ft}^3)}{2.5 \times 10^{-6} \text{ lb} \cdot \text{s} / \text{ft}^2}$$

$$= 54746.8 \approx 55 \text{ k} \cdot \text{sh}$$

and using sharp-edged orifice chart!

for a) $d/D = 1 \text{ in} / 6 \text{ in} = .1$ $C = .595$ b) $d/D = 7 \text{ in} / 6 \text{ in} = .7$ $C = .618$ Using $N_R \approx 65000$

Cont

2/6

15.4 Core

a. 1 in diameter

$$V_1 = C \sqrt{\frac{2g(P_1 - P_2)/\gamma}{(A_1/A_2)^2 - 1}}$$

q. 1 in diameter is
27.97 ft deflection

$$= C \sqrt{\frac{2gh(\gamma_m/\gamma_f - 1)}{(A_1/A_2)^2 - 1}}$$

4 ft units
more

$$\left\{ \begin{array}{l} .102 \text{ ft/s} \\ = (.595) \cdot \sqrt{\frac{(2) \cdot (32.2 \text{ ft/s}^2) \cdot (1) \cdot \left[\left(\frac{1}{.866}\right) - 1\right]}{\left[\frac{\pi (5/16)^2}{4} / \frac{\pi (1/24)^2}{4}\right]^2 - 1}} \end{array} \right.$$

$$\frac{.102 \text{ ft/s}}{.595} = \frac{.5 \sqrt{10.52(h)}}{9944 \text{ ft}^2}$$

$$h = (.1714)^2 \cdot \frac{9944 \text{ ft}^2}{10.5} = \underline{27.97 \text{ ft}}$$

Unit: Check, all good

b. 7 in diameter

$$.102 \text{ ft/s} = .618 \cdot \sqrt{\frac{(2) \cdot (32.2 \text{ ft/s}^2) \cdot h \cdot \left(\frac{1}{.666} - 1\right)}{\left[\frac{\pi (5/16)^2}{4} / \frac{\pi (7/24)^2}{4}\right]^2 - 1}}$$

$$\frac{.102 \text{ ft/s}}{.618} = \sqrt{\frac{10.52(h)}{3.165 \text{ ft}^2}}$$

$$h = (.165)^2 \cdot \frac{3.165}{10.5} = \underline{.008 \text{ ft}}$$

Solas

a.) 27.97 ft deflection at 1 in diameter orifice

b.) .008 ft deflection at 7 in diameter orifice

← this seems suspect

15-a/ Flow nozzle to be installed in a 5-in Type 12
Copper tube carrying Insulated oil @ 77°F.

Mercury Manometer. measure Δp across nozzle,
with flowrate between 700-1000 gal/min.

Mercury manometer between a- 8.0 in.

... Size of nozzle? (Diameter)

First app. App H

5 in Type 12 Copper tube $ID = .4004$ ft
 $A_c = .1254$ ft²

APP B

Mercury $S_g = 13.54$

Insulated oil @ 77°F: $S_g = .930$

$\rho = 1.8$ slugs/ft³

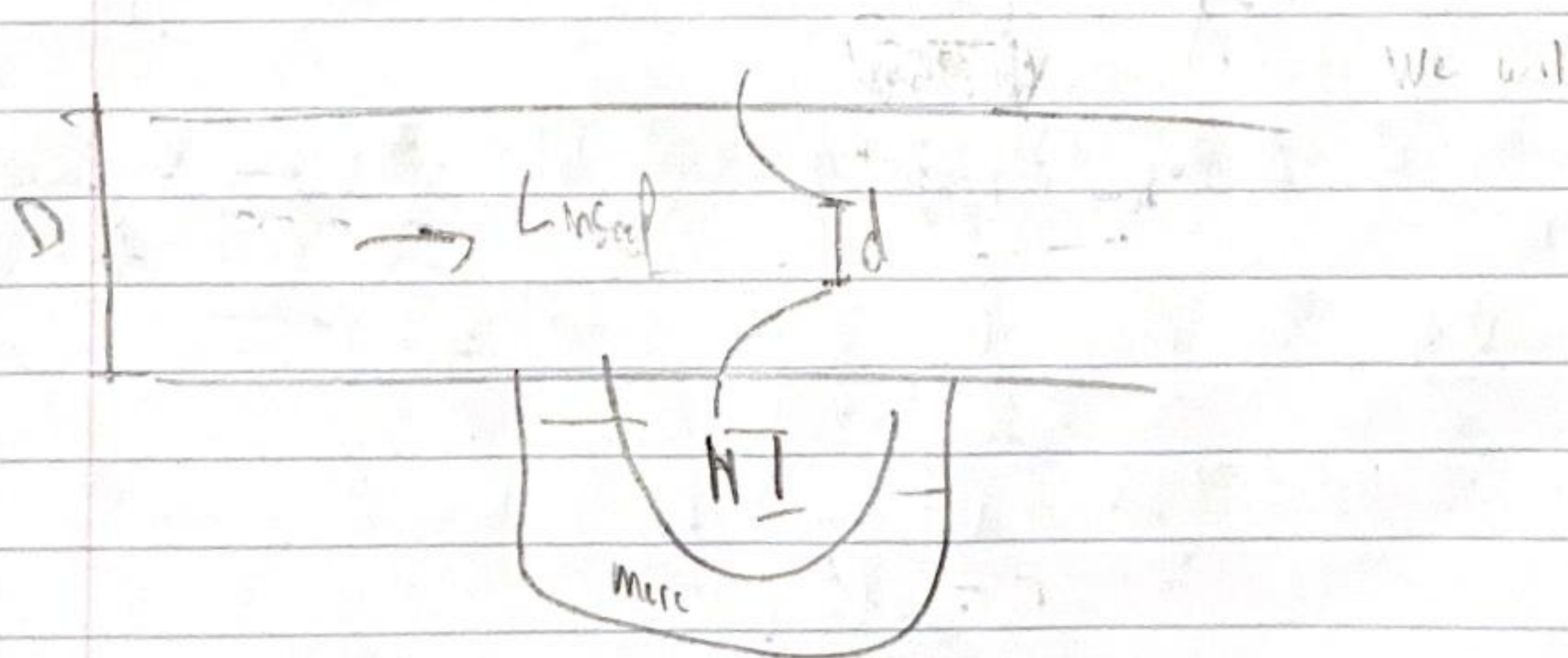
$\mu = 6.91 \times 10^{-4}$ lb-s/ft²

$Q = 700 - 1000$ gal/min

H must be lower than 8.0 in = $\frac{2}{3}$ ft

a 1 ft³/s = 449 gal/min

$Q = 1.56 - 2.23$ ft³/s



4/6

15-9 | ConL

Using (15-6)

$$V_1 = C \sqrt{\frac{2gh \left[\frac{\gamma_m}{\gamma_L} - 1 \right]}{\left[\left(\frac{A_1}{A_2} \right)^2 - 1 \right]}}$$

$$Q = VA$$

$$V = Q/A$$

$$\left. \begin{array}{l} Q = 1.56 \text{ ft}^3/\text{s} \\ \text{or } Q = 2.23 \text{ ft}^3/\text{s} \end{array} \right\} A_1 = 1259 \text{ ft}^2 \rightarrow V_1 = 12.4 \text{ ft/s} \\ \text{or } V_1 = 17.7 \text{ ft/s}$$

A_2 refers to the cross-sectional area of the nozzle, which is how we find diameter

Also

$$\begin{aligned} \gamma_m / \gamma_L &= \rho_m / \rho_L \\ &= 13.54 / 0.93 \\ &= 14.56 \end{aligned}$$

$$A_2 = \frac{A_1}{\sqrt{\frac{2gh \left(\frac{\gamma_m}{\gamma_L} - 1 \right)}{\left(\frac{V_1}{C} \right)^2 + 1}}}$$

all variables

available

except C and A_2 How to find last unknown C :Using largest flow rate $2.23 \text{ ft}^3/\text{s}$ Guess $C = 0.95$, check work

$$A_2 = 0.077 \text{ ft}^2$$

Maybe?

$$\text{If } A = 0.077 \text{ ft}^2 = \pi (d/2)^2 \Rightarrow d = 0.313 \text{ ft} \quad \text{Check}$$

Now check V

$$\begin{aligned} \text{M Np} &= \frac{VD\rho}{\eta} = \frac{(17.23 \text{ ft/s})(0.667 \text{ ft})(1.8 \text{ slugs/ft}^3)}{6.91 \times 10^{-4} \text{ lb-s/ft}^2} \\ &= 36738 \end{aligned}$$

and using Fig 15.5

$$C = 0.93$$

down with $C = 0.93$

$$C = .93$$

$$A_2 = A_1 \sqrt{\frac{2\gamma\eta[(\gamma_2/\gamma_1) + 1]}{(\gamma_1/C)^2 - 1} + 1}$$

$$A_1 = .1259 \text{ ft}^2$$

$$\eta = 32.2 \text{ ft/s}^2$$

$$\eta = 2/3 \text{ ft}$$

$$V_1 = 17.7 \text{ ft/s}$$

$$C = .93$$

$$\gamma_2/\gamma_1 = 13.54 / .93$$

$$A_2 = .078 \text{ ft}^2$$

$$d = \sqrt{\left(\frac{.078 \text{ ft}^2}{\pi}\right)} \cdot 2$$

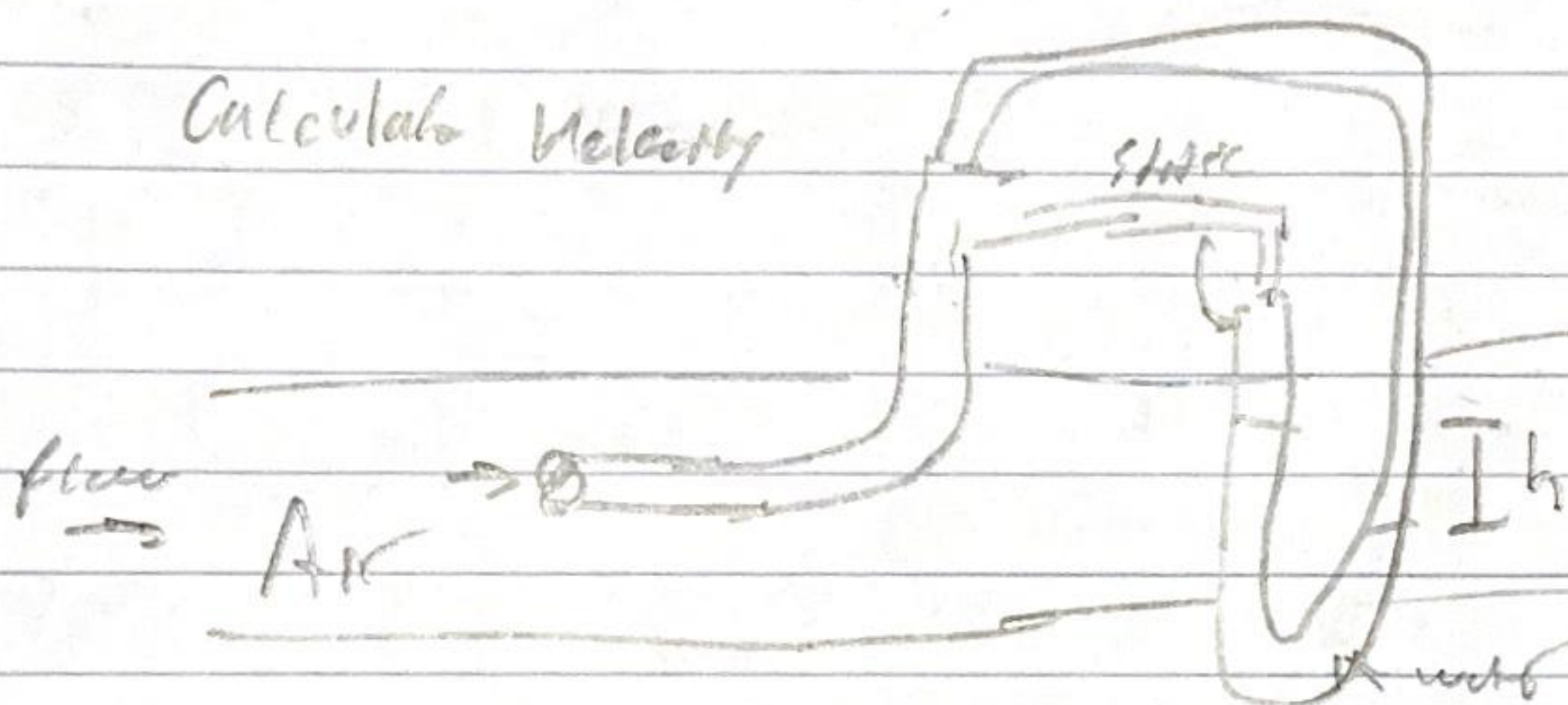
$$d = .315 \text{ ft}$$

Conclusion. appropriate nozzle diameter
would be .315 ft

15-151 a pitot-static probe is used to determine the velocity of air at standard conditions and a temperature of 120°F .

A manometer reads 0.24 m of water.

Calculate Velocity



Let's say 120°F , close to 30°C from last question (15-14)

$$V_1 = \sqrt{2gh(\gamma_g - \gamma)/\gamma}$$

where $h = 0.24 \text{ m} = 0.79 \text{ ft}$

$$g = 32.2 \text{ ft/s}^2$$

$$\gamma_g = 61.7 \text{ lb/ft}^3 \text{ for water at } 120^\circ\text{F} \text{ [APPA]}^{1.2}$$

$$\gamma = 0.0685 \text{ lb/ft}^3 \text{ for air at } 120^\circ\text{F} \text{ [APPE]}^{1.2}$$

$$V_1 = \sqrt{2(32.2 \text{ ft/s}^2)(0.79 \text{ ft})[(61.7 - 0.0685) / 0.0685]}$$

Conclusion

$$= 34 \text{ ft/s}$$

Seems like a realistic answer

34 ft/s is how fast the air is moving (Velocity of flow)