

Curtis Domingues Exam 3 April 10 (problem 2 chosen)

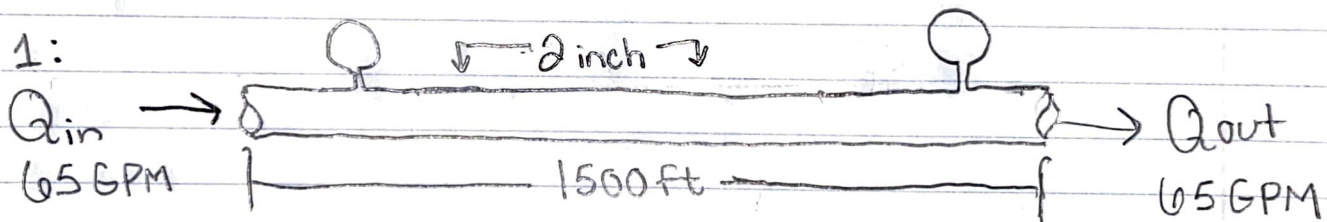
> Problem 2

> Purpose: Part 1: Determine the corresponding pressure drop associated with the 1500 ft 2-inch steel tubing given a flow rate of 65 GPM.

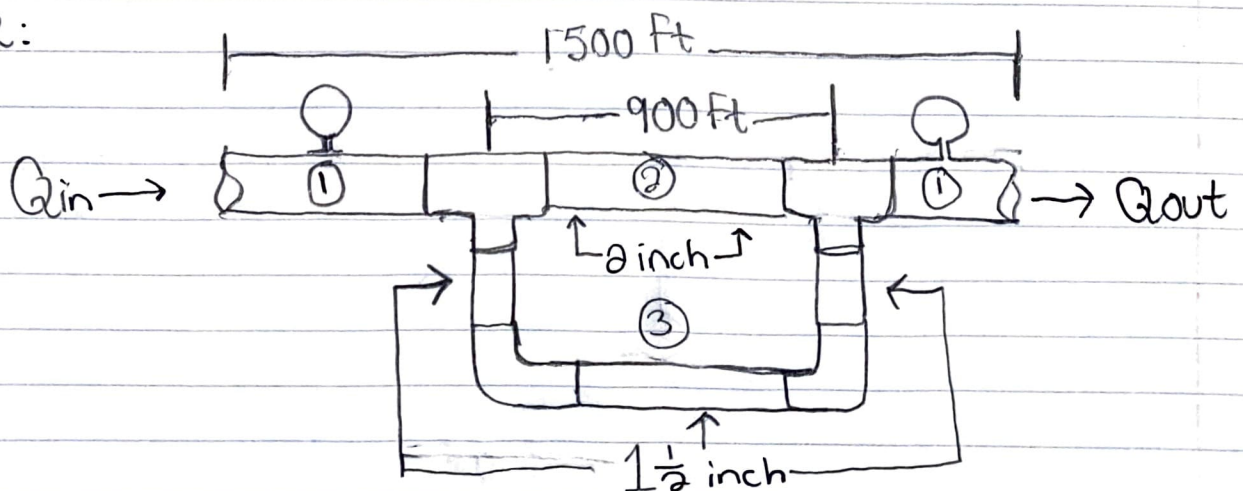
Part 2: Determine the expected increase in flow rate given a 900 ft loop of 1 1/2 inch steel tubing is added to the system, and pressure drop is unchanged.

> Drawings & Diagrams:

Part 1:



Part 2:



> Sources: Mott & Untener. Applied Fluid Mechanics. 7th Edition. Pearson 2015

> Design Consideration:

- 1) Incompressible fluid (water)
- 2) Constant "pressure change" (ΔP)
- 3) Isothermal process (70°F)
- 4) Steady state

> Data & Variables: Table G.1 pg. 508 Table A.2 pg 489

Tubing

2-inch:

$$\text{Flow area} = 1.907 \times 10^{-2} \text{ ft}^2$$

$$\text{Length} = 1500 \text{ ft}$$

$$\text{Diameter} = 1.870 \text{ in} = .1558 \text{ ft}$$

$$E = 5.0 \times 10^{-6} \text{ ft}$$

1½ inch

$$\text{Flow area} = 1.024 \times 10^{-2} \text{ ft}^2$$

$$\text{Length} = 900 \text{ ft}$$

$$\text{Diameter} = 1.370 \text{ in} = .1142 \text{ ft}$$

Water @ 70°F

$$\text{Density} = 1.94 \text{ slugs/ft}^3 = 1.94 \text{ lb-s/ft}^3$$

$$\gamma = 62.3 \text{ lb/ft}^3$$

$$\mu = 2.04 \times 10^{-5} \text{ lb-s/ft}^2$$

$$\nu = 1.05 \times 10^{-5} \text{ ft}^2/\text{s}$$

> Materials:

Standard steel tubing

Water

Fittings

> Procedure 3 Calculations

Let us begin by applying Bernoulli's equation to solve for the change in pressure for part 1.

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_{L_{1 \rightarrow 2}} \quad (1)$$

As height and velocity are constant, Bernoulli's can be rewritten as:

$$\frac{P_1}{\gamma} - \frac{P_2}{\gamma} = h_{L_{1 \rightarrow 2}} \quad \text{or} \quad \Delta p = \gamma [h_{L_{1 \rightarrow 2}}] \quad (2)$$

Thus, change in pressure is equal to γ_{water} times the total energy loss within the pipe.

To solve for h_L , we will need to calculate f , which will require solving for Reynolds number and D/ϵ .

$$D/\epsilon = \frac{.1558 \text{ ft}}{5.0 \times 10^{-6} \text{ ft}} = \boxed{31160}$$

$$N_R = \frac{VD}{\nu} \quad \nu = \frac{Q}{A}$$

$$Q = 65 \text{ GPM} \cdot \frac{1 \text{ ft}^3/\text{s}}{449 \text{ GPM}} = .144 \text{ ft}^3/\text{s}$$

$$V = \frac{.144 \text{ ft}^3/\text{s}}{.01907 \text{ ft}^2} = 7.59 \text{ ft/s}$$

$$N_R = \frac{(7.59)(.1558)}{1.05 \times 10^{-5}}$$

$$\boxed{N_R = 112621.14}$$

↳ solve for f

> Calculations Continued...

$$f = \frac{.25}{\left[\log\left(\frac{1}{3.7(D/\epsilon)} + \frac{5.74}{N_R^{.9}}\right) \right]^2} = \frac{.25}{\left[\log\left(\frac{1}{3.7(31160)} + \frac{5.74}{112621.14^{.9}}\right) \right]^2}$$

$$f = \frac{.25}{\left[\log(8.6736E^{-6} + 1.631E^{-4}) \right]^2} \quad f = \frac{.25}{14.1755} \quad \boxed{f = .0176}$$

Now that f is known, we shall plug the known values into "Darcy's Equation" and solve for total energy loss.

$$h_L = f \times \frac{L}{D} \times \frac{V^2}{2g} = (.0176) \times \frac{1500 \text{ ft}}{.1558 \text{ ft}} \times \frac{7.59 \text{ ft/s}^2}{2(32.2 \text{ ft/s}^2)}$$

$$h_L = 169.448 \times \frac{57.61 \text{ ft}^2/\text{s}^2}{64.4 \text{ ft/s}^2}$$

$$\boxed{h_L = 151.58 \text{ ft}}$$

Now that h_L is calculated, we will plug into Bernoulli's and solve for the change in pressure.

$$\Delta p = \gamma [h_{L_{1-2}}] = 62.3 \text{ lb/ft}^3 [151.58 \text{ ft}] = 9443.43 \text{ lb/ft}^2$$

Thus, Δp is equal to $\boxed{9443.43 \text{ PSF or } 65.58 \text{ PSI}}$

ANS

Calculations & Procedure Continued...

Part 2:

To determine the expected increase in flow rate, we will determine the minor losses added to the system and derive the 3 flow rates generated by the 3 sections of the pipe system. Since $Q_{in} = Q_{out}$, summing the two new flow rates will result in the new total flow. Thus,

$$Q_1 = Q_2 + Q_3 \quad \textcircled{I}$$

Next, we will manipulate Bernoulli's Equation to solve for Q_2 and Q_3 . The two resulting equations will be in terms of Q_1 , which is also unknown, therefore Q_1 must be assumed and solved through iteration.

$$Q_2) \quad \frac{\Delta P}{\gamma} = \left(f_1 \frac{L_1}{D_1} + 2K_{Tee (run)} \right) \frac{8Q_1^2}{g\pi^2 D_1^4} + \left(f_2 \frac{L_2}{D_2} \right) \frac{8Q_2^2}{g\pi^2 D_2^4}$$

$$Q_3) \quad \frac{\Delta P}{\gamma} = \left(f_1 \frac{L_1}{D_1} + 2K_{Tee (branch)} \right) \frac{8Q_1^2}{g\pi^2 D_1^4} + \left(f_3 \frac{L_3}{D_3} + 2K_{Elbow} \right) \frac{8Q_3^2}{g\pi^2 D_3^4}$$

NOTE: This procedure neglects the presence of "reducers" as they are not present in the problem statement. Solving for Q_2 & Q_3 yields:

$$Q_2 = \sqrt{\frac{\frac{\Delta P}{\gamma} - \left(f_1 \frac{L_1}{D_1} \right) \frac{8Q_1^2}{g\pi^2 D_1^4}}{\left(2K_{Tee run} + f_2 \frac{L_2}{D_2} \right) \frac{8}{g\pi^2 D_2^4}}}$$

II

$$Q_3 = \sqrt{\frac{\frac{\Delta P}{\gamma} - \left(f_1 \frac{L_1}{D_1} \right) \frac{8Q_1^2}{g\pi^2 D_1^4}}{\left(2K_{Tee brch} + 2K_{Elb} + f_3 \frac{L_3}{D_3} \right) \frac{8}{g\pi^2 D_3^4}}}$$

III

Part 2 Calculations Continued...

I will start the iteration process, NOTE: Full iteration will be in the form of an excel sheet and attached to this document.

Assume						Assume				solve	
Q1	NR1	D/E1	F1	F+1	Number	F2	D/E2	F+2	DEN2	Q2	
.15	1.19E5	3.18E4	1.74E-2	9.73E-3	9.28E1	.02	3.18E4	9.73E3	4.5E3	.143	
↓	↓	↓	↓	↓	↓	.0175	↓	↓	3.9E3	.153	
↓	↓	↓	↓	↓	↓	.0173	↓	↓	↓	.154	
↓	↓	↓	↓	↓	↓	.0173	↓	↓	↓	.154	
↓	↓	↓	↓	↓	↓	.0173	↓	↓	↓	.154	

New				Assume				solve			
V2	NR2	F2	% Diff	F3	D/E3	F+3	DEN3	Q3	V3	NR3	
7.53	1.14E5	1.7E-2	-3%	.02	2.28E4	1.03E-2	2.35E4	.0628	6.16	6.7E4	
8.03	1.21E5			1.9E-2	↓	↓	2.31E4	.0633	6.21	6.76E4	
8.08	1.22E5			1.96E-2	↓	↓	↓	.0634	6.22	↓	
8.08	1.22E5	1.735E-2	-.01%	1.96E-2	↓	↓	↓	.0634	6.22	↓	

New		New	
F3	% Diff	Q1	% Diff "Q1"
1.97E-2	-2%	.218	45%
1.96E-2			
↓	0.0%		

NOTE: This represents one complete iteration. Variables assumed: Q1, F2 and F3. As N_k is dependant on velocity which is dependant on Q. Thus, assuming F2 and F3 and reiterating will result in solving for Q2 & Q3 which sum to equal Q1 new.

Calculations Continued...

As shown in the attached excel sheet, this iteration was repeated 6 times, until a sufficient level of precision was reached. After 6 iterations Q_1 "new" was found to be $\boxed{.183 \text{ ft}^3/\text{s}}$ with a percent error of .07%

Thus, $Q_2 = .1295 \text{ ft}^3/\text{s}$ and $Q_3 = .0532 \text{ ft}^3/\text{s}$.

plugging into equation (I) $.1295 + .0532 = .183 \text{ ft}^3/\text{s} = Q_1$

Finally, given the original flow rate from part 1 was $.144 \text{ ft}^3/\text{s}$, the expected increase of flow rate is:

$$.183 - .144 = .039 \text{ ft}^3/\text{s} \text{ increase in flow rate}$$

or

17.5 GPM

ANS

> Summary:

The change in pressure from part 4 was calculated to be 9443.43 PSF. Using this same pressure change in part 2, Q_1 was assumed to be $.15 \text{ ft}^3/\text{s}$, but through iteration it was proved to actually be $.183 \text{ ft}^3/\text{s}$.

Thus, the expected increase in flow rate is roughly 17.5 GPM.

> Analysis:

The values obtained seem to be justified in that they do make sense within the system given the slight modifications made. It should be noted however, this procedure did not account for reduction fittings within the system. Therefore, in real-world applications the expected increase would be slightly lower as there would be more energy loss within the system. Since no reduction fittings were present in the problem, I assumed they were negligible. (This could be easily fixed by adding in the two reducers).