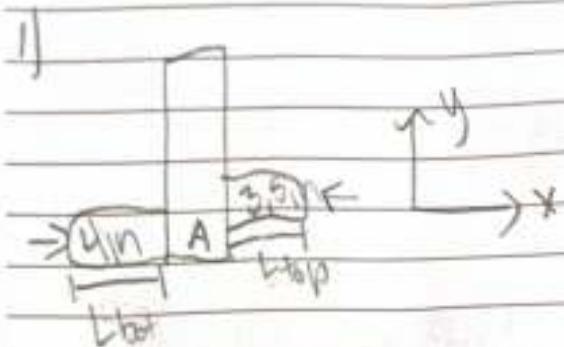


MET 330 Test 3 Main Ferguson UIN 01184025



design

inertial sys  
1st law

steady state

data

$4\text{in} \times 4\text{in} L_{bat}$

$3.5\text{in} \times 4\text{in} 4\text{in}$

$T = 71^\circ\text{F}, \rho = 0.0747 \text{ lb/ft}^3$

$V = 80 \text{ m/h} = 117.3 \text{ ft/s}$

UIN 01184025 1st law

$L_{bat} = 2\text{ft}$

$L_{op} = 1\text{ft}$

purpose  
Compute the moment of  
the pole compressed by 2 cylinders  
at point A.

calculations

$$T_A = \rho Q(V_{x_0} - V_{x_1})$$

$$\frac{P_1 + V_1^2}{\gamma} + z_1 = \frac{P_2 + V_2^2}{\gamma} + z_2 + h$$

$$T_x = \rho Q(V_{x_2} + V_{x_1})$$

$$V_1 = \sqrt{V_{x_1}^2 + 2g(z_1 - z_2)}$$

$$P_x = \rho A \sqrt{V_{x_1}^2 + 2g(z_1 - z_2) + V_1}$$

$$V_2 = 108.6 \text{ ft/s}$$

$$Q = V \left( \frac{\pi D^2}{4} \right) = 117.3 \pi \left( \frac{4.5}{12} \right)^2 = 6.48 \text{ ft}^3/s$$

$$P_x = 0.0747 \text{ lb/in}^2 (6.48 \text{ ft}^3/s) \left( \frac{117.3 \text{ ft/s}}{12} \right) + 117.3$$

$$P_x = 59.03 \text{ lb}$$

$$\Sigma m = 0$$

$$F_x(d_{1x}) + \rho Q V_x(d_2) - \rho Q V(d_1) = 0$$

$$d_{1x} = \frac{\rho Q V(d_2) + \rho Q V(d_1)}{F_x}$$

$$= -0.949(6.48)108.173 + 0.942(6.48)111.5(4) \\ 57.03$$

$$d_{1x} = 0.761 \text{ in}$$

$$M = F_x(d_{1x}) = 57.03 \left( \frac{0.761}{12} \right) = 3.617 \text{ ft/lb}$$

### Summary

The reaction force is 57.03 lb and the produced moment is 3.617 ft/lb.

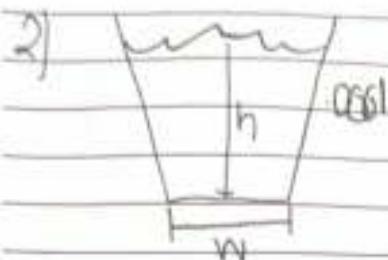
### material

Air

4 in Schedule 40 steel pipe  
3.5 in schedule steel pipe

### Source

Matt, R. Hentzur, SA, "Applied fluid Mechanics," 7th edition, Pearson Education Inc (2015)



design considerations  
incompressible fluid  
open channel

data

UTN 0104625 2nd from right  
 $W = 18\text{ft}$

$$Q = 360 \text{ A } \frac{\text{ft}^3}{\text{s}}$$

$$S = 0.0001$$

$$n \text{ cement} = 0.017 \text{ from table 14.1}$$

purpose

Calculate the height of the open channel with the data provided. Using Manning's equation and since we can get  $A$

calculations

$$A = 12(h) + X(h^2) = 12h + h^2$$

$$A = \frac{12h}{1.495^{1/2}}$$

$$R = \frac{A}{P} = \frac{A}{2\sqrt{2}h^2 + 12}$$

$$12h + h^2 \left( \frac{(12h + h^2)}{2\sqrt{2}h + 12} \right)^{2/3} = nq$$

$$\frac{(12h + h^2)^{5/3}}{(2\sqrt{2}h + 12)^{2/3}} = \frac{0.017 \times 50(1/3)}{1.49(0.001)^{1/2}} = 309.3$$

$$\text{Using Excel } h = 0.56785\text{ft}$$

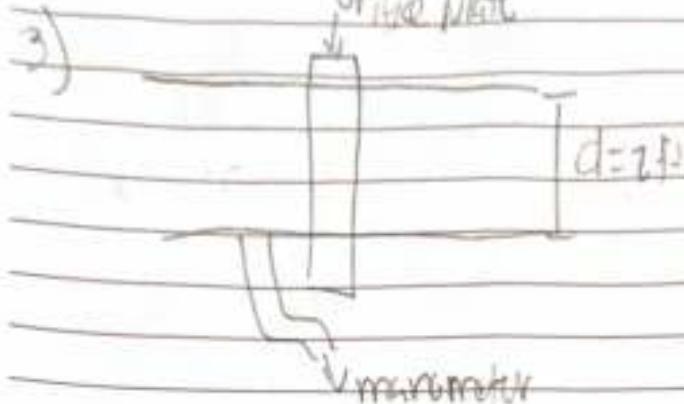
Summary

By using Manning's equation getting both sides solved for  $h$  and solving out for the percentage difference the height is calculated to  $0.56785\text{ft}$  for a 0.0171 difference.

source

Mohr R, Ullman J.A. "Applied Fluid Mechanics, 9th edition Design"

principle



design

magnetizable  
isothermal  
steady state

data

$$\beta = 0.5$$

$U_{MN}$  3rd from right

$$D = 18.4 \text{ in}$$

$$Q = 12060 \text{ cfm} = 26.74 \text{ ft}^3/\text{s}$$

$$D = 24 \text{ in} \quad 46 = 2 \text{ ft}$$

$$A = 2.79 \text{ ft}^2$$

$$y_m = 844.9 \text{ lb/ft}^3$$

$$y_w = 62.4 \text{ lb/ft}^3$$

$$g = 32.2 \text{ ft/s}^2$$

$$V_1 = C \sqrt{\frac{2gh(y_m - y_w) - 1}{(A_1 - A_2)^2 - 1}}$$

$$h = \left( \frac{V_1}{C} \right)^2 \left( \frac{(D/16)^4 - 1}{2g(y_m - y_w) - 1} \right)$$

$$C = .9975 \cdot 1.5 \cdot \sqrt{A/\rho_e}$$

$$= .9975 \cdot 1.5 \cdot \sqrt{21.94 \cdot 10^{-7}}$$

$$= .9965$$

$$= \left( \frac{9.57}{0.015} \right)^2 \left( \frac{21^4 - 1}{2(32.2)(\frac{844.9}{62.4} - 1)} \right)$$

$$V_C = \frac{V_D}{\sqrt{8912 \text{ in}^{-2}}} = 9.57(21)$$

$$= 2.14 \times 10^3$$

$$h = 92.229(15/807.52)$$

$$V = Q = \frac{21.94}{2.14 \times 10^3} = 9.57 \text{ ft/s}$$

$$h = 1.713 \text{ ft}$$

$$\beta = d/D$$

$$d = \beta(D) = .5(24) = 12 \text{ in}$$

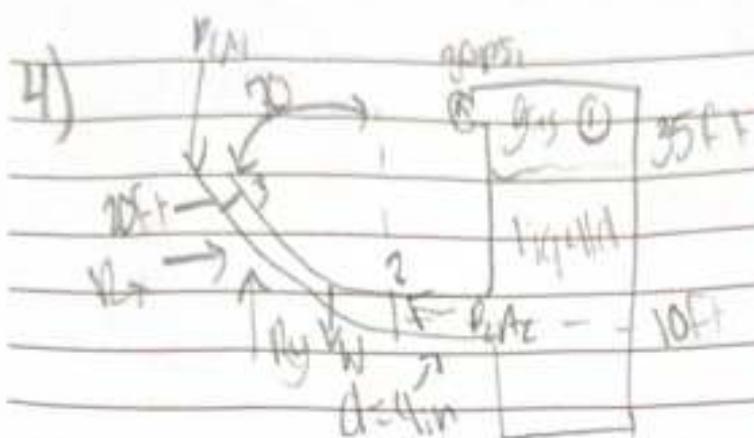
### Summary

The mercury manometer range was found by using the equation in solve for height. The range is 0 - 1.713 ft.

### Material Mercury

### Source

Mill R, Unitpr, J.A "Applied Fluid Mechanics", 7th edition  
Pearson Education 2015



derivation  
incompressible  
inertial  
steady state

Eqn.  
 $y = 55 \text{ lb/ft}^3$

$4 \text{ in } D \times 10 \text{ ft } L$   
from right  
 $L_{\text{curved}} = 10 \text{ ft}$   
 $n = 30 \text{ rad/s} = 452 \text{ rad/s}$   
 $\rho = 173 \text{ slug/s}$

### Procedure

compute the force on the curved pipe and provide the magnitude and direction.

### Simplifications

$$F_x = \rho Q (V_2 - V_1)$$

$$R_x = p_1 A_1 - p_2 A_2 \cos 70^\circ - \rho Q V_2 \cos 70^\circ + \rho Q V_1$$

$$F_y = \rho Q (V_{ay} - V_{iy})$$

$$R_y = p_2 A_2 \sin 70^\circ - \rho Q V_2 \sin 70^\circ$$

$$A_1 = \frac{\pi}{4} 4 \text{ in}^2 = 0.02513 \text{ ft}^2 \quad A_2 = \frac{\pi}{4} 3 \text{ in}^2 = 0.049 \text{ ft}^2$$

$$p_2 = p_1 + \gamma (V_1^2 - V_2^2) / 2g$$

$$P_1 A_1 = 4320(0.0218)$$

$$P_2 A_2 = 90.24(0.049)$$

$$P_2 V_1 = 55(1.129)51.8$$

$$P_2 V_1 = 55(1.129)23.05$$

$$V = \sqrt{\frac{P_x}{P A_1 (0.0218 + 1)}} = \sqrt{\frac{4320}{55(0.0218)(0.0218 + 1)}} = 51.8 \text{ ft/s}$$

$$V_2 = V_1 \left( \frac{A_1}{A_2} \right) = 51.8 \left( \frac{0.0218}{0.049} \right) = 23.05 \text{ ft/s}$$

$$P_2 = P_1 + \gamma (V_1^2 - V_2^2) / 2g$$

$$= 4320 + 55(51.8 \cdot 23.05) / 2(32.2) = 90.24$$

$$Q = AV = 51.8(0.0218) = 1.129$$

$$P_x = 4320(0.0218) \sin 70 - 55(1.129)(13.65) \cos 70 + 55(1.129)51.8$$

$$P_x = 28154.81 \text{ lb/ft positive right}$$

$$P_y = 4320(0.0218) \sin 70 - 55(1.129)23.05 \sin 70$$

$$P_y = 1240.81 \text{ lb/ft down negative}$$

## Natural Curved pipe

### Source

Munro R, Uritskur, JA, "Applied Fluid Mechanics," 7th Edition Pearson Education Inc (2015)

### Summary

The force on the length of the curved pipe in the x direction is  $2815.48 \text{ lb/ft}$  in the positive direction. The force in the y direction is negative  $-340.8 \text{ lb/ft}$

Steel

KSIAN  
incompressible  
isothermal  
sticky state

Purpose:

Calculate the pressure increment  
before the valve suddenly closes

data

(IN DIP4025 Standard)

D = 300 mm

V = 1.0 m/s

C = 100 mm

E =  $2 \times 10^5$  N/m<sup>2</sup>

E<sub>0</sub> =  $2.03 \times 10^5$  N/m<sup>2</sup>

$\rho$  = 1000 kg/m<sup>3</sup>

Calculations

$$\Delta p = \rho V C$$

$$C = \frac{E_0 / \rho}{1 + \frac{E_0 / D}{E(D)}} = \frac{2.03 \times 10^5 / 1000}{1 + \frac{2.03 \times 10^5 / 300 \text{ mm}}{2 \times 10^7 \text{ (100 mm)}}} = 1639.52 \text{ m/s}$$

$$\Delta p = 1000 \text{ kg/m}^3 (1639.52) 1.0 \text{ m/s} = 1.64 \times 10^6 \text{ Pa}$$

Material

Steel pipe  
gauge

Murphy, J.M. Applied Fluid Mechanics, 7th edition Pearson Education 2015

Summary

The pressure increment before the valve closes is  
 $1.64 \times 10^6 \text{ Pa}$

Honor Code: Mechatronics