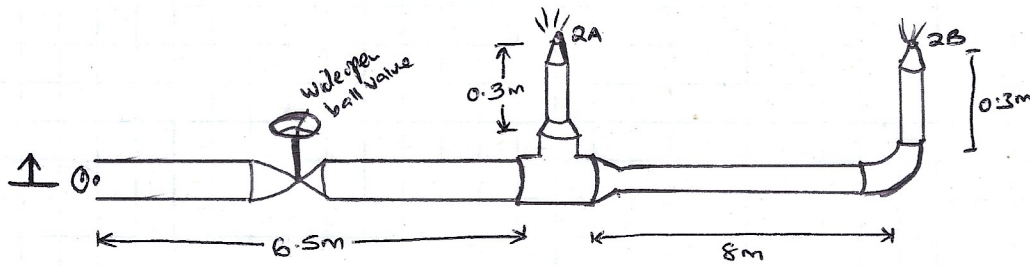


Problem 1

$$P_1 = 400 \text{ kPa}$$

$$K_{\text{g. sprinkler}} = 50$$

$$K_{\text{g. ball valve}} = 3 \text{ ft}$$

Water at 20°C (room temperature)

$$\gamma = 9790 \text{ N/m}^3$$

$$\nu = 1.02 \times 10^{-6}$$

Schedule 40 pipe

$$D_1 = 0.0409 \text{ m}$$

$$f_1 = 0.020$$

$$D_{2A} = D_{2B} = 0.0266 \text{ m}$$

$$f_1 = 0.022$$

$$\epsilon = 4.6 \times 10^{-5}$$

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + Z_1 = \frac{P_{2A}}{\gamma} + \frac{V_2^2}{2g} + Z_2 + h_{L1-2}$$

$$\frac{P_1}{\gamma} - Z_2 = \frac{V_2^2}{2g} - \frac{V_1^2}{2g} + h_{L1-2}$$

For each branch

branch 2A

$$\frac{P_1}{\gamma} - Z_{2A} = \frac{V_{2A}^2}{2g} - \frac{V_1^2}{2g} + h_{L1-2A}$$

branch 2B

$$\frac{P_1}{\gamma} - Z_{2B} = \frac{V_{2B}^2}{2g} - \frac{V_1^2}{2g} + h_{L1-2B}$$

$$h_{L1-2A} = h_{\text{pipe } 1} + h_{\text{valve } 1} + h_{\text{tee } 1} + h_{\text{connection } 2A} + h_{\text{pipe } 2A} + h_{\text{sprinkler } 2A}$$

$$= f_1 \frac{L_1}{D_1} \frac{V_1^2}{2g} + K_{\text{valve}} \frac{V_1^2}{2g} + K_{\text{tee}} \frac{V_1^2}{2g} + K_{\text{cont.}} \frac{V_{2A}^2}{2g} + f_{2A} \frac{L_{2A}}{D_{2A}} \frac{V_{2A}^2}{2g} + K_{\text{sprinkler}} \frac{V_{2A}^2}{2g}$$

$$h_{L1-2B} = h_{\text{pipe } 1} + h_{\text{valve } 1} + h_{\text{tee } 1} + h_{\text{connection } 2B} + h_{\text{pipe } 2B} + h_{\text{elbow } 2B} + h_{\text{sprinkler } 2B}$$

$$= f_1 \frac{L_1}{D_1} \frac{V_1^2}{2g} + K_{\text{valve}} \frac{V_1^2}{2g} + K_{\text{tee}} \frac{V_1^2}{2g} + K_{\text{cont.}} \frac{V_{2B}^2}{2g} + f_{2B} \frac{L_{2B}}{D_{2B}} \frac{V_{2B}^2}{2g} + K_{\text{elbow}} \frac{V_{2B}^2}{2g} + K_{\text{sprinkler}} \frac{V_{2B}^2}{2g}$$

$$h_{L1-2A} = \left(f_1 \frac{L_1}{D_1} + K_{\text{valve}} + K_{\text{tee}} \right) \frac{V_1^2}{2g} + \left(K_{\text{connection}} + f_{2A} \frac{L_{2A}}{D_{2A}} + K_{\text{sprinkler}} \right) \frac{V_{2A}^2}{2g}$$

$$h_{L1-2B} = \left(f_1 \frac{L_1}{D_1} + K_{\text{valve}} + K_{\text{tee}} \right) \frac{V_1^2}{2g} + \left(K_{\text{cont.}} + f_{2B} \frac{L_{2B}}{D_{2B}} + K_{\text{elbow}} + K_{\text{sprinkler}} \right) \frac{V_{2B}^2}{2g}$$

$$V = \frac{4Q}{\pi D^2} \Rightarrow V^2 = \frac{16Q^2}{\pi^2 D^4}$$

The equation become

$$h_{L1-2A} = \left(f_1 \frac{L_1}{D_1} + K_{valve} + K_{tee} \right) \frac{8}{g\pi^2 D_1^4} Q_1^2 + \left(K_{cont} + f_{2A} \frac{L_{2A}}{D_{2A}} + K_{pinch} \right) \frac{8}{g\pi^2 D_{2A}^4} Q_{2A}^2$$

$$h_{L1-2B} = \left(f_1 \frac{L_1}{D_1} + K_{valve} + K_{tee} \right) \frac{8}{g\pi^2 D_1^4} Q_1^2 + \left(K_{cont} + f_{2B} \frac{L_{2B}}{D_{2B}} + K_{elbow} + K_{pinch} \right) \frac{8}{g\pi^2 D_{2B}^4} Q_{2B}^2$$

The original equation was

$$\left(\frac{P_1}{\gamma} - Z_{2A} \right) = \frac{V_{2A}^2}{2g} - \frac{V_1^2}{2g} + h_{L1-2A} = \frac{8}{g\pi^2 D_{2A}^4} Q_{2A}^2 - \frac{8}{g\pi^2 D_1^4} Q_1^2 + h_{L1-2A}$$

Which can be simplified as

$$\left(\frac{P_1}{\gamma} - Z_{2A} \right) = \left(f_1 \frac{L_1}{D_1} + K_{valve} + K_{tee} - 1 \right) \frac{8}{g\pi^2 D_1^4} Q_1^2 + \left(K_{cont} + f_{2A} \frac{L_{2A}}{D_{2A}} + K_{pinch} + 1 \right) \frac{8}{g\pi^2 D_{2A}^4} Q_{2A}^2$$

$$Q_{2A} = \sqrt{\frac{\left(\frac{P_1}{\gamma} - Z_{2A} \right) - \left(f_1 \frac{L_1}{D_1} + K_{valve} + K_{tee} - 1 \right) \frac{8}{g\pi^2 D_1^4} Q_1^2}{\left(K_{cont} + f_{2A} \frac{L_{2A}}{D_{2A}} + K_{pinch} + 1 \right) \frac{8}{g\pi^2 D_{2A}^4}}}$$

Similarly

$$\left(\frac{P_1}{\gamma} - Z_{2B} \right) = \frac{V_{2B}^2}{2g} - \frac{V_1^2}{2g} + h_{L1-2B} = \frac{8}{g\pi^2 D_{2B}^4} Q_{2B}^2 - \frac{8}{g\pi^2 D_1^4} Q_1^2 + h_{L1-2B}$$

Simplified to

$$\left(\frac{P_1}{\gamma} - Z_{2B} \right) = \left(f_1 \frac{L_1}{D_1} + K_{valve} + K_{tee} - 1 \right) \frac{8}{g\pi^2 D_1^4} Q_1^2 + \left(K_{cont} + f_{2B} \frac{L_{2B}}{D_{2B}} + K_{pinch} + K_{elbow} \right) \frac{8}{g\pi^2 D_{2B}^4} Q_{2B}^2$$

$$Q_{2B} = \sqrt{\frac{\left(\frac{P_1}{\gamma} - Z_{2B} \right) - \left(f_1 \frac{L_1}{D_1} + K_{valve} + K_{tee} - 1 \right) \frac{8}{g\pi^2 D_1^4} Q_1^2}{\left(K_{cont} + f_{2B} \frac{L_{2B}}{D_{2B}} + K_{elbow} + K_{pinch} \right) \frac{8}{g\pi^2 D_{2B}^4}}}$$

$$\text{But } Q_1 = Q_{2A} + Q_{2B}$$

Iteration procedure:

- * Guess f_{2A} and f_{2B}
- * Guess $Q_1 = Q_T$
- * Compute V_T , R_{2A} and f_T
- * Compute Q_{2A} and Q_{2B}
- * Compute R_{HS}
- * Compare R_{HS} with $LHS(\text{Guessed } Q_T)$ (% diff)
- * Compute R_{2A} and R_{2B}
- * Compute f_{2A} and f_{2B}
- * Compare f_{2A} and f_{2B} with guessed values (% diff)
- * Repeat the iteration using the computed f_{2A} , f_{2B} and $Q_T(R_{HS})$ until the % diff is acceptable.

Results

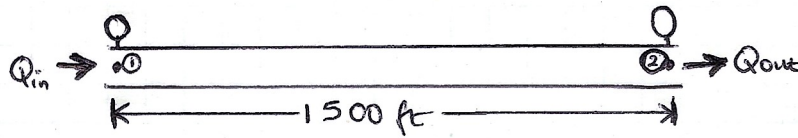
With a $R_{HS}-LHS$ % diff of 0.00%, $Q_{2A} = 0.00214 \text{ m}^3/\text{s}$ $V_{2A} = 3.86 \text{ m/s}$

$Q_{2B} = 0.00202 \text{ m}^3/\text{s}$ $V_{2B} = 3.63 \text{ m/s}$

$Q_T = 0.00416 \text{ m}^3/\text{s}$ $V_T = 3.166 \text{ m/s}$

- From the iterations, the flow through each sprinkler is relatively the same.
- The fluid velocity through the main pipe and through the sub-branches are very close to the critical velocity (3 m/s)

If the flow rates and/or the velocity were to be change, the most applicable way of altering them would be use valves. A different kind of valve can be installed in the main pipe that can be adjusted to affect the flow rate.

Problem 2 (GRADE THIS PROBLEM FOR TEST 3)

$$Q = 65 \text{ gpm} = 0.1448 \text{ ft}^3/\text{s}$$

Water at 70°F (room temperature)

$$\gamma = 62.3 \text{ lb/ft}^3$$

$$\nu = 1.05 \times 10^{-5} \text{ ft}^2/\text{s}$$

$$D = 2 \text{ in} = 0.1558 \text{ ft}$$

$$E = 1.5 \times 10^{-4} \text{ ft}$$

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + Z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + Z_2 + h_{L1-2}$$

$$\frac{P_1 - P_2}{\gamma} = h_{L1-2} = h_{L \text{ pipe } 1-2}$$

$$h_{L1-2} = f \frac{L}{D} \frac{V^2}{2g} \quad \text{but } V^2 = \frac{16Q^2}{\pi^2 D^4}$$

$$h_{L1-2} = f \frac{L}{D} \cdot \frac{8}{g \pi^2 D^4} Q^2$$

$$V = \frac{4Q}{\pi D^2} = \frac{4 \times 0.1448}{\pi (0.1558)^2}$$

$$V = 7.5953 \text{ ft/s}$$

$$f = \frac{0.25}{\left[\log \left(\frac{1}{3.7(D/E)} + \frac{5.74}{Re^{0.7}} \right) \right]^2}$$

$$\frac{D}{E} = \frac{0.1558 \text{ ft}}{1.5 \times 10^{-4}} = 1038.67$$

$$= \frac{0.25}{\left[\log \left(\frac{1}{3.7(1038.67)} + \frac{5.74}{(1.27 \times 10^5)^{0.7}} \right) \right]^2}$$

$$N_R = \frac{VD}{\nu} = \frac{7.5953 \times 0.1558}{1.05 \times 10^{-5}} = 1.127 \times 10^5$$

$$= 0.022$$

$$h_{L1-2} = 0.022 \times \frac{1500 \text{ ft}}{0.1558 \text{ ft}} \times \frac{8}{g \pi^2 (0.1558)^4} \times 0.1448^2$$

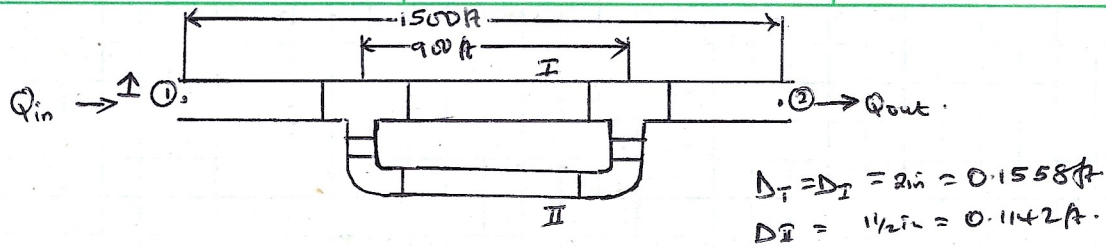
$$h_{L1-2} = 189.46 \text{ ft}$$

$$\frac{\Delta P}{\gamma} = 189.46 \text{ ft}$$

$$\Delta P = 189.46 \text{ ft} \times 62.3 \text{ lb/ft}^3$$

$$= 11803.358 \text{ lb/ft}^2 \times \frac{\text{ft}^2}{144 \text{ in}^2}$$

$$\Delta P = 81.97 \text{ psi}$$



$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + Z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + Z_2 + h_{L1-2}$$

$$\frac{P_1 - P_2}{\gamma} = h_{L1-2} \Rightarrow \frac{\Delta P}{\gamma} = h_{L1-2(I)}$$

$$\Rightarrow \frac{\Delta P}{\gamma} = h_{L1-2(II)}$$

$$h_{L1-2(I)} = h_{L\text{pipe I}} + 2h_{\text{tee I}} + h_{L\text{pipe II}}$$

$$= f_0 \frac{L_0}{D_0} \cdot \frac{V_0^2}{2g} + 2K_{\text{tee}} \cdot \frac{V_0^2}{2g} + f_I \frac{L_I}{D_I} \cdot \frac{V_I^2}{2g} \quad V^2 = \frac{16Q^2}{\pi^2 D^4}$$

$$h_{L1-2} = \left(f_0 \frac{L_0}{D_0} + 2K_{\text{tee}} \right) \frac{8}{g\pi^2 D_0^4} Q_0^2 + \left(f_I \frac{L_I}{D_I} \right) \cdot \frac{8}{g\pi^2 D_I^4} Q_I^2 = \frac{\Delta P}{\gamma}$$

$$Q_I = \sqrt{\frac{\frac{\Delta P}{\gamma} - \left(f_0 \frac{L_0}{D_0} + 2K_{\text{tee}} \right) \frac{8}{g\pi^2 D_0^4} Q_0^2}{f_I \frac{L_I}{D_I} \cdot \frac{8}{g\pi^2 D_I^4}}}$$

$$h_{L1-2(II)} = h_{L\text{pipe I}} + 2h_{\text{tee I}} + h_{L\text{connection II}} + h_{L\text{elbow II}} + h_{L\text{pipe II}}$$

$$= f_I \frac{L_I}{D_I} \frac{V_I^2}{2g} + 2K_{\text{tee}} \frac{V_I^2}{2g} + K_{\text{cont}} \frac{V_{II}^2}{2g} + K_{\text{elbow}} \frac{V_{II}^2}{2g} + K_{\text{elb}} \frac{V_{II}^2}{2g} + f_{II} \frac{L_{II}}{D_{II}} \frac{V_{II}^2}{2g} \quad V^2 = \frac{16Q^2}{\pi^2 D^4}$$

$$h_{L1-2(II)} = \left(f_I \frac{L_I}{D_I} + 2K_{\text{tee}} \right) \frac{8}{g\pi^2 D_I^4} Q_I^2 + \left(K_{\text{cont}} + K_{\text{elbow}} + K_{\text{elb}} + f_{II} \frac{L_{II}}{D_{II}} \right) \frac{8}{g\pi^2 D_{II}^4} Q_{II}^2 = \frac{\Delta P}{\gamma}$$

$$Q_{II} = \sqrt{\frac{\frac{\Delta P}{\gamma} - \left(f_I \frac{L_I}{D_I} + 2K_{\text{tee}} \right) \frac{8}{g\pi^2 D_I^4} Q_I^2}{\left(K_{\text{cont}} + K_{\text{elbow}} + K_{\text{elb}} + f_{II} \frac{L_{II}}{D_{II}} \right) \frac{8}{g\pi^2 D_{II}^4}}}$$

$$\text{Also } Q_1 = Q_I + Q_{II}$$

Iteration procedure

* Guess f_I & f_{II}

* Guess $Q_1 = Q_T$

* Compute V_I, R_{eI} & f_I

* Compute Q_I & Q_{II}

* Compute R_{eII}

* Compare R_{eII} with LHS (Guess Q_I)

* Compute R_{eI} & R_{eII}

* Compute f_I & f_{II}

* Compare f_I & f_{II} with the guessed values

* Repeat the procedure until the computed f_I, f_{II} & Q_T until 2 diff is acceptable.

Result

With R_{eI} -LHS 2 diff of 0.36%, $Q_I = 0.1218 \text{ ft}^3/\text{s}$

$$Q_{II} = 0.05 \text{ ft}^3/\text{s}$$

$$Q_T = 0.1712 \text{ ft}^3/\text{s}$$

$$\Delta Q_I = (0.1712 - 0.1448) \text{ ft}^3/\text{s} = 0.0264 \text{ ft}^3/\text{s}$$

$\therefore$ Apply a branch increase the flow rate by $0.0264 \text{ ft}^3/\text{s}$