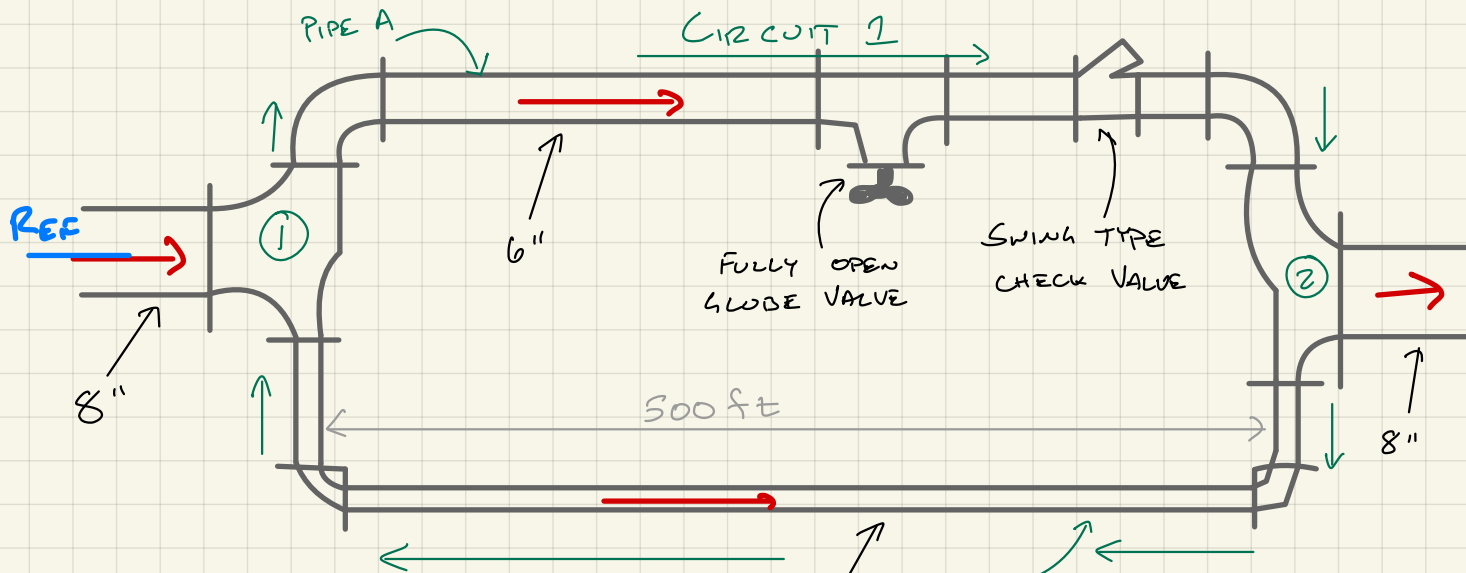


12-7

## GIVEN:

BENZENE IS FLOWING IN THE SYSTEM BELOW:



$$Q = 1350 \text{ gal/min (in 8")}$$

$$S_{g \text{ Ben}} = 0.87$$

$$T = 140^\circ\text{F}$$

ALL PIPES = SCH 40

$$\nu = 7.41 \cdot 10^{-6} \text{ ft}^2/\text{s}$$

$$\gamma = 54.55 \text{ lb/ft}^3$$

## REQUIRED

CALCULATE THE VOLUME FLOW RATE IN THE 6" AND 2" PIPES USING THE CROSS TECHNIQUE

## SOLUTION:

- STEP BY STEP HARDY CROSS METHOD:

1.  $h = KQ^2$  • SET UP HEADLOSS EQUATIONS FOR EACH PIPE

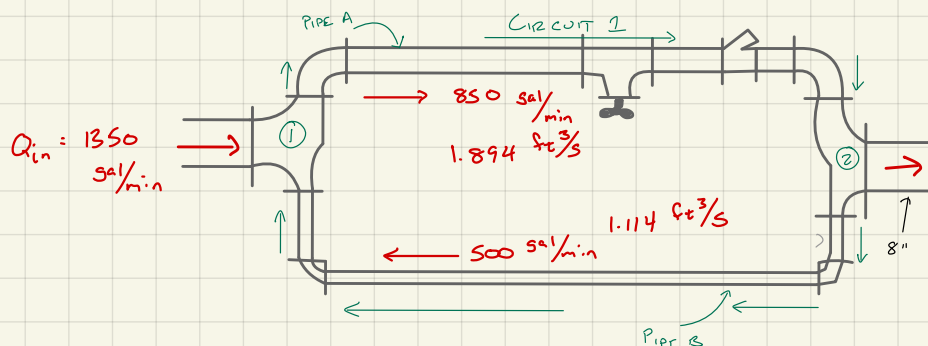
$$K = \frac{8(L + \sum L_e)}{\pi^2 g D^5} \quad \text{• THIS IS THE } K \text{ FOR } h = KQ^2, \text{ MINOR LOSSES ARE ACCOUNTED FOR W/ } L_e$$

$$L_{e_{1b}} = 30 \quad L_{e_{\text{slope}}} = 340 \quad L_{e_{\text{valve}}} = 100 \quad \text{• MINOR LOSSES IN PIPE A}$$

$$K_A = \frac{8(500 \text{ ft} + (2 \cdot 30 + 340 + 100) \text{ ft}) f_A}{\pi^2 (32.2 \text{ ft/s}^2) (0.5 \text{ ft})^5}$$

$$K_B = \frac{8(500 \text{ ft}) f_B}{\pi^2 (32.2 \text{ ft/s}^2) (0.1667 \text{ ft})^5}$$

2. GUESS FLOW RATE FOR EACH BRANCH SO THAT THE TOTAL EQUALS THE FLOW OUT OF THE JUNCTION

12-7  
CONT

- GUESSED 850 gal/min FOR PIPE A, 500 FOR PIPE B
- PIPE B IS GOING TO THE LEFT, SO ITS VALUE WILL BE NEGATIVE GOING FORWARD.

### 3. DIVIDE SERIES INTO CLOSED LOOPS

- THIS PARTICULAR SERIES ONLY HAS A SINGLE LOOP, LABELED CIRCUIT 1

### 4. FOR EACH PIPE, CALCULATE THE HEAD LOSS W/ ASSUMED Q.

PIPE A:

$$h_A = \frac{8(500\text{ft} + (2.30 + 340 + 100)\text{ft}) f_A \cdot (1.894\text{ft}^3/\text{s})^2}{\pi^2 (32.2\text{ft}/\text{s}^2) (0.5\text{ft})^5}$$

$$= 2889.64 f_A$$

$$f_A = \frac{0.25}{\left(\log\left(\frac{1}{3.7 \cdot D/\epsilon} + \frac{5.47}{Re^{0.9}}\right)\right)^2}$$

$$= \frac{0.25}{\left(\log\left(\frac{1}{3.7 \cdot 3333} + \frac{5.47}{(6.51 \cdot 10^5)^{0.9}}\right)\right)^2}$$

$$= \boxed{0.016}$$

$$Re = \frac{VD}{\nu} = \frac{4Q \cdot D}{\pi D^2 \cdot \nu}$$

$$= \frac{4(1.894\text{ft}^3/\text{s}) \cdot (0.5\text{ft})}{\pi (0.5)^2 \cdot 7.41 \cdot 10^{-6}\text{ft}^2/\text{s}} = 6.51 \cdot 10^5$$

$$\frac{D}{\epsilon} = \frac{0.5\text{ft}}{1.5 \cdot 10^{-4}\text{ft}} = 3333$$

$$h_A = 2889.64 \cdot 0.016 = \boxed{46.23\text{ft}}$$

PIPE B:

$$h_B = \frac{8(500\text{ft})(0.019) \cdot (1.114\text{ft}^3/\text{s})^2}{\pi^2 (32.2\text{ft}/\text{s}^2) (0.1667\text{ft})^5} = \boxed{2305.42\text{ft}}$$

$$f_B = \frac{0.25}{\left(\log\left(\frac{1}{3.7 \cdot 1111} + \frac{5.47}{(1.15 \cdot 10^6)^{0.9}}\right)\right)^2}$$

$$= 0.019$$

$$Re = \frac{4(1.114\text{ft}^3/\text{s})(0.1667\text{ft})}{\pi (0.1667\text{ft})^2 \cdot (7.41 \cdot 10^{-6}\text{ft}^2/\text{s})} = 1.15 \cdot 10^6$$

$$D/\epsilon = \frac{0.1667\text{ft}}{(1.5 \cdot 10^{-4}\text{ft})} = 1111\text{ft}$$

12-7  
cont

5. ALGEBRAICALLY SUM HEAD LOSSES TAKING DIRECTION INTO ACCOUNT

$$\sum h_i = h_A + h_B = \overset{\rightarrow}{46.23 \text{ ft}} + \overset{\leftarrow}{(-2305.42 \text{ ft})}$$

$$= -2259.19$$

6. CALCULATE  $2KQ$  FOR EACH PIPE

$$A = 2 \cdot 12.89 \cdot 1.894 \text{ ft}^3/\text{s} = 48.83$$

$$B = 2 \cdot 1857.72 \cdot 1.114 \text{ ft}^3/\text{s} = 4139$$

7. SUM ALL  $2KQ$  VALUES FOR EACH CIRCUIT, ASSUMING ALL POSITIVE VALUES

$$\sum 2KQ = 48.83 + 4139 = 4187.83$$

8. FOR EACH CIRCUIT, CALCULATE A  $\Delta Q$

$$\Delta Q = \frac{\sum h}{\sum 2KQ} = \frac{(-2259.19)}{(4187.85)} = -0.539$$

9. FOR EACH PIPE, CALCULATE A NEW ESTIMATED VALUE OF  $Q$

$$Q' = Q - \Delta Q$$

$$Q'_A = 1.894 - (-0.539) = 2.433$$

$$Q'_B = -1.114 - (-0.539) = -0.575$$

•  $Q_B$  IS NEGATIVE B/C IT FLOWS TO THE RIGHT  $\leftarrow$

10. REPEAT 4-8 UNTIL  $\Delta Q$  BECOMES NEGLIGIBLY SMALL

• STEP 10 COMPLETED IN EXCEL, SEE TABLE.

FINAL SOLUTION:

$$Q_A = 2.787 \text{ ft}^3/\text{s} \left( \frac{7.48052 \text{ gal} \cdot 60 \text{ s}}{1 \text{ ft}^3 \cdot 1 \text{ min}} \right) = 1250.89 \text{ gal/min}$$

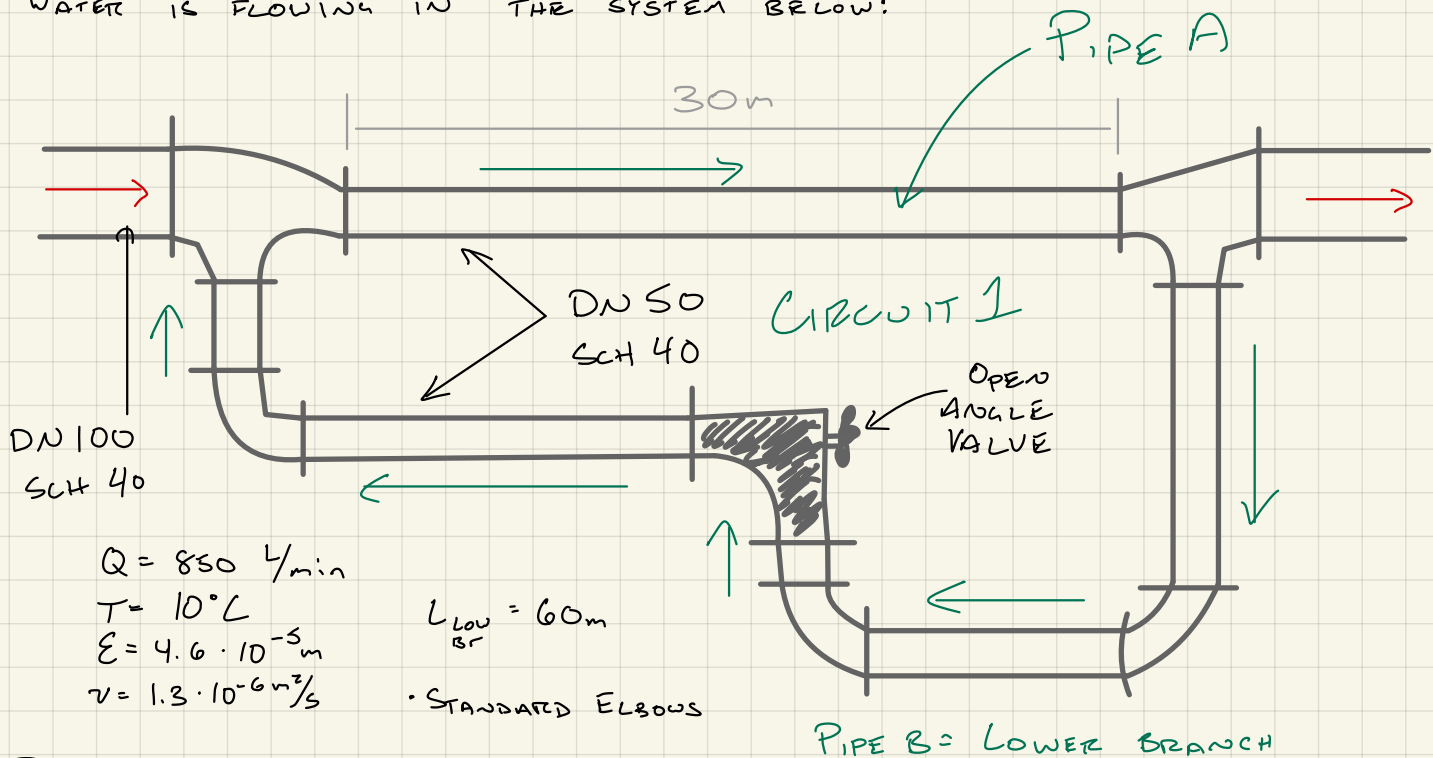
$$Q_B = 0.221 \text{ ft}^3/\text{s} \left( \frac{7.48052 \text{ gal} \cdot 60 \text{ s}}{1 \text{ ft}^3 \cdot 1 \text{ min}} \right) = 99.19 \text{ gal/min}$$

Initial:																
Circuit	Pipe	Q (gal/min)	Q (ft^3/s)	D (ft)	e (ft)	L (ft)	Le	D/e	V	Re	f	k	kQ^2	2kQ		Error %
1	A	850	1.894	0.500	1.50E-04	500	500	3.33E+03	9.645	6.51E+05	0.016	12.97	46.52	49.13		-28.505
	B	-500	-1.114	0.167	1.50E-04	500	0	1.11E+03	-51.062	1.15E+06	0.020	1909.81	-2370.09	4255.08	Delta Q	48.459
												Σ:	-2323.57	4304.21	-0.540	
Iteration 1:																
1	A		2.434	0.500	1.50E-04	500	500	3.33E+03	12.394	8.36E+05	0.016	12.80	75.79	62.29		-10.114
	B		-0.574	0.167	1.50E-04	500	0	1.11E+03	-26.318	5.92E+05	0.020	1938.21	-638.97	2225.72	Delta Q	42.869
												Σ:	-563.17	2288.01	-0.246	
Iteration 2																
1	A		2.680	0.500	1.50E-04	500	500	3.33E+03	13.648	9.21E+05	0.016	12.74	91.48	68.28		-3.315
	B		-0.328	0.167	1.50E-04	500	0	1.11E+03	-15.036	3.38E+05	0.020	1977.79	-212.81	1297.53	Delta Q	27.081
												Σ:	-121.33	1365.81	-0.089	
Iteration 3:																
1	A		2.769	0.500	1.50E-04	500	500	3.33E+03	14.100	9.51E+05	0.016	12.72	97.50	70.44		-0.611
	B		-0.239	0.167	1.50E-04	500	0	1.11E+03	-10.964	2.47E+05	0.021	2009.18	-114.95	961.17	Delta Q	7.071
												Σ:	-17.45	1031.60	-0.017	
Iteration 4:																
1	A		2.786	0.500	1.50E-04	500	500	3.33E+03	14.187	9.57E+05	0.016	12.72	98.67	70.85		-0.038
	B		-0.222	0.167	1.50E-04	500	0	1.11E+03	-10.189	2.29E+05	0.021	2017.63	-99.69	896.96	Delta Q	0.472
												Σ:	-1.02	967.80	-0.001	
Iteration 5:																
1	A		2.787	0.500	1.50E-04	500	500	3.33E+03	14.192	9.58E+05	0.016	12.72	98.75	70.87		-0.001
	B		-0.221	0.167	1.50E-04	500	0	1.11E+03	-10.140	2.28E+05	0.021	2018.19	-98.78	892.97	Delta Q	0.015
												Σ:	-0.03	963.85	0.000	
γ Benzene: 54.55 lb/ft^3																
v:	7.41E-06 ft^2/s															
g:	32.2 ft/s^2															

12-3

## GIVEN:

WATER IS FLOWING IN THE SYSTEM BELOW:



## REQUIRED:

- FIND  $Q$  IN EACH BRANCH.
- FIND  $P_A - P_B$

- INCLUDE MINOR LOSSES IN LOWER BRANCH
- SOLVE W/ HARDY CROSS METHOD

## SOLUTION:

- $h = kQ^2$  FOR EACH BRANCH:

$$k = \frac{8(L + L_e)f}{\pi^2 g D^5}$$

$$h_A = \frac{8(30 \text{ m} + 0 \text{ m})f_A}{\pi^2 (9.81 \text{ m/s}^2) (0.0525)^5} \cdot Q_A^2 = (6.22 \cdot 10^6) f_A \cdot Q_A^2$$

$$L_{\text{elbow}} = 30 \text{ m} \quad L_{\text{angle valve}} = 150 \text{ m}$$

$$h_B = \frac{8(60 \text{ m} + 3 \cdot 30 \text{ m} + 150 \text{ m})f_B}{\pi^2 (9.81 \text{ m/s}^2) (0.0525)^5} \cdot Q_B^2 = (6.22 \cdot 10^7) f_B \cdot Q_B^2$$

- GUESS  $Q$  VALUE FOR EACH BRANCH THAT ADDS UP TO  $Q$  AT JUNCTION:

$$Q_{\text{in}} = 850 \text{ L/min}$$

$$Q_A = 650 \text{ L/min} = 0.0108 \text{ m}^3/\text{s}$$

$$Q_B = 200 \text{ L/min} = 0.00333 \text{ m}^3/\text{s}$$

12.8  
cont 3. SPLIT NETWORK INTO CIRCUITS

• THIS NETWORK ONLY HAS 1 LOOP, CIRCUIT 1

4. CALCULATE  $h = KQ^2$  w/ ASSUMED  $Q_A$ ,  $Q_B$  VALUES: $h_A$ :

$$f_A = \frac{0.25}{\left(105 \left( \frac{1}{3.7 \cdot D/E} + \frac{5.47}{Re^{0.9}} \right) \right)^2}$$

$$= \frac{0.25}{\left(105 \left( \frac{1}{3.7 \cdot 1141} + \frac{5.47}{(2.01 \cdot 10^5)^{0.9}} \right) \right)^2}$$

$$= 0.0206$$

$$Re = \frac{4 Q D}{\pi D^2 v} = \frac{4(0.0108)(0.0525)}{\pi (0.0525)^2 (1.3 \cdot 10^{-6})} = 2.01 \cdot 10^5$$

$$\frac{D}{E} = \frac{0.0525}{4.6 \cdot 10^{-5}} = 1141$$

$$h_A = (6.22 \cdot 10^6) f_A \cdot Q_A^2 = (6.22 \cdot 10^6)(0.0206)(0.0108)^2$$

$$= \boxed{14.945}$$

 $h_B$ :

$$f_B = \frac{0.25}{\left(105 \left( \frac{1}{3.7 \cdot 1141} + \frac{5.47}{(6.21 \cdot 10^4)^{0.9}} \right) \right)^2}$$

$$= 0.023$$

$$Re = \frac{4(0.00333)(0.0525)}{\pi (0.0525)^2 (1.3 \cdot 10^{-6})} = 6.21 \cdot 10^4$$

$$\frac{D}{E} = 1141$$

$$h_B = (6.22 \cdot 10^7) f_B \cdot Q_B^2 = (6.22 \cdot 10^7)(0.023)(0.00333)^2$$

$$= \boxed{15.864}$$

5. SUM UP  $h$  VALUES, TAKING FLOW DIRECTION WITHIN THE CIRCUIT INTO ACCOUNT.

$$\sum h = h_A + h_B = (14.945) + (-15.864) = \boxed{-0.9187}$$

6. CALCULATE  $2KQ$  FOR EACH PIPE.

$$\text{PIPE A: } 2K_A Q_A = 2 \cdot (6.22 \cdot 10^6)(0.0206)(0.0108) = \boxed{2768}$$

$$\text{PIPE B: } 2K_B Q_B = 2 \cdot (6.22 \cdot 10^7)(0.023)(0.00333) = \boxed{9528}$$

12-8  
cont7. SUM ALL  $2KQ$  VALUES, ASSUMING ALL ARE POSITIVE

$$\Sigma 2KQ = 2K_A Q_A + 2K_B Q_B = (2768) + (9528)$$

$$= \boxed{12,296}$$

8. FOR EACH CIRCUIT, CALCULATE  $\Delta Q$ 

$$\Delta Q = \frac{\Sigma h}{\Sigma 2KQ} = \frac{(-0.9187)}{(12,296)} = \boxed{-7.5 \cdot 10^{-5}}$$

9. CALCULATE NEW  $Q$  VALUE FOR EACH PIPE

$$Q' = Q - \Delta Q$$

$$Q'_A = (0.0108) - (-7.5 \cdot 10^{-5}) = \boxed{0.010875}$$

$$Q'_B = (0.00333) - (-7.5 \cdot 10^{-5}) = \boxed{0.003405}$$

10. REPEAT 4-8 UNTIL  $\Delta Q$  BECOMES NEGLIGIBLY SMALL

• MY GUESSES FOR FLOW RATE WERE QUITE CLOSE, BUT I MADE AN EXCEL SHEET ANYWAY FOR PRACTICE. SEE TABLE FOR ITERATIONS.

FINAL ITERATION FLOW RATES:

$$Q_A = 0.01091 \text{ m}^3/\text{s} = \boxed{655 \text{ L/min}}$$

$$Q_B = 0.00326 \text{ m}^3/\text{s} = \boxed{196 \text{ L/min}}$$

• USE BERNOULLI'S EQUATION TO FIND PRESSURE LOSS B/T INLET PIPE (1) AND OUTLET PIPE (2)

$$\cancel{h_p} + \frac{P_1}{\gamma} + \cancel{\frac{V_1^2}{2g}} + \cancel{z_1} = \frac{P_2}{\gamma} + \cancel{\frac{V_2^2}{2g}} + h_L + \cancel{z_2}$$

$$\frac{P_1 - P_2}{\gamma} = h_L \quad \therefore \Delta P = h_L \cdot \gamma$$

•  $h_{LA} = h_{LB}$ , SO I WILL USE  $h_{LA}$  AS IT HAS NO MINOR LOSSES

$$\Delta P = f_A \left( \frac{L_A}{D} \cdot \frac{V_A^2}{2g} \right) \gamma_{\text{WAT}}$$

$$= (0.0206) \left( \frac{30}{0.0525} \cdot \frac{16 \cdot (0.01091)^2}{\pi^2 (0.0525)^4 \cdot 2(9.81)} \right) (9.81) = \boxed{149.5 \text{ kPa}}$$

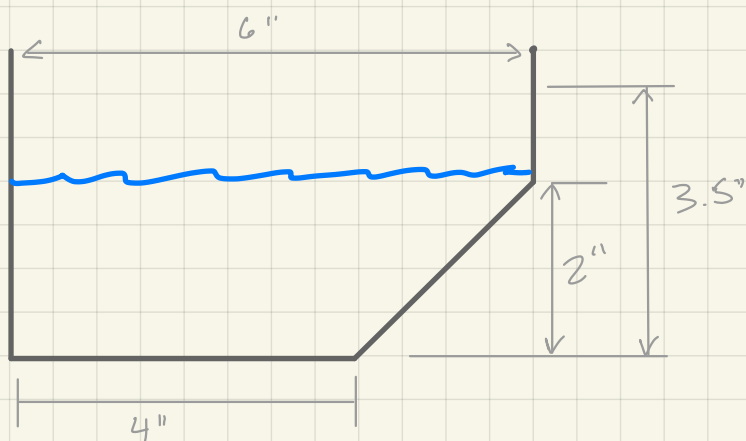
[illegible]



14.6

## GIVEN:

THE FOLLOWING FIGURE REPRESENTS THE CROSS SECTION OF A RAIN GUTTER ON A HOUSE:



## REQUIRED:

CALCULATE THE HYDRAULIC RADIUS FOR THE SECTION IF WATER IS 2" DEEP.

## SOLUTION:

$$R = \frac{A}{WP}$$

A:

- SPLIT INTO IDENTIFIABLE SHAPES, SUM THE AREA

LOWER RECTANGLE:  $4" \cdot 2" = 8 \text{ si}$   $\therefore A = \boxed{10 \text{ si}}$

TRIANGLE:  $\frac{2" \cdot 2"}{2} = 2 \text{ si}$

WP:

- SUM WETTED LENGTHS TOGETHER, USE PYTHAGOREAN THEORY FOR ANGLED WALL

$$C = \sqrt{a^2 + b^2} = \sqrt{2^2 + 2^2} = 2.83"$$

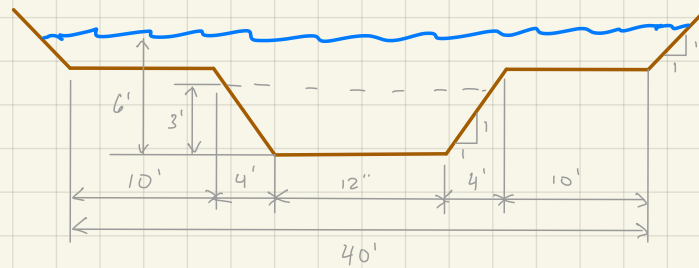
$$2" + 4" + 2.83" = \boxed{8.83"}$$

$$R = \frac{10 \text{ si}}{8.83"} = \boxed{1.13"}$$

14-15

## GIVEN:

BELOW IS AN APPROXIMATION OF A NATURAL STREAM CHANNEL W/ LEVEES ON BOTH SIDES:



$$n = 0.04$$

$$\text{AVG SLOPE} = 0.00015$$

## REQUIRED:

CALCULATE NORMAL DISCHARGE RATE AT WATER DEPTHS OF 3' AND 6'

## SOLUTION:

- USE MANNING'S EQUATION W/ MASS FLOW RATE EQUIVALENCY:

$$Q = \left( \frac{1.49}{n} \right) A R^{2/3} S^{1/2}$$

- $n$  AND  $S$  ARE GIVEN; FIND  $A$  AND  $R$

$A @ 6'$ :

$$\text{TOP TRAPAZOID: } (b + zy)y = (40\text{ft} + (1\text{ft} \cdot 2\text{ft})) \cdot 2\text{ft} = 84\text{sf}$$

$$\text{BOT TRAPAZOID: } (12\text{ft} + (1 \cdot 4\text{ft})) \cdot 4\text{ft} = 64\text{sf}$$

$$A = 84\text{sf} + 64\text{sf} = \boxed{148\text{sf}}$$

$A @ 3'$ :

$$\text{TRAPAZOID: } (12\text{ft} + (1 \cdot 3\text{ft})) \cdot 3\text{ft} = \boxed{45\text{sf}}$$

$R @ 6'$ :

$$\text{WP: } 2(\sqrt{2^2 + 2^2}) + 2(10\text{ft}) + 2(\sqrt{4^2 + 4^2}) + 12\text{ft} = \boxed{48.97\text{ft}}$$

$$R = \frac{A}{\text{WP}} = \frac{148\text{sf}}{48.97\text{ft}} = \boxed{3.022\text{ft}}$$

$R @ 3'$ :

$$\text{WP: } 2(\sqrt{3^2 + 3^2}) + 12\text{ft} = 20.49\text{ft}$$

$$R = \frac{45\text{sf}}{20.49\text{ft}} = \boxed{2.196\text{ft}}$$

14-15  
cont

- SOLVE FOR Q:

$$Q = \left( \frac{1.49}{n} \right) A R^{2/3} S^{1/2}$$

Q @ 6':

$$Q_6' = \left( \frac{1.49}{0.04} \right) (148 \text{ sf}) (3.022)^{2/3} (0.00015)^{1/2}$$

$$= 141.1 \text{ ft}^3/\text{s}$$

$$Q_3' = \left( \frac{1.49}{0.04} \right) (45 \text{ sf}) (2.196)^{2/3} (0.00015)^{1/2}$$

$$= 34.7 \text{ ft}^3/\text{s}$$

15-4

GIVEN:

A SHARP EDGED ORIFICE PLATE IS PLACED IN A 10" PIPE CARRYING AMMONIA.

$$S_{\text{G AMMONIA}} = 0.83 \quad \eta = 2.5 \cdot 10^{-6} \text{ lb/ft}^2 \quad Q = 25 \text{ gal/min} = 0.0557 \text{ ft}^3/\text{s}$$

REQUIRED:

CALCULATE THE DEFLECTION OF A WATER MANOMETER IF THE ORIFICE:

a) is 1"      b) is 7"

SOLUTION:

- EQUATION FOR VELOCITY, PULLED FROM LECTURE:

$$V_1 = C \sqrt{\frac{2gh \left( \frac{\gamma_m}{\gamma_f} - 1 \right)}{\left( \frac{A_1}{A_2} \right)^2 - 1}} \quad \therefore h = \frac{V^2}{C^2} \frac{\left( \frac{A_1}{A_2} \right)^2 - 1}{2g \left( \frac{\gamma_m}{\gamma_f} - 1 \right)} \quad \text{--- (1)}$$

• WHERE  $A_1 = A_{\text{TUBC}}$ ,  $A_2 = A_{\text{ORIFICE}}$ ,  $C = \text{ORIFICE COEFF}$ ,  $\gamma_m = \text{SW OF MAN}$   
 $\gamma_f = \text{SW OF WORKING FLUID}$ ,  $h = \text{DISPLACEMENT IN MANOMETER}$

- FOR THE ABOVE EQUATION, ALL BUT  $h$  AND  $C$  ARE KNOWN OR CAN BE CALCULATED W/ GIVEN INFO.
- $C$  CAN BE FOUND USING THE DISCHARGE COEFFICIENT GRAPH FOUND ON PAGE 403, FIGURE 15.7. IT REQUIRES A REYNOLDS NUMBER AND A RATIO B/T THE PIPE AND THE ORIFICE, BOTH OF WHICH CAN BE CALCULATED

C:

$$N_P = \frac{VD}{\nu}$$

$$= \frac{(0.1022 \text{ ft/s})(0.8333 \text{ ft})}{1.55 \cdot 10^{-6} \text{ ft}^2/\text{s}}$$

$$= \boxed{5.49 \cdot 10^4}$$

$$\frac{d_1}{D} = \frac{0.08333 \text{ ft}}{0.8333 \text{ ft}}$$

$$= \boxed{0.1}$$

$$\frac{d_7}{D} = \frac{0.5833 \text{ ft}}{0.8333 \text{ ft}}$$

$$= \boxed{0.7}$$

$$Q = AV \quad \therefore V = \frac{Q}{A} \quad A = \pi \left( \frac{D}{2} \right)^2$$

$$V_1 = \frac{4Q}{\pi D^2} = \frac{4(0.0657 \text{ ft}^3/\text{s})}{\pi (0.833 \text{ ft})^2} = \boxed{0.1022 \text{ ft/s}}$$

$$\nu = \frac{\mu}{\rho} \quad S_g = \frac{\gamma}{\gamma_{\text{water}}} \quad \rho = \frac{\gamma}{g}$$

$$\gamma_{\text{ann}} = S_{g_{\text{ann}}} \cdot \gamma_{\text{water}} = (0.83)(62.4 \text{ lb/ft}^3) = \boxed{51.792 \text{ lb/ft}^3}$$

$$\rho = \frac{51.792 \text{ lb/ft}^3}{32.2 \text{ ft/s}^2} = 1.608 \text{ slug/ft}^3$$

$$\nu = \frac{2.5 \cdot 10^{-6} \text{ lb/ft}^2}{1.608 \text{ slug/ft}^3} = \boxed{1.55 \cdot 10^{-6} \text{ ft}^2/\text{s}}$$

$$C_1 = 0.595$$

$$C_7 = 0.618$$

• FIGURE 15.7

• CALCULATE (1) FOR EACH ORIFICE SIZE (1" AND 7")

- CALCULATE AREA FOR PIPE AND BOTH ORIFICE SIZES ( $A_1$ ,  $A_{o1}$ ,  $A_{o7}$ )

$$A_1 = \pi \left( \frac{0.8333 \text{ ft}}{2} \right)^2 = \boxed{0.545 \text{ ft}^2}$$

$$A_{o1} = \pi \left( \frac{0.08333 \text{ ft}}{2} \right)^2 = \boxed{0.00545 \text{ ft}^2} \quad A_{o7} = \pi \left( \frac{0.5833 \text{ ft}}{2} \right)^2 = \boxed{0.267 \text{ ft}^2}$$

$$h_1 = \frac{(0.1022 \text{ ft/s})^2}{(0.595)^2} \cdot \left( \frac{\left( \frac{0.545 \text{ ft}^2}{0.00545 \text{ ft}^2} \right)^2 - 1}{2(32.2 \text{ ft/s}^2) \left( \frac{62.4 \text{ lb/ft}^3}{51.792 \text{ lb/ft}^3} - 1 \right)} \right) = \boxed{22.4 \text{ ft}}$$

$$h_7 = \frac{(0.1022 \text{ ft/s})^2}{(0.618)^2} \cdot \left( \frac{\left( \frac{0.545 \text{ ft}^2}{0.267 \text{ ft}^2} \right)^2 - 1}{2(32.2 \text{ ft/s}^2) \left( \frac{62.4 \text{ lb/ft}^3}{51.792 \text{ lb/ft}^3} - 1 \right)} \right) = \boxed{0.00656 \text{ ft}}$$

15-15

## GIVEN:

A PITOT-STATIC TUBE IS INSERTED INTO A DUCT CARRYING AIR @ STANDARD ATMOSPHERIC PRESSURE AND A TEMPERATURE OF  $50^{\circ}\text{C}$ . A DIFFERENTIAL MANOMETER READS  $0.24''$  OF WATER.

$$0.24'' \left( \frac{0.0254 \text{ m}}{1''} \right) = 0.0061 \text{ m}$$

## REQUIRED:

FIND THE VELOCITY OF THE FLOW OF AIR.

## SOLUTION:

FOR PITOT-STATIC TUBES USING A DIFFERENTIAL MANOMETER:

$$V_1 = \sqrt{2gh(\gamma_g - \gamma)/\gamma}$$

- $\gamma_g = \gamma$  OF GAUGE FLUID, WATER HERE
- $\gamma = \gamma$  OF WORKING FLUID, AIR IN THIS CASE

$$\gamma_g = \gamma_w = 9810 \text{ N/m}^3 \quad \bullet \text{ ASSUMING MANOMETER IS @ ROOM TEMP } (\sim 10^{\circ}\text{C})$$

$$\gamma = \gamma_{\text{air}} = 10.71 \text{ N/m}^3 \quad \bullet \text{ AT GIVEN } 50^{\circ}\text{C}$$

$$V_1 = \sqrt{\frac{2(9.81 \text{ m/s}^2)(0.0061 \text{ m})(9810 \text{ N/m}^3 - 10.71 \text{ N/m}^3)}{(10.71 \text{ N/m}^3)}}$$

$$= 10.46 \text{ m/s}$$