For the problems in the lecture notes, we discussed calculating values for pipes with flowing fluids. The notes and lectures for the past week have discussed using Bernoulli's equation to find the requested values of properties. When using Bernoulli's equation, it is critical to identify a reference point for elevation and place points on the system where we either know the most information and/or where we need to find information. Once said points are identified, Bernoulli's equation should be used to solve the problem based on what the question is asking for; this ensures that the equation is used correctly instead of using the equation to solve for assumed values.

For the problems in the lecture notes we have covered, we have used the volume, pressure, and elevation head value in the equation, but we have yet to use the pump, turbine, or friction head. When using Bernoulli's equation, it is essential to identify the values and concepts to substitute the relative equations to solve for the unknowns. Regarding specific specs for the tank volume head, the volume can be negligible to the large volume of the water in the tank. For the pressure head, anything exposed to the atmosphere is zero and negligible.

Hw#3 Yin dia. JA= 411 flow rate equation , inside JB= 2in oil Q=VA 590= 0.90 the flit in the 1 1 lindia. 28-2A 59m= 13.54 tubes before are not inside h=2912 ht N=2911 Moving So AP=4/h Ywate = 9.81 32 Q=? 0:1 Flow BT (59=0,90) h=281 V=A Z Refrace WWWWWWWW - no energy lass = 10 hL or Friction Merce FY (Sg= 13,54) p+hr +22 -2 )9 Volta ZB ZA= )9 V graup then minus 29 Find PA - KB this ( AB2 29 AA LAL -ĀR PA-PB+(2A-ZB) p 29. AB2 PB-PA+(2A-2B) dont 29( Q Know SU Find this AB2 AA N

 $hA + PA + VA^{2} + 28 = PB + VB + 28 + hA + hc$ PB-PA VB-VA2 +(28-2A) VA ( = 2 - ) = VB (= 2 - ) VA ( E(4,026)2) = VB (E(4,067)2) VA(12.799) = VB(3.35 ) VB = 3.7 GIVA PA + Yoil (19in) - Ywate (Sin) - Yoil (3011) - PB - PA PB PA = 55 16/7+3 (1912) - (62,4 16/7+5) (0.5811) - 55 6/7+3 (3011)  $\frac{P_{B}-P_{A}}{V} = \pm \frac{1}{6} \frac{1}{17} \pm \frac{1}{62} \frac{1}{47} \frac{1}{62} \frac{1}{47} \frac{1}{47} \frac{1}{62} \frac{1}{7} \frac{1}{7} \frac{1}{1674} \frac{1}{16747} \frac{1}{121} \frac{$ 



U SIACE OPEN to cotmarphone P= O PS: 9 Yuntr= 9.81 MU/M3 h======== 2.60m AJ. Paset Tom 0.85m fragrence  $\frac{P_1}{y} + \frac{V_1^2}{2g} + 2_1 = \frac{P_2}{y} + \frac{V_2^2}{2g} + 2_2$   $\frac{P_1 - P_2}{y} + \frac{V_1^2 - V_2^2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{y} + \frac{V_1^2 - V_2^2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{y} + \frac{V_1^2 - V_2^2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{y} + \frac{V_1^2 - V_2^2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{y} + \frac{V_1^2 - V_2^2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{y} + \frac{V_1^2 - V_2^2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{y} + \frac{V_1^2 - V_2^2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{2g} + 2_1 \quad \text{top of jet ioses}$   $\frac{P_1 - P_2}{2g} + 2_1 \quad \text{top of jet ioses}$ (Z2 = Z1) SO Z Portatal lesth 2.60 = 0.075 m +0.8 m +h h= 1.675