

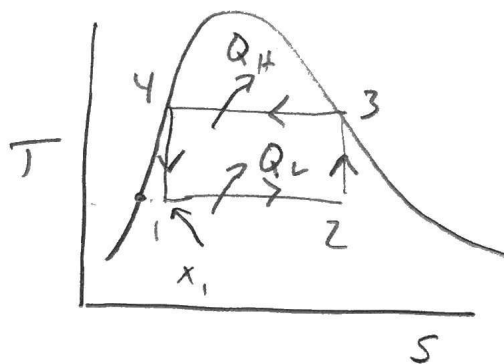
11-41

Given: R-134a Carnot refrigerator

Saturated vapor = 90 psia (Warm)

$$x = 0.05$$

Pressure Cold = 30 psia



From Table A-11E

$$T_{\text{Sat @ 90 psia}} = 72.78^\circ\text{F} + 459.67 = 532.45^\circ\text{R}$$

$$T_{\text{Sat @ 30 psia}} = 15.37^\circ\text{F} + 459.67 = 475.04^\circ\text{R}$$

$$a) \text{ COP}_{\text{Carnot}} = \frac{1}{\frac{T_H}{T_L} - 1} = \frac{1}{\frac{532.45}{475.04} - 1} = \boxed{8.28}$$

b) quality @ point 1 is beginning of heat absorption

$$s_1 = s_4 = s_f + x_4 s_{fg} = 0.07481 + (0.05)(1.1452) =$$

$$s_1 = 0.08208 \text{ Btu/lbm-R}$$

From Table A-12E

$$x_1 = \left( \frac{s_1 - s_f}{s_{fg}} \right) = \frac{0.08208 - 0.03792}{0.14595} = \boxed{0.237}$$

11-4 cont

c) Find Net Work input

Find Area of cycle

$$W_{net} = (T_H - T_L)(S_3 - S_4)$$

$$= (532.8 - 475.4)(.2201 - .08208)$$

$$W_{net} = 7.92 \text{ Btu/lbm}$$

$$S_3 = S_{g_{90H}} = 0.22011$$

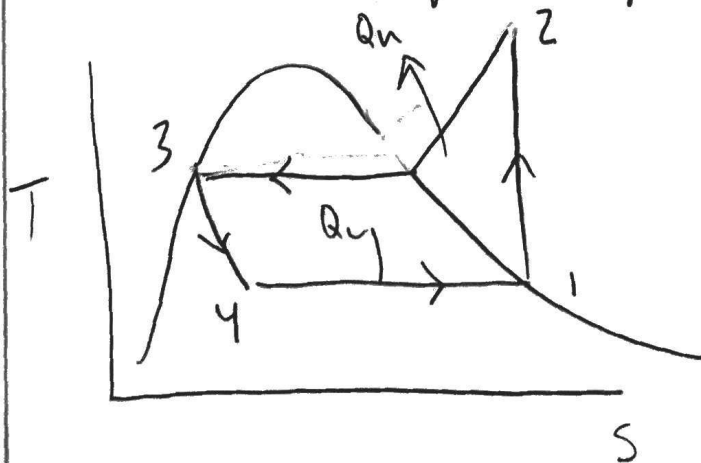
$$S_4 = S_{f_{90H}} = .08208$$

11-5

Not need to have turbine in real cycle  $\Rightarrow$  throttling valve used to make it closer to actual cycle

11-11

Given: Ideal vapor-compression cycle of R-134a



$$P_1 = 20 \text{ psia}$$

$$P_2 = 80 \text{ psia}$$

$$P_3 = 80 \text{ psia}$$

$$P_4 = 20 \text{ psia}$$

11-11 Cont

Water enters @ 55 F

From Table A-12E

$$h_1 = 102.74 \text{ Btu/lbm}$$

$$s_1 = .22570 \text{ Btu/lbm R}$$

$$s_1 = s_2 \Rightarrow \text{find } h_2 @ 80 \text{ psia on Table A-13E}$$

That matches  $s_1$ 

$$\Rightarrow h_2 = 115.01 \text{ Btu/lbm}$$

$$h_3 (80 \text{ psia}) = h_f @ 80 \text{ psia} = 33.39 \text{ Btu/lbm}$$

$$h_3 = h_4 \Rightarrow h_4 = 33.39 \text{ Btu/lbm}$$

$$\dot{Q}_L = \dot{m}_{ice} (\Delta h_{ice})$$

$$= \frac{(.004167 \text{ lbm})}{s} \left| \frac{169 \text{ Btu}}{\text{lbm}} \right.$$

$$\dot{Q}_L = 0.7042 \text{ Btu/s}$$

 $\Delta h$  given @ 169 Btu/lbm

$$\dot{m}_{ice} = \frac{15 \text{ lbm}}{\text{hr}} \left| \frac{1 \text{ hr}}{3600 \text{ s}} \right.$$

$$\dot{m}_{ice} = .004167 \text{ lbm/s}$$

$$\dot{m}_g = \frac{\dot{Q}_L}{h_1 - h_4} = \frac{.7042}{102.74 - 33.39} = .01015 \text{ lbm/s}$$

$$W_{in} = \dot{m}_g (h_2 - h_1) = (.01015 (115.01 - 102.74)) \left| \frac{1 \text{ hp}}{.07068 \text{ Btu/s}} \right. =$$

$$\boxed{.0176 \text{ hp}}$$

11-13 Given: Ideal vapor-compression R-134a

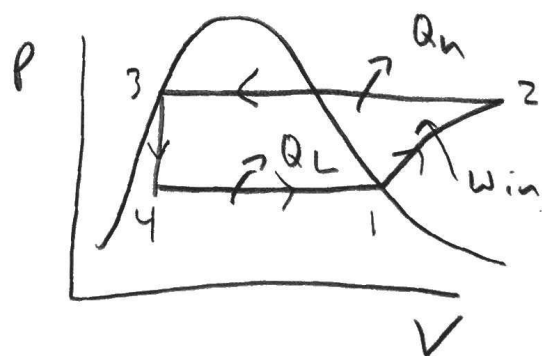
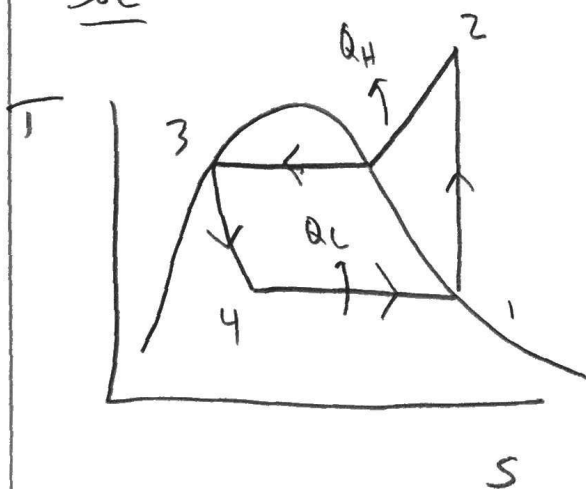
Condensor @ 800 kPa

Evaporator @  $-12^{\circ}\text{C}$

FIND:

- System COP
- Power required for 150 kW cooling load

SOL



1-2  
Compressor

2-3  
Condensor  
 $P = 800 \text{ kPa}$

3-4  
Expansion

4-1  
Evap

$$h_1 = h_{g, -12^{\circ}\text{C}} = 243.34 \text{ kJ/kg}$$

$$s_1 = s_{g, -12^{\circ}\text{C}} = 0.93425 \text{ kJ/kgK}$$

Find  $h_2$  using  $s_2 = s_1$  at 800 kPa

$$h_2 = 273.73 \text{ kJ/kg}$$



11-13 contFind  $h_3$  @ 0.8 MPa at saturation liquid @ pt 3

$$h_3 = 95.48 \text{ kJ/kg}$$

$$h_3 = h_4$$

$$\Rightarrow \dot{Q}_L = \dot{m} (h_1 - h_4)$$

$$\dot{m} = \frac{\dot{Q}_L}{h_1 - h_4} = \frac{150 \text{ kJ/s}}{(243.34 - 95.48) \text{ kJ}} \text{ kg}$$

$$\dot{m} = 1.014 \text{ kg/s}$$

$$\Rightarrow \dot{W}_{in} = \dot{m} (h_2 - h_1)$$

$$= (1.014 \text{ kg/s}) (273.73 - 243.34)$$

$$\boxed{\dot{W}_{in} = 30.8 \text{ kW}}$$

$$\text{COP}_R = \frac{\dot{Q}_L}{\dot{W}_{in}} = \frac{150 \text{ kW}}{30.8 \text{ kW}} = \boxed{4.87}$$