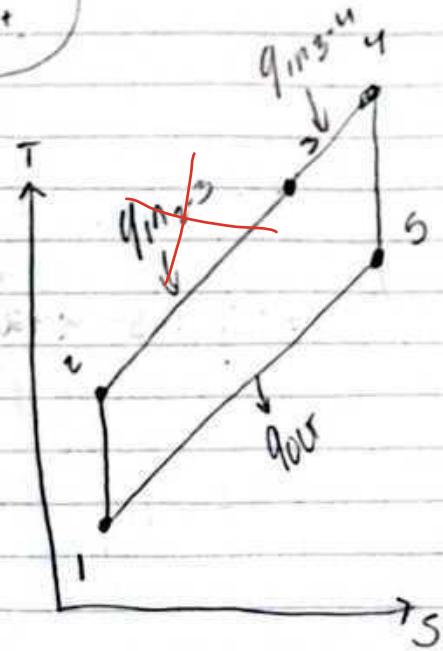
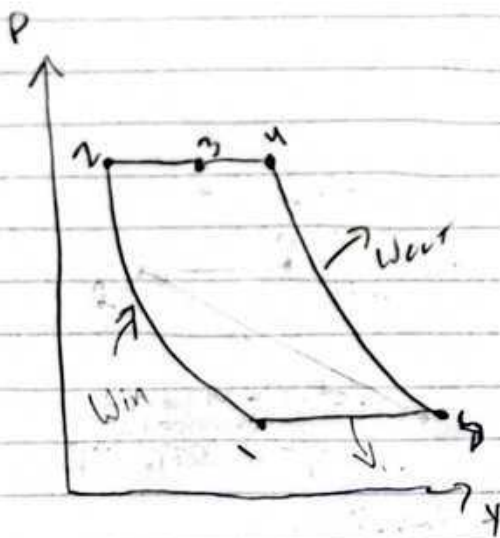
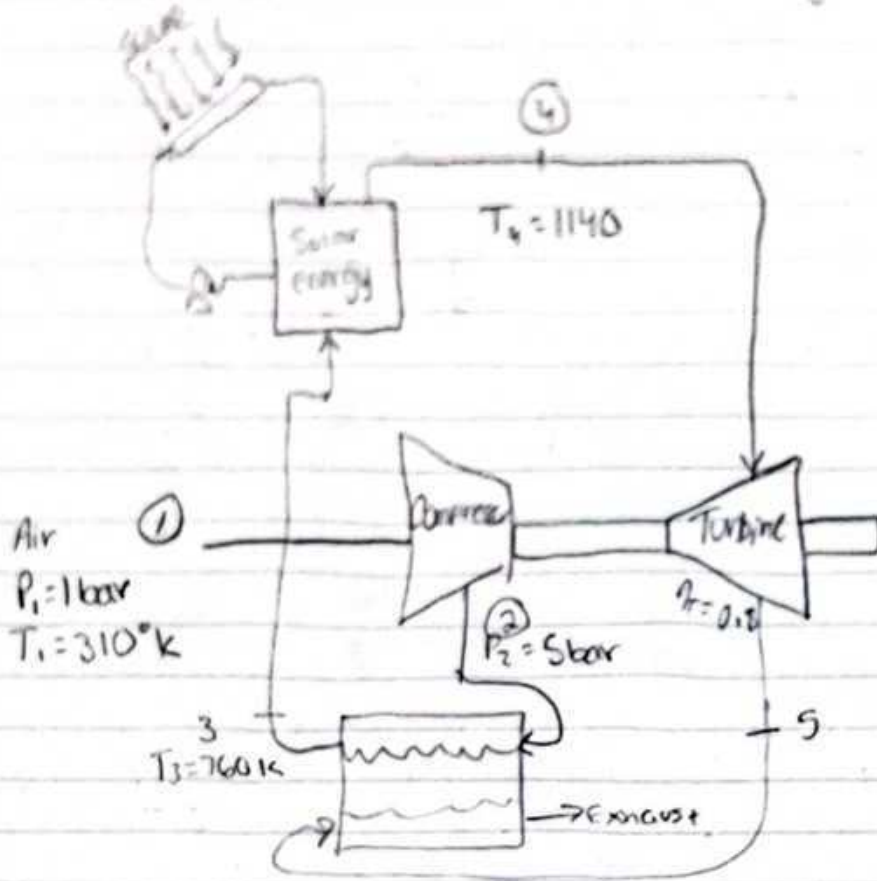


$$-25 \frac{55}{90} + \frac{9.5}{10} = \frac{64.5}{100}$$

TEST 1

1. Solar energy proposed solution of heat source in an ideal cold air standard cycle



1

Assuming $C_p C_v$ CONSTANT

$\text{Isentropic Compression } 1 \rightarrow 2$ $P = \text{const } 2 \rightarrow 3$ $P = \text{const } 3 \rightarrow 4$ $\text{Isentropic Exp } 4 \rightarrow 5$ $P = \text{const } 5 \rightarrow 1$

$P_1 = 1 \text{ bar}$	$P_2 = 5 \text{ bar}$	$P_3 = 5 \text{ bar}$	$P_4 = 5 \text{ bar}$	$P_5 = 1 \text{ bar}$
$T_1 = 310 \text{ K}$	$T_2 = 490 \text{ K}$	$T_3 = 760 \text{ K}$	$T_4 = 1140 \text{ K}$	$T_5 = 719.78 \text{ K}$
	$h_2 = 492.74$	$h_3 = 778.18$	$h_4 = 1207.57$	

$$\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\frac{k-1}{k}}$$

$$T_2 = 310 \text{ K} \left(\frac{5}{1}\right)^{\frac{1.4-1}{1.4}}$$

$$T_2 = 490.98 \text{ K}$$

$$\frac{T_5}{T_4} = \left(\frac{P_5}{P_4}\right)^{\frac{k-1}{k}}$$

$$T_5 = 1140 \left(\frac{1}{5}\right)^{\frac{1.4-1}{1.4}}$$

$$T_5 = 719.78 \text{ K}$$

a) Thermal Efficiency and Heat exchanger effectiveness

$$\eta_T = \frac{W_{\text{net}}}{Q_{\text{in}}}$$

$$W_{\text{net}} = W_{\text{out}} - W_{\text{in}} = W_{4-5} - W_{1-2} = 337.84 - 181.88 = 155.96$$

$$W_{\text{out}} = h_5 - h_4 = C_p (T_4 - T_5) = 1.005 (1140 - 719.78)$$

$$= 422.3 \cdot 0.8 = 337.84$$

$$W_{\text{in}} = h_2 - h_1 = C_p (T_2 - T_1) = 1.005 (490.98 - 310)$$

$$= 181.88$$

$$Q_{\text{in}} = \cancel{q_{1-2}} + q_{2-3}$$

$$= (h_3 - h_2) + (h_4 - h_3)$$

$$= (778.18 - 492.74) + (1207.57 - 778.18)$$

$$= 714.83$$

$$\eta_T = \frac{155.96}{714.83}$$

$$= 21.8 \%$$

$$\epsilon = \frac{h_3 - h_2}{h_4 - h_2} = \frac{\text{Actual}}{\text{Max}}$$

$$= \frac{778.18 - 492.74}{1207.57 - 492.74}$$

$$0.3913 = 39.13\%$$

Effective

-3

b) The air mass flow rate, in kg/s, for a net power output of 500 kW

$$\dot{m} = \frac{\dot{Q}_{\text{net}}}{\dot{W}_{\text{net}}} = \frac{500 \text{ kW}}{155.96} = 3.20 \frac{\text{kg}}{\text{s}}$$

c) What would be the thermal efficiency if the heat exchanger were operating at 100% effectiveness.

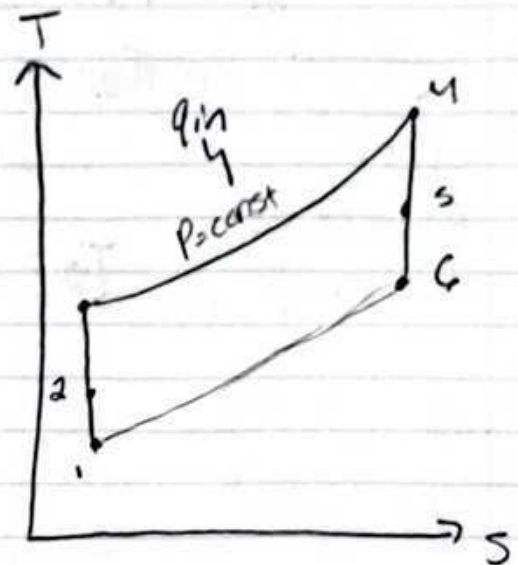
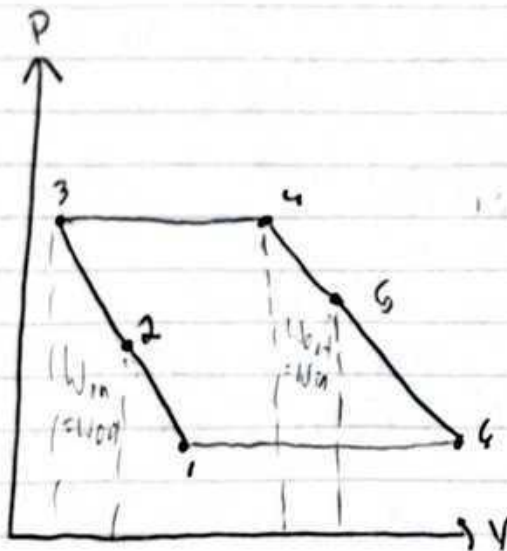
$$\eta_0 = 1 - \frac{T_1}{T_3}$$

$$= 1 - \frac{310}{719.78} = 56.91\%$$

-5 NO Writing

-10

2) A turbojet aircraft flies w/ a velocity of 900 km/h at an altitude where Temp is -35°C and P is 40 kPa. Combustion gases enter turbine at 950°C . The turbine produces 500 kJ/kg of work, all of which is used to drive the compressor. Assuming an isentropic efficiency of 80% for the compressor, an isentropic efficiency of 90% for the turbine and using variable specific heats.



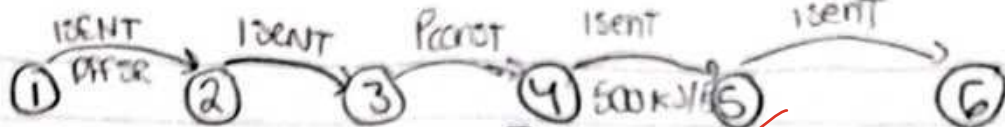
DIFFER

COMPRESSOR

Boiler

Turbine

NOZZLE



$$T_1 = 238 \text{ K} \quad T_2 = 239.45$$

$$P_1 = 40 \text{ kPa} \quad P_2 = 40.85$$

$$V_1 = 900 \text{ km/h} \quad V_2 = 0$$

$$V_1 = \frac{RT_1}{P_1} \quad V_2 = \frac{RT_2}{P_2} = 1.68$$

$$= \frac{0.287 \cdot 238}{40}$$

$$= 1.708$$

$$\frac{V_1^2}{2} + h_1 = \frac{V_2^2}{2} + h_2$$

$$C_p(T_2 - T_1) = \frac{V_1^2}{2}$$

$$T_2 = T_1 + \frac{V_1^2}{2C_p} = 238 + \frac{900^2}{2(1.005)}$$

$$T_2 = 239.45 \text{ K}$$

$$\frac{P_2}{P_1} = \left(\frac{T_2}{T_1}\right)^{\frac{\gamma}{\gamma-1}}$$

$$P_2 = P_1 \cdot \left(\frac{T_2}{T_1}\right)^{\frac{\gamma}{\gamma-1}}$$

$$P_2 = 40.85$$

$$q_{in} = C_p(T_3 - T_2)$$

$$T_3 = 1223 \text{ K}$$

$$T_5 = 1221.007 \text{ K}$$

$$W_c = W_t$$

$$C_p(T_2 - T_1) = C_p(T_4 - T_5)$$

$$239.45 - 238 = (1223 - T_5)$$

$$1.45 = 1223 - T_5$$

$$T_5 = 1221.55$$

$$\eta_T = \frac{h_4 - h_{5a}}{h_4 - h_{5s}}$$

$$h_4 = 1301$$

$$h_5 = 1905.93 \text{ interpolation app}$$

$$.90 = \frac{1301 - h_{5a}}{1301 - 1905.93}$$

$$h_5 = 1845.437$$

$$T_3 = T_2 + \frac{V_2^2}{2C_p}$$

$$= 239.45 + \frac{1.68^2}{2(1.004)}$$

$$T_3 = 240.86$$

$$\frac{T_5}{T_1} = \left(\frac{P_5}{P_1}\right)^{\frac{\gamma-1}{\gamma}}$$

$$\frac{1221.007}{238} = \left(\frac{P_5}{40}\right)^{\frac{\gamma-1}{\gamma}}$$

$$P_5 = 41.62$$

$$\frac{T_6}{T_5} = \left(\frac{P_6}{P_5}\right)^{\frac{\gamma-1}{\gamma}}$$

$$T_6 = 1221.55 = \left(\frac{40}{41.6}\right)^{\frac{1.4-1}{1.4}}$$

$$T_6 = 1207.9$$

$$\left(\frac{T_3}{T_2}\right) = \left(\frac{P_3}{P_2}\right)^{\frac{\gamma-1}{\gamma}}$$

$$\frac{240.85}{239.45} = \left(\frac{P_3}{40.85}\right)^{\frac{0.4}{1}}$$

$$P_3 = 41.69$$

✓ a) Pressure of Combustion gases @ Turbine exit

$$P_5 = 41.62 \text{ kPa}$$

✗
✓ b) Velocity of the gases at the nozzle exit

$$V_6 = \sqrt{2 C_p (T_6 - T_0)}$$
$$= \sqrt{2 (1.005) (1221.55 - 1207.9)}$$

$$V_6 = 5.237 \text{ km/h}$$

✓ c) The thrust for engine if diffuser inlet diameter is 1.6 m

$$\dot{m} = \rho_1 V_1 A_1$$
$$= \frac{1}{\gamma} \cdot V_1 \cdot \pi r^2$$
$$= \frac{1}{1.709} \cdot 900 \cdot (\pi \cdot 0.8^2)$$

Correct equations wrong numbers

$$\dot{m} = 1059.46$$

$$F = \dot{m} (V_{\text{exit}} - V_{\text{inlet}})$$

$$= 947965.608$$

UHOH !!

-5 NO Writing