

TEST 1

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MET 350

CAMERON MORTON

2/23/25

CMORT 008 @ ODU.EDU

COLD AIR - STANDARD BRAYTON CYCLE

$$\eta_T = 0.8 \quad k = 1.4$$

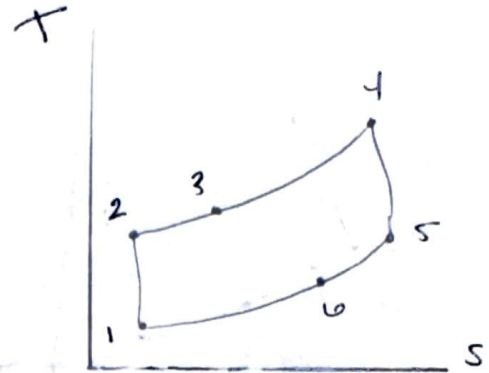
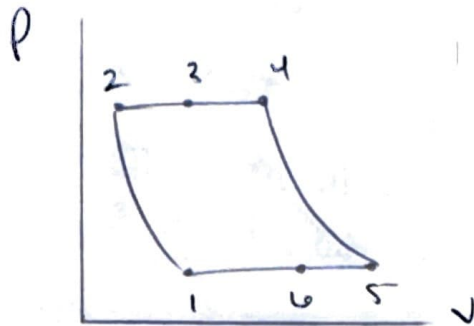
$$P_1 = 1 \text{ BAR}$$

$$P_2 = 5 \text{ BAR}$$

$$T_3 = 760 \text{ K}$$

$$T_4 = 1140 \text{ K} \quad P_5 = 1 \text{ BAR}$$

$$T_1 = 310 \text{ K}$$



$P = \text{CONST.}$ $\xrightarrow{\text{1.5 ENT.}}$ $P = \text{CONST.}$ $\xrightarrow{\text{1.5 ENT.}}$ $P = \text{CONST.}$ $\xrightarrow{\text{1.5 ENT.}}$ $P = \text{CONST.}$

$P_1 = 100 \text{ kPa}$ $T_1 = 310 \text{ K}$ $h_1 = 310.24 \frac{\text{kJ}}{\text{kg}}$ $P_{r1} = 1.5546$	$P_2 = 500 \text{ kPa}$ $T_2 = \dots$ $T_2 = T_1 \left(\frac{P_2}{P_1} \right)^{\frac{k-1}{k}} = 490.98 \text{ K}$ $h_2 = 493.747$ $P_{r2} = 7.882$	$P_3 = P_2$ $T_3 = 760 \text{ K}$ $h_3 = 778.18$ $P_{r3} = 39.27$	$P_4 = P_3$ $T_4 = 1140 \text{ K}$ $h_4 = 1207.57$ $P_{r4} = 193.1$	$P_5 = P_4$ $T_5 = \dots$ $h_5 = 826.162$ $P_{r5} = 10.721$	$P_6 = 100 \text{ kPa}$ $T_6 = \dots$ $h_6 = 538.962$
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$$\frac{T_4}{T_{5s}} = \left(\frac{P_4}{P_{5s}} \right)^{\frac{k-1}{k}} \rightarrow \frac{1140}{T_{5s}} = \left(\frac{5}{1} \right)^{\frac{1.4-1}{1.4}} = 719.78 \text{ K}$$

$$h_{5s} = 784.583 \frac{\text{kJ}}{\text{kg}}$$

$$P_{r5s} = 21.984$$

$$\eta_T = \frac{T_4 - T_5}{T_4 - T_{5s}} \rightarrow 0.8 = \frac{1140 - T_5}{1140 - 719.78}$$

$$T_5 = 803.824 \text{ K}$$

$$h_5 = 826.162 \frac{\text{kJ}}{\text{kg}}$$

$$P_{r5} = 48.675$$

$$(T_3 - T_2) = (T_5 - T_6) \rightarrow (760 - 490.98) = (803.824 - T_6)$$

$$T_6 = 534.804 \text{ K}$$

a) THERMAL EFFICIENCY

$$\eta_{TH} = \frac{W_{NET}}{\dot{Q}_{IN}} \rightarrow$$

$$\begin{aligned}\dot{Q}_{IN} &= C_p (T_4 - T_3) \\ &= 1.005 (1140 - 760) \\ &= 381.9 \text{ kJ/kg}\end{aligned}$$

$$= \frac{155.97}{381.9}$$

$$\boxed{\eta = 0.4084}$$

$$40.84\%$$

$$W_{NET} = W_T - W_C$$

$$\begin{aligned}&= C_p (T_4 - T_5) - C_p (T_2 - T_1) \\ &= 1.005 (1140 - 803.824) \\ &\quad - 1.005 (490.98 - 310)\end{aligned}$$

$$W_{NET} = 155.97 \text{ kJ/kg}$$

$$\text{EFFECTIVENESS, } \epsilon = \frac{T_3 - T_2}{T_5 - T_2} = \frac{760 - 490.98}{803.824 - 490.98}$$

$$\boxed{= 0.8599}$$

$$85.99\%$$

b) NET POWER (500W)

$$\dot{m} \cdot W_{NET} = 500$$

$$\dot{m} = \frac{500}{W_{NET}} \rightarrow \frac{500}{155.97}$$

$$\boxed{3.206 \text{ kg/s}}$$

c) EFFECTIVENESS @ 100%

$$\frac{T_3 - T_2}{T_5 - T_2} = 1 \rightarrow T_3 - T_5 = T_2 - T_1$$

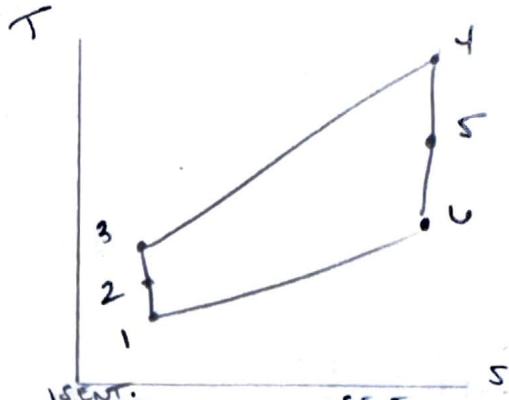
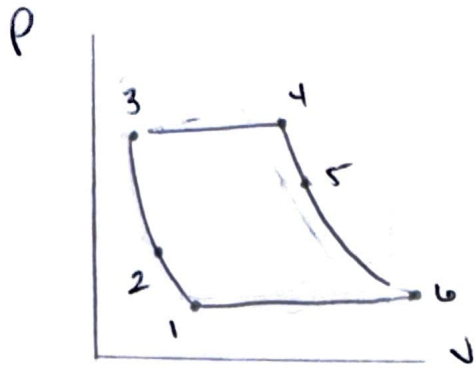
$$\eta_{TH} = \frac{W_{NET}}{\dot{Q}_{IN}} = \frac{C_p (T_4 - T_5 - T_2 + T_1)}{C_p (T_4 - T_3)}$$

$$\boxed{= 0.5237}$$

$$52.37\%$$

11. TURBOJET AIRCRAFT $\eta_c = 80\%$
 $V = 900 \text{ km/h} = 250 \text{ m/s}$ $\eta_T = 90\%$
 $T = -35^\circ\text{C}$ $T_T = 950^\circ\text{C}$
 $P = 40 \text{ kPa}$

$w_{\text{comp}} = 500 \text{ kJ/kg}$
 $w_{\text{turb.}} = 500 \text{ kJ/kg}$
 $v_1 = \frac{RT_1}{P_1} = 1.7077 \text{ m}^3/\text{kg}$



$P = \text{const.}$
 $\xrightarrow{\text{1-2}} \xrightarrow{\text{2-3}} \xrightarrow{\text{3-4}} \xrightarrow{\text{4-5}} \xrightarrow{\text{5-6}}$
 $\eta_c = 0.8$ $\eta_T = 0.95$ $P_6 = P_1$

$V_1 = 900 \text{ km/h}$

$T_1 = 238 \text{ K}$ $T_2 = 269.1 \text{ K}$ $h_2 = 269.208$ $P_1 = 40 \text{ kPa}$ $P_2 = 37.595$ $T_3 = 751.788$ $T_4 = 1223 \text{ K}$ $T_5 = 784.401 \text{ K}$
 $h_1 = 238.02$ $h_2 = 269.208$ $h_3 = 669.208$ $h_4 = 1304.853$ $h_5 = 804.853$
 $P_{r1} = 0.618$ $P_{r2} = 0.948$ $P_{r3} = 257.34$ $P_{r4} = 44.818$
 $v_1 = 1.7077 \text{ m}^3/\text{kg}$ $s_2 = 1.593$ $s_3 = 3.201$ $P_5 = (P_{r5})P_4$
 $P_5 = 256.174 \text{ kPa}$

$$T_2 = T_1 + \frac{V_1^2}{2C_p} \quad \left| \begin{array}{l} P_{r35} = 22.979 \\ T_{35} = 658.813 \end{array} \right|$$

$$238 = \frac{900}{2} \left| \frac{1}{1.005} \right| \left| \frac{1}{1} \right| \left| \frac{1}{1000} \right| \left| \frac{1}{1} \right| \left| \frac{1}{3600} \right|$$

$$= 269.1 \text{ K}$$

$$P_2 = \left(\frac{P_{r2}}{P_{r1}} \right) P_1 = \frac{0.948}{0.618} (40) = 61.36 \text{ kPa}$$

$$w_{\text{comp}} = h_2 - h_1$$

$$h_3 = h_2 + w_{\text{turb.}} \Rightarrow 500 + 269.208 = 769.208$$

$$P_{35} = \left(\frac{P_{r35}}{P_{r2}} \right) P_2 \Rightarrow \left(\frac{22.979}{0.948} \right) 61.36 = 1487.33 \text{ kPa} = P_4 = P_5$$

$$w_{\text{turb.}} = h_4 - h_5 \Rightarrow 1304.853 - 500 = 804.853$$

$$\eta_T = \frac{h_4 - h_5}{h_4 - h_{5s}} \rightarrow h_{5s} = -h_4 + h_5 + \eta_T(h_4)$$

$$h_{5s} = 749.3$$

$$T_{5s} = 727.85 \text{ K}$$

$$P_{5s} = 33.355$$

$$P_{v6} \cdot \left(\frac{P_v}{P_r} \right) P_{r5} = 5.2082$$

$$T_6 = 437.03 \text{ K}$$

$$h_6 = 438.588 \text{ kJ/kg}$$

b) VELOCITY @ NOZZLE EXIT

$$V_6 = \sqrt{2(h_5 - h_6)}$$

$$= 27.065 \text{ kJ/kg}$$

$$\rightarrow \boxed{855.893 \text{ m/s}}$$

c) THRUST w/ 1.6 m INLET

$$F = \frac{V_1}{\bar{v}_1} \left(\frac{\pi}{4} \right) D^2 (V_6 - V_1) \rightarrow \frac{250}{1.7077} \left(\frac{\pi}{4} \right) (1.6 \text{ m})^2 (V_6 - V_1)$$

$$\boxed{F = 178342.24 \text{ N}}$$

a) PRESSURE @ TURBINE EXIT

$$\boxed{P_5 = 256.174 \text{ kPa}}$$