

Homework 3.2

The problems discussed this week were a continuation of series and parallel piping systems. We continued our discussion on how to tackle the problems and ended up creating a new way to do them, dubbed "Kyle's Method". We also began talking about how to select pumps and why pump choice is an important factor in piping systems. One of the factors that was discussed was how the RPM of a pump affects the flowrate of a liquid.

Homework Problems

11.23

11-23) For the system below, compare total head on the pump and power delivered by the pump on the coolant.

$Q = 30 \frac{\text{gal}}{\text{min}} = 6930 \frac{\text{in}^3}{\text{min}} = 115.5 \frac{\text{in}^3}{\text{s}}$
 $\Rightarrow Q = 0.07 \text{ ft}^3/\text{s}$

1" Schedule 40
 $D_1 = 2.067'' \Rightarrow A_1 = 3.36 \text{ in}^2 = 0.0233 \text{ ft}^2$
1/4" Schedule 40
 $D_2 = 1.38'' \Rightarrow A_2 = 1.50 \text{ in}^2 = 0.01 \text{ ft}^2$

$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + Z_1 + P_{\text{del}} = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + Z_2 + h_f$
 $V_{2 \text{ pipe}} = 0.07 \text{ ft}^3/\text{s} / 0.0233 \text{ ft}^2 = 3 \text{ ft/s} = V_1$
 $V_{1/4 \text{ pipe}} = 0.07 \text{ ft}^3/\text{s} / 0.01 \text{ ft}^2 = 7 \text{ ft/s} = V_2$

$\rho = \gamma/g \Rightarrow 57.4 \frac{\text{lb}}{\text{ft}^3} / 32 \frac{\text{ft}}{\text{s}^2} = 1.79 \frac{\text{lb}}{\text{ft}^3}$
 $N_{R_1} = \frac{3 \text{ ft/s} \cdot (1.04 \text{ in} / 12 \frac{\text{in}}{\text{ft}}) \cdot 57.4 \frac{\text{lb}}{\text{ft}^3}}{3.6 \cdot 10^{-5} \frac{\text{lb}}{\text{ft} \cdot \text{s}}} = 82392.9$
 $N_{R_2} = \frac{7 \text{ ft/s} \cdot (1.38 \text{ in} / 12 \frac{\text{in}}{\text{ft}}) \cdot 57.4 \frac{\text{lb}}{\text{ft}^3}}{3.6 \cdot 10^{-5} \frac{\text{lb}}{\text{ft} \cdot \text{s}}} = 128352.8$

$\Rightarrow f_{2''} = 0.0185 \quad f_{1/4''} = 0.016$
 $\Rightarrow h_{f_{2''}} = 0.0185 \cdot \left(\frac{120''}{2.067''} \right) \cdot \left(\frac{36 \text{ ft/s}}{(2.098 \frac{\text{in}}{\text{s}})} \right)$
 $\Rightarrow h_{f_{2''}} = 1.8'' = 0.15'$
 $\Rightarrow h_{f_{1/4''}} = 0.016 \cdot \left(\frac{240''}{1.38''} \right) \cdot \left(\frac{84 \text{ ft/s}}{(2.098 \frac{\text{in}}{\text{s}})} \right)$
 $\Rightarrow h_{f_{1/4''}} = 25.4'' = 2.11'$

$h_{\text{tot}} = 27.2'' = 2.27'$
 $P_{\text{del}} = 27.2'' = 2.27'$
 $P_1 = 57.4 \frac{\text{lb}}{\text{ft}^3} \cdot 3 \text{ ft} = 172.2 \frac{\text{lb}}{\text{ft}^2} = 1.2 \text{ PSI}$
 $P_2 = 57.4 \frac{\text{lb}}{\text{ft}^3} \cdot 22 \text{ ft} = 1262.8 \frac{\text{lb}}{\text{ft}^2} = 9.77 \text{ PSI}$

$\Rightarrow \text{total head at pump} = \frac{P_1}{\gamma} + \frac{V_1^2}{2g} + Z_1 + P_{\text{del}}$
 $\Rightarrow \frac{172.2 \frac{\text{lb}}{\text{ft}^2}}{57.4 \frac{\text{lb}}{\text{ft}^3}} + \frac{3 \text{ ft/s}^2}{2 \cdot 32 \frac{\text{ft}}{\text{s}^2}} + 3 \text{ ft} + 2.27 \text{ ft} = 8.41 \text{ ft} = \text{head at inlet of pump}$

11.24

11-24) For the system in the previous problem, specify the size pipes necessary to return coolant to the machines. Machine 2 requires 20 gal/min & machine 1 requires 10 gal/min. Fluid leaves at 0 PSI.

$Q = 30 \frac{\text{gal}}{\text{min}} = 6930 \frac{\text{in}^3}{\text{min}} = 115.5 \frac{\text{in}^3}{\text{s}}$
 $= 0.07 \text{ ft}^3/\text{s} = 4.2 \frac{\text{ft}^3}{\text{min}}$

• Velocity must remain constant, therefore area of the pipes must change to achieve desired flow rates

$\Rightarrow 0.07 \frac{\text{ft}^3}{\text{s}} = 3 \frac{\text{ft}}{\text{s}} \cdot A \Rightarrow A = 0.0233 \text{ ft}^2 \Rightarrow 2'' \text{ Schedule 40}$
 $20 \frac{\text{gal}}{\text{min}} = 4620 \frac{\text{in}^3}{\text{min}} = 77 \frac{\text{in}^3}{\text{s}} = 0.045 \frac{\text{ft}^3}{\text{s}}$
 $\Rightarrow 0.045 \frac{\text{ft}^3}{\text{s}} = 3 \frac{\text{ft}}{\text{s}} \cdot A \Rightarrow A = 0.015 \text{ ft}^2 \Rightarrow 1 \frac{1}{2}'' \text{ Schedule 40 pipe}$
 $10 \frac{\text{gal}}{\text{min}} = 2310 \frac{\text{in}^3}{\text{min}} = 38.5 \frac{\text{in}^3}{\text{s}} = 0.0222 \frac{\text{ft}^3}{\text{s}}$
 $\Rightarrow 0.0222 \frac{\text{ft}^3}{\text{s}} = 3 \frac{\text{ft}}{\text{s}} \cdot A \Rightarrow A = 0.0074 \Rightarrow 1'' \text{ Schedule 40 pipe}$

Main pipe: 2" Schedule 40
 to #1: 1 1/2" Schedule 40
 to #2: 1" Schedule 40

12.3

12.3

$\frac{D}{L} = \frac{0.0525 \text{ m}}{4.5 \times 10^{-2} \text{ m}} = 1.17 \times 10^{-3}$

Moody's $\rightarrow$ at (0.019) for f_2 (and f_1)

$(571.43 f_2 + 0.7) \left(\frac{V_2^2}{2g} \right) = (1142.86 f_2 + 4.66) \left(\frac{V_2^2}{2g} \right)$

$V_2 = 0.44 V_1$ $A = 2.168 \times 10^{-3} \text{ m}^2$ $850 \text{ L/min} = 0.0141 \text{ m}^3/\text{s}$

$Q_1 = Q_2 = Q_3 \rightarrow Q = A_1 V_1 + A_2 V_2$

$0.0141 = (2.168 \times 10^{-3}) V_1 + (2.168 \times 10^{-3}) (0.44 V_1)$

$V_1 = 3.97 \text{ m/s}$

$V_2 = 0.44 (3.97) = 1.75 \text{ m/s}$

$N_H = \frac{V_2^2}{2g} \rightarrow \frac{(1.75)^2 (0.0525)}{1.30 \times 10^{-2}} = 102576.9 \rightarrow f_2 = 0.021$

$N_H = \frac{V_1^2}{2g} = \frac{(3.97)^2 (0.0525)}{1.30 \times 10^{-2}} = 10326.9 \rightarrow f_1 = 0.021$

smaller than assumed

$(571.43 (0.021) + 0.7) \left(\frac{V_2^2}{2g} \right) = (1142.86 (0.021) + 4.66) \left(\frac{V_2^2}{2g} \right)$

$V_2 = 0.44 V_1$

$0.0141 = (2.168 \times 10^{-3}) V_1 + (2.168 \times 10^{-3}) (0.44 V_1)$

$V_1 = 3.96 \text{ m/s}$

$V_2 = 0.44 (3.96) = 1.75 \text{ m/s}$

$Q_1 = A_1 V_1 = (2.168 \times 10^{-3}) 3.96 = 0.008585 \text{ m}^3/\text{s} = 515.15 \text{ L/min}$

$Q_2 = A_2 V_2 = (2.168 \times 10^{-3}) 1.75 = 0.003794 \text{ m}^3/\text{s} = 227.7 \text{ L/min}$

$h_L = \frac{(571.43 (0.021) + 0.7) \frac{V_1^2}{2g}}{2g} = 10.15 \text{ m}$

$\Delta p = \gamma h_L$

$9.81 \text{ kN/m}^3 (10.15 \text{ m}) = 99.57 \text{ kPa}$

12.5

Problem 12.5

160 mm outer diam. 150 mm inner diam. 150 mm outer diam. 150 mm inner diam.

Section I: 160 mm outer diam. 150 mm inner diam. 150 mm outer diam. 150 mm inner diam.

Section II: 150 mm outer diam. 150 mm inner diam. 150 mm outer diam. 150 mm inner diam.

Defined flow rate through both pipes = 32 L/min = 0.000533 m³/s

L = 30 m

Water at 10°C

$\gamma = 9.81 \text{ kN/m}^3$

$\nu = 1.30 \times 10^{-6} \text{ m}^2/\text{s}$

$\frac{p_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{p_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_{L1-2}$

$\frac{p_1}{\gamma} - \frac{p_2}{\gamma} = h_{L1-2} \Rightarrow \frac{\Delta p}{\gamma} = h_{L1-2}$

$\Rightarrow \frac{\Delta p}{\gamma} = h_{L1-2}$

$h_{L1-2} = 2 f_{1-2} \frac{L}{D} \frac{V_1^2}{2g} + h_{f1-2} + h_{L1-2} + h_{L2-3}$

$h_{L1-2} = 2 f_{1-2} \frac{L}{D} \frac{V_1^2}{2g} + h_{f1-2} + h_{L1-2}$

For the pipe network, $h_{L1-2} = h_{L1-2}$

$2 f_{1-2} \frac{L}{D} \frac{V_1^2}{2g} + h_{f1-2} + h_{L1-2} = 2 f_{1-2} \frac{L}{D} \frac{V_1^2}{2g} + h_{f1-2} + h_{L1-2}$

And LHS = $h_{L1-2} + h_{L1-2} + h_{L1-2}$

$= f_1 \frac{L}{D} \frac{V_1^2}{2g} + 2 K_{90} \frac{V_1^2}{2g} + K_{valve} \frac{V_1^2}{2g}$ $V_1 = \frac{16Q}{\pi D^2}$

$LHS = f_1 \frac{L}{D} \frac{8}{g \pi^2 D^5} Q^2 + 2 K_{90} \frac{8}{g \pi^2 D^5} Q^2 + K_{valve} \frac{8}{g \pi^2 D^5} Q^2$

$= (f_1 \frac{L}{D} + 2 K_{90} + K_{valve}) \frac{8}{g \pi^2 D^5} Q^2$

Similarly, RHS = $(f_2 \frac{L}{D} + 2 K_{90}) \frac{8}{g \pi^2 D^5} Q^2$

Combine the two equations

$(f_1 \frac{L}{D} + 2 K_{90} + K_{valve}) \frac{8}{g \pi^2 D^5} Q^2 = (f_2 \frac{L}{D} + 2 K_{90}) \frac{8}{g \pi^2 D^5} Q^2$

For the exact diameter

$(f_1 \frac{L}{D} + 2 K_{90} + K_{valve}) \frac{1}{D^5} = (f_2 \frac{L}{D} + 2 K_{90}) \frac{1}{D^5}$

$(6.6926 + 0.9995 + K_{valve}) \frac{1}{(0.015)^5} = (13.5553 + 1.17192) \frac{1}{(0.015)^5}$

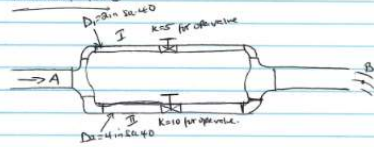
$(7.6926 + K_{valve}) \frac{1}{(0.015)^5} = 302628.1$

$7.6926 + K_{valve} = 226.82$

$K_{valve} = 219.13$

12.6

Problem 12.6



$$P_A = 20 \text{ psi}$$

$$K_{LB} = 0.9$$

$$\text{Neglect Tee losses}$$

$$\text{Pipe losses}$$

$$10 \text{ m/s } V = 6.24 \text{ m}^3/\text{s}$$

$$D_1 = 0.1733 \text{ m}$$

$$D_2 = 0.1335 \text{ m}$$

$$\frac{P_A}{\gamma} + \frac{V_A^2}{2g} + z_A = \frac{P_B}{\gamma} + \frac{V_B^2}{2g} + z_B + h_{L_{A-B}}$$

$$\frac{P_A}{\gamma} = h_{L_{A-B}} \Rightarrow \frac{P_A}{\gamma} = h_{L_{A-B}}$$

$$\Rightarrow \frac{P_A}{\gamma} = h_{L_{A-B}}$$

$$h_{L_{A-B}} = 2h_{L_{I}} + h_{L_{II}}$$

$$h_{L_{A-B}} = 2h_{L_{I}} + h_{L_{II}} = 2K_{LB} \frac{V_I^2}{2g} + K_{LB} \frac{V_{II}^2}{2g}$$

$$V^2 = \frac{16Q^2}{\pi^2 D^5}$$

$$h_{L_{A-B}} = 2h_{L_{I}} + h_{L_{II}} = 2K_{LB} \frac{V_I^2}{2g} + K_{LB} \frac{V_{II}^2}{2g}$$

$$h_{L_{A-B}} = (2K_{LB} + K_{LB}) \frac{8}{g\pi^2 D^5} Q^2 = (2 \times 0.9 + 0.9) \frac{8}{9.81 \pi^2 D^5} Q^2$$

$$h_{L_{A-B}} = (2K_{LB} + K_{LB}) \frac{8}{g\pi^2 D^5} Q^2 = (2 \times 0.9 + 0.9) \frac{8}{9.81 \pi^2 D^5} Q^2$$

$$\frac{P_A}{\gamma} = \left(\frac{2 \times 0.9 + 0.9}{6.24 \times 10^6} \right) Q^2 = 46.15 \text{ ft}$$

To evaluate for Q_I

$$46.15 \text{ ft} = \frac{(6.8) \cdot 8}{9.81 \pi^2 (0.1733)^5} Q_I^2$$

$$Q_I = \sqrt{\frac{46.15 \times 9.81 \times \pi^2 \times (0.1733)^5}{6.8 \times 8}} = 0.487 \text{ ft}^3/\text{s}$$

To evaluate for Q_{II}

$$46.15 \text{ ft} = \frac{(11.8) \cdot 8}{9.81 \pi^2 (0.1335)^5} Q_{II}^2$$

$$Q_{II} = \sqrt{\frac{46.15 \times 9.81 \times \pi^2 \times (0.1335)^5}{11.8 \times 8}} = 1.403 \text{ ft}^3/\text{s}$$

Total flow rate if:

a) Both valves open

$$Q_T = Q_I + Q_{II}$$

$$= 0.487 + 1.403$$

$$Q_T = 1.89 \text{ ft}^3/\text{s}$$

b) Valve II open (only)

$$Q_T = Q_{II}$$

$$Q_T = 1.403 \text{ ft}^3/\text{s}$$

c) Valve I open (only)

$$Q_T = Q_I$$

$$Q_T = 0.487 \text{ ft}^3/\text{s}$$