

Homework 3.3

This was the final week of the course; however, we still discussed a very important topic. The primary topic was how to select pumps and how to read graphs and charts to find the correct pump for a system. Pumps are usually thrown onto a graph with a great deal of overlap as pumps can cover certain ranges of speed and flow rate. Companies sometimes have these graphs in pamphlets to help sell their pumps or as a user's manual. The homework problems focused on chapter 13 and finding the Net Positive Suction Head or NPSH.

Homework Problems

Problem 13.17

For a given centrifugal pump, if the speed of rotation of the impeller is cut in half, how does the total capacity change?

$$\frac{h_{a1}}{h_{a2}} = \left(\frac{N_1}{N_2}\right)^2 \quad \text{If } N_2 = \frac{1}{2} N_1$$

$$\frac{h_{a1}}{h_{a2}} = \left(\frac{N_1}{\frac{1}{2}N_1}\right)^2 = 4$$

$$\frac{h_{a1}}{h_{a2}} = 4 \Rightarrow h_{a1} = 4h_{a2}$$

$$\therefore h_{a2} = \frac{h_{a1}}{4}$$

\Rightarrow If the speed of rotation of the impeller is cut in half, the total capacity reduced by a factor of 4.

Problem 13.19

For a given size of centrifugal pump casing, if the diameter of the impeller is reduced by 25%, how much does the capacity change?

$$\frac{Q_1}{Q_2} = \frac{D_1}{D_2} \quad \text{if } D_2 = 0.25 D_1$$

$$\frac{Q_1}{Q_2} = \frac{D_1}{0.25 D_1} \Rightarrow \frac{Q_1}{Q_2} = \frac{1}{0.25} \Rightarrow 0.25 Q_1 = Q_2$$

$$\therefore Q_2 = 0.25 Q_1$$

\Rightarrow If the diameter of the impeller is reduced by 25%, the capacity reduced by 25%.

Problem 13.22

Describe each part of this centrifugal pump design: 1½x3-6

- \rightarrow 1½-in discharge connection
- \rightarrow 3-in suction connection
- \rightarrow A casing that can accommodate an impeller with a diameter of 6-in or smaller.

Problem 13.23

Suitable pump size for delivering 100 gal/min of water at a total head of 300 ft.

Pump size: 1½x3-10

Problem 13.25

For a 2x3-10 pump, describe the performance that can be expected from a pump with an 8-in impeller operating against a system head of 300 ft.

Capacity - ~~23.5~~ gal/min

Power required - 22.5 hp

Efficiency - 53%

Required NPSH - 11 ft.

Problem 13.34

For each of the following sets of operating conditions, list the appropriate type of pump.

a) 500 gal/min of water at 80 ft of total head.
- Centrifugal pump - 3500 rpm.

b) 500 gal/min of water at 800 ft of head
- Reciprocating pump

f) 8000 gal/min of water at 200 ft of head.
- mixed flow pump

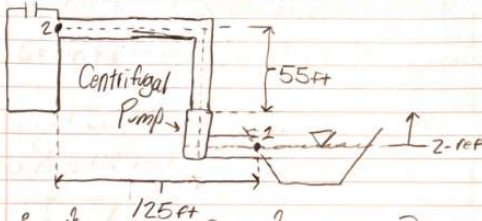
55 Q_{h1}
 FIND NPSH $T = 80^\circ C$ $P = 191.8 \text{ kPa}$
 water level 2m below pump
 DN 80 Sch 40 pipe - steel
 DN 50 Sch 40 pipe, 1.5m long 180° elbow
 $Q = 300 \text{ L/min}$ $\rho = 953$ $\nu = 3.60 \cdot 10^{-7}$
 $\frac{101.8 \cdot 10^3}{9.53 \cdot 10^3} = 10.682 \text{ m}$

 DN 80 $V = \frac{300 \text{ L/min}}{3.785 \cdot 10^{-3}} \cdot \frac{1 \text{ m}^3}{60000 \text{ L/min}} = 1.048 \text{ m/s}$
 $Re = \frac{(1.048)(953)}{3.6 \cdot 10^{-7}} = 226775.556$ $f = 0.019$
 $\frac{L}{D} = \frac{0.0779}{3.6 \cdot 10^{-2}} = 1693.428$ $\frac{L}{D} \cdot \frac{f}{2(9.81)} = 0.0559$
 DN 50 $V = \frac{300 \text{ L/min}}{2.16 \cdot 10^{-3}} \cdot \frac{1 \text{ m}^3}{60000 \text{ L/min}} = 2.306 \text{ m/s}$
 $Re = \frac{(2.306)(953)}{3.6 \cdot 10^{-7}} = 336291.667$ $f = 0.025$
 $(0.019) \left(\frac{1.048^2}{2(9.81)} \right) (0.0559) + (75 \cdot 0.018 \cdot \frac{1.048^2}{2(9.81)}) + (20 \cdot 0.018 \cdot \frac{1.048^2}{2(9.81)})$
 $+ 0.025 \left(\frac{2.306^2}{2(9.81)} \right) (1.5) = 0.3166 \text{ m}$
 $NPSH = 10.682 - 2 - 0.3166 - 4.967 = 3.3984 \text{ m}$

65 $C413$
 PROpane $45^\circ C$ $sg = 0.48$ 1.84m below pump
 $h_{\text{solution}} = 0.92 \text{ m}$ $P_{\text{atm}} = 98.4 \text{ kPa}$ $NPSHA = 1.50 \text{ m}$
 $\rho = 0.48 \cdot 981 = 470.88$ $h_{VP} = 340 \text{ m}$
 $P_2 = [470.88(1.5 + 1.84 + 0.92 + 340)] - 98.4$
 $= 1522.6515 \text{ kN/m}^2$

Design problem #3 Trey Ward

Design a system to pump water at 80°F from a river to a tank elevated 55 ft above the surface of the river. Minimum flowrate is 1500 gal/min. The tank is to be set back 125 ft from the river bank.



$$\left\{ \frac{P_1}{\gamma} + \frac{V_1^2}{2g} + Z_1 - h_L = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + Z_2 - h_{\text{pump}} \right\}$$

Both points 1 & 2 are open to atmosphere with no velocity of note. $\Rightarrow P_1 = 0, P_2 = 0, V_1 = 0, V_2 = 0$

$$\Rightarrow \{ Z_1 - h_L = Z_2 - h_{\text{pump}} \} \cdot Z_1 = 0 = Z_{\text{ref}}$$

$$\Rightarrow \{ h_{\text{pump}} - h_L = Z_2 \} \quad Z_2 = 55 \text{ ft}$$

$$\Rightarrow \{ h_{\text{pump}} - h_L = 55 \text{ ft} \}$$

Water @ 80°F

$$\gamma = 62.2 \text{ lb/ft}^3$$

System Info

$$Q = 1500 \frac{\text{gal}}{\text{min}} = 25 \frac{\text{gal}}{\text{sec}} = 3.34 \frac{\text{ft}^3}{\text{sec}}$$

$$L_{\text{pipe}} = 55 + 125 = 180 \text{ ft}$$

$$\eta = 1.77 \cdot 10^{-5}$$

Calculating for Cross Section of pipe & diameter

$$\{ Q = V \cdot A \} \quad V = 10 \text{ ft/s}, Q = 3.34 \text{ ft}^3/\text{s}$$

$$\Rightarrow A = 3.34 \frac{\text{ft}^3}{\text{s}} / 10 \frac{\text{ft}}{\text{s}} = 0.334 \text{ ft}^2$$

$$\Rightarrow A = 48.1 \text{ in}^2 \quad \{ A = \pi \cdot r^2 \}$$

$$\Rightarrow \{ r = \sqrt{\frac{A}{\pi}} \} \Rightarrow r = 3.91 \Rightarrow D = 7.83$$

• Round up for efficiency losses

$$\Rightarrow D = 8 \text{ in} \quad \text{• Use NPS 8 schedule 40 steel pipe}$$

$$\Rightarrow \epsilon = 1.5 \cdot 10^{-4} \text{ ft}$$

Reynolds # Calculations

$$\{ N_R = \frac{V \cdot D \cdot \gamma}{\eta} \} = \frac{10 \frac{\text{ft}}{\text{s}} \cdot 0.6667 \text{ ft} \cdot 62.2 \frac{\text{lb}}{\text{ft}^3}}{1.77 \cdot 10^{-5} \text{ lb-s/ft}^2}$$

$$= N_R = 23428666.67 = 2.3 \cdot 10^7$$

$$\frac{D}{\epsilon} = \frac{0.6667 \text{ ft}}{1.5 \cdot 10^{-4} \text{ ft}} = F = 0.015$$

Calculating energy losses in 180 ft of NPS 8 schedule 40 steel pipe, when water at 80°F is flowing through it at 10 ft/s

$$\left\{ h_L = f \cdot \frac{L}{D} \cdot \frac{V^2}{2g} \right\} \quad f = 0.015$$

$$L = 180 \text{ ft} \quad D = 0.6667 \text{ ft}$$

$$V = 10 \text{ ft/s} \quad g = 32.2 \text{ ft/s}^2$$

$$\Rightarrow \frac{180}{0.6667} = 270 \quad V^2 = 100 \frac{\text{ft}^2}{\text{s}^2} \quad 2g = 64.4 \frac{\text{ft}}{\text{s}^2}$$

$$\Rightarrow 0.015 \cdot 270 \cdot \frac{100 \frac{\text{ft}^2}{\text{s}^2}}{64.4 \frac{\text{ft}}{\text{s}^2}} = 6.3 \text{ ft}$$

Calculating necessary pump head for given losses & system

$$\{ h_{\text{pump}} = 55 \text{ ft} + h_L \} \Rightarrow 55 \text{ ft} + 6.3 \text{ ft} = 61.3 \text{ ft}$$

$$\Rightarrow h_{\text{pump}} = 61.3 \text{ ft} \quad \text{• based off figure 13-20 we know a centrifugal pump should deliver the necessary pump head.}$$