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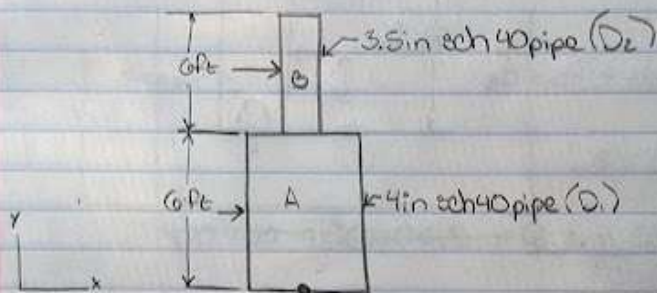
exam 3

Problem 1

Purpose:

Compute the moment at the base of a vertical pole

Drawing



Sources

Mott Robert L. Untener, Joseph Applied Fluid mechanics
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Design considerations

The flow must be assumed:

- 1) Incompressible fluid
- 2) Isothermal process
- 3) Steady state

Data and Variables

$$D_1 = 4.5 \text{ in} \rightarrow 0.375 \text{ ft}$$

$$D_2 = 40 \text{ in} \rightarrow 0.333 \text{ ft}$$

Temp 71°

$$P = 2.28 \times 10^{-3} \text{ slug/ft}^2$$

$$V = 80 \text{ mi/h} \rightarrow 117.35 \text{ ft/s}$$

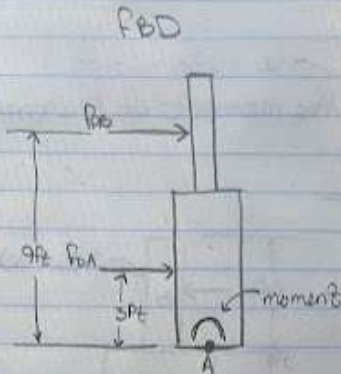
$$\nu = 1.69 \times 10^{-4} \text{ ft}^2/\text{s}$$

Procedure:

$$F_D = C_D \left(\frac{\rho V^2}{2} \right) A$$

$$C_D = \frac{V_D}{V}$$

$$M = F_D \times d_A + F_D \times d_B$$



Calculations:

$$C_{D1} = \frac{117.33 (0.375)}{1.69 \times 10^4} = 2.60 \times 10^{-3} = C_D = 0.9$$

$$C_{D2} = \frac{117.33 (0.833)}{1.69 \times 10^4} = 2.31 \times 10^{-3} = C_D = 0.9$$

$$A_A = 6 \times 0.375 = 2.25 \text{ ft}^2$$

$$A_B = 6 \times 0.833 = 1.998 \text{ ft}^2$$

$$F_{D1} = 0.9 \left(\frac{2.28 \times 10^{-3} \times 117.33^2}{2} \right) 2.25 = 31.78 \text{ lbf}$$

$$F_{D2} = 0.9 \left(\frac{2.28 \times 10^{-3} \times 117.33^2}{2} \right) 1.998 = 28.22 \text{ lbf}$$

$$M = 31.78 \times 3 + 28.22 \times 9 = \boxed{349.32 \text{ lb}\cdot\text{ft}}$$

Summary:

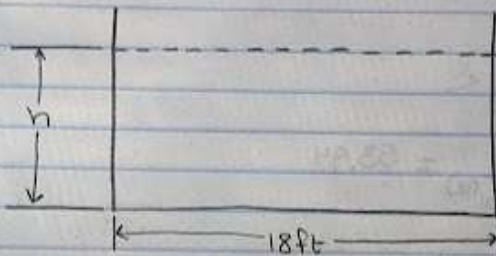
The moment at the base of the pole is
349.32 lb·ft.

Problem 2

Purpose

Determine the liquid height
Is the flow supercritical or subcritical?

Drawings



Source:

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Design considerations

The following must be assumed

- 1) Incompressible fluid
- 2) Isothermal process
- 3) Steady state

Data and Variables

$$Q = 150 \text{ ft}^3/\text{s}$$

$$W = 18 \text{ ft}$$

$$n = 0.017$$

$$S = 0.001$$

Procedure:

$$AR^{2/3} = \frac{nQ}{1.49S^{1/2}}$$

$$R = \frac{A}{WP}$$

Calculations

$$AR^{2/3} = \frac{0.017 * 150}{1.495 * 0.001^{1/2}} = 53.94$$

$$A = 18(h)$$

$$R = \frac{18(h)}{2h+18}$$

See excel $h = 1.11 \text{ ft}$

$$18(h) \left(\frac{18(h)}{2h+18} \right)^{2/3} = 53.94$$

$$E = \gamma + \frac{Q^2}{2g(A^3)} = 1.11 + \frac{150^2}{2 * 32.2 * (18 * 1.11)^2} = 2.80$$

$$V = \frac{Q}{A} = \frac{150}{19.98} = 7.51 \text{ ft/s}$$

$$Fr = \frac{V}{\sqrt{gY}} = \frac{7.51}{\sqrt{32.2 * (1.11/18)}} = 1.20$$

$Fr > 1.0 \therefore$ Supercritical

h (ft)	LHS	%diff
2	165.0656	101%
1.5	95.77408	56%
1.15	57.58066	7%
1.13	55.66843	3%
1.11	53.78612	0%

Summary:

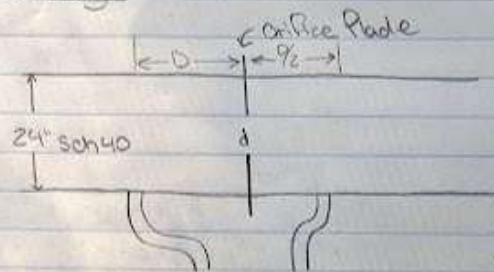
The height of the liquid is 1.11 ft and the flow is supercritical.

Problem 3

Purpose:

Compute the reading of a mercury manometer

Drawing:



Data and Variables:

$$Q = 6000 \text{ gpm} \rightarrow 13.37 \text{ ft}^3/\text{s}$$

$$D = 24'' \rightarrow ID = 1.886 \text{ ft} \quad A_1 = 2.792 \text{ ft}^2$$

$$B = 0.5$$

$$\gamma_{\text{water}} = 62.4 \quad \nu = 1.21 \times 10^{-5} \text{ @ } 60^\circ\text{F}$$

$$\gamma_m = 844.9 \text{ lb/ft}^3$$

Sources:

Mott Robert L. Untener, Joseph Applied Fluid mechanics
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Design considerations

The following must be assumed.

- 1) Incompressible fluid
- 2) Isothermal process
- 3) steady state

Procedure:

$$\beta = \frac{d}{D} \quad \therefore d = \beta D$$

$$h_0 = \frac{VD}{\nu}$$

$C =$ from chart

$$h = \frac{\left(\frac{Q}{A \times C}\right)^2 \times \left[\left(\frac{A_1}{A_2}\right)^2 - 1\right]}{2g \left(\frac{Y_m}{Y_w} - 1\right)}$$

Calculations:

$$d = 0.5(1.886) = 0.943 \text{ ft} \quad A_2 = \frac{\pi(0.943)^2}{4} = 0.70 \text{ ft}^2$$

$$Q = \frac{V}{A} \quad \therefore V = QA = 13.37 \times 2.792 = 37.33 \text{ ft}^3/\text{s}$$

$$h_0 = \frac{37.33 \times 1.886}{1.21 \times 10^{-5}} = 5.82 \times 10^6$$

$$C = 0.602 \text{ (from table)}$$

$$h = \frac{\left(\frac{13.37}{2.792 \times 0.602}\right)^2 \times \left[\left(\frac{2.792}{0.70}\right)^2 - 1\right]}{2 \times 32.2 \left(\frac{844.9}{62.4} - 1\right)} = \frac{63.28 \times 14.91}{807.58} = 1.168 \text{ ft}$$

Summary

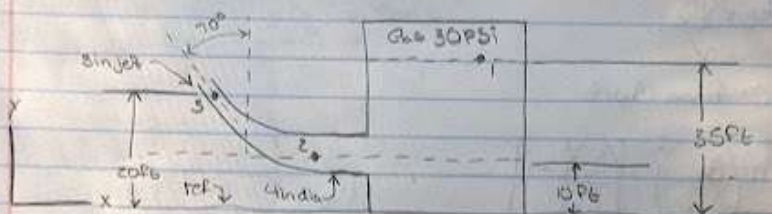
The mercury deflection is 1.168 ft or 14.01 in.

Problem 4

Purpose:

Compute the force on the curve pipe section.

Drawing:



Source:

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Design considerations:

The following must be assumed

- 1) Incompressible fluid
- 2) Isothermal process
- 3) Steady state

Data and Variables:

$$P_1 = 30 \text{ PSI} \rightarrow 4320 \text{ lbf/ft}^2$$

$$L_{\text{curve}} = 10 \text{ ft}$$

$$\gamma = 55 \text{ lbf/ft}^3$$

$$D_{\text{jet}} = 3 \text{ in} \rightarrow 0.25 \text{ ft}$$

$$D_{\text{discharge}} = 4 \text{ in} \rightarrow 0.33 \text{ ft}$$

$$A_2 = 8.727 \times 10^{-2} \text{ ft}^2$$

$$A_3 = 4.909 \times 10^{-2} \text{ ft}^2$$

Procedure

$$\begin{aligned} \text{Find } Q \\ \frac{P_1 + V_1^2}{\gamma z_0} + z_1 &= \frac{P_2 + V_2^2}{\gamma z_0} + z_2 \\ \frac{P_1 + z_1}{\gamma} &= \frac{V_2^2}{\gamma z_0} + z_2 \end{aligned}$$

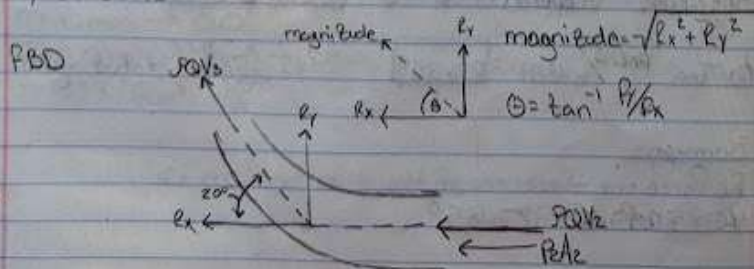
$$V_2 = \sqrt{\frac{(P_1 + z_1 - z_2) \gamma z_0}{\gamma}}$$

$$Q = V_2(A_2) \quad V_2 = \frac{Q}{A_2}$$

$$\begin{aligned} \frac{P_1 + V_1^2}{\gamma z_0} + z_1 &= \frac{P_2 + V_2^2}{\gamma z_0} + z_2 \\ \frac{P_1 + z_1}{\gamma} &= \frac{P_2 + V_2^2}{\gamma z_0} + z_2 \\ P_1 - P_2 &= \gamma \left(\frac{V_2^2}{z_0} + (z_2 - z_1) \right) \\ &= -P_2 = P_1 + \gamma \left(\frac{V_2^2}{z_0} + (z_2 - z_1) \right) \end{aligned}$$

$$R_x = P_2 A_2 - \rho g A_2 \cos 20^\circ + \rho g V_2$$

$$R_y = \rho g V_2 \sin 20^\circ$$



Calculations

$$V_0 = \sqrt{\frac{4320 + 25}{55}} 2(32.2) = 81.66 \text{ ft/s}$$

$$A_3 = 4.909 \times 10^{-2} \text{ (from table)}$$

$$Q = 81.66 \times 4.909 \times 10^{-2} = 4.009 \text{ ft}^3/\text{s}$$

$$V_2 = \frac{4.009}{8.727 \times 10^{-2} \text{ (from table)}} = 45.93 \text{ ft/s}$$

$$P_2 = 4320 + 55 \left(\frac{45.93^2}{2 \times 32.2} \right) + 25 = 6146.65 \text{ lbf/ft}^2$$

~~$$\text{Volume} = \frac{\gamma L}{12} (D_{\text{top}}^2 + D_{\text{top}} \times D_{\text{discharge}} + D_{\text{discharge}}^2)$$
$$= \frac{97.10}{12} (0.25^2 + 0.25 \times 0.33 + 0.33^2) = 0.605 \text{ ft}^3$$~~

$$P = \frac{\gamma}{g} = \frac{55 + 0.108 \text{ slugs/ft}^3}{32.2}$$

$$R_x = 6146.65(8.727 \times 10^{-2}) - 17.08 \times 4.009 \cos 20^\circ + 17.08 \times 4.009 \times 45.93$$
$$= 3618.91 \text{ lbf}$$

$$R_y = 17.08 \times 4.009 \times 81.66 \sin 20^\circ = 112.43 \text{ lbf}$$

$$\text{magnitude} = \sqrt{(3618.91)^2 + (112.43)^2} = 4093.15 \text{ lbf}$$

$$\theta = \tan^{-1} \frac{112.43}{3618.91} = 27.85^\circ$$

Summary

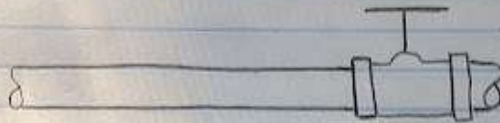
The force on the curve of the pipe section is 4093 lbf at 27.85°.

Problem 5

Purpose:

Calculate the pressure increment when the valve closes all of a sudden.

Drawing



Source:

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Design considerations

The following must be assumed

- 1) Incompressible fluid
- 2) Isothermal process
- 3) Steady state

Data and Variables:

$$D = 600 \text{ mm} \rightarrow 0.6 \text{ m}$$

$$V = 1.0 \text{ m/s}$$

$$E = 2 \times 10^7 \text{ N/cm}^2 \rightarrow 2 \times 10^9$$

$$\sigma = 10 \text{ mm} \rightarrow 0.01$$

$$E_0 = 2.03 \times 10^5 \text{ N/cm}^2 \rightarrow 2.03 \times 10^9$$

$$\rho = 978 \text{ kg/m}^3$$

Procedure:

$$\Delta P = 30 \text{ V}$$

$$C = \frac{\sqrt{\frac{E_0}{P}}}{\sqrt{\frac{1 + E_0 D}{E_0}}}$$

Calculations:

$$C = \frac{\sqrt{\frac{2.03 \times 10^9 \text{ N/m}^2}{978 \text{ kg/m}^2}}}{\sqrt{\frac{1 + 2.03 \times 10^9 \text{ N/m}^2 * 0.001 \text{ m}}{2 \times 10^{11} \text{ N/m}^2 * 0.01 \text{ m}}}} = \frac{1440.72}{1.27} = 1135.80$$

$$\Delta P = 978 * 1135.80 * 1.0 = \boxed{1110811.63 \text{ kPa}}$$

Summary:

The pressure increment when the valve shuts suddenly is 1110811.63 kPa.